LETHBRIDGE COUNTY IN THE PROVINCE OF ALBERTA

BY-LAW NO. 1426

A BY-LAW OF LETHBRIDGE COUNTY BEING A BY-LAW PURSUANT TO SECTION 633(1) OF THE MUNICIPAL GOVERNMENT ACT, REVISED STATUTES OF ALBERTA 2000, CHAPTER M.26

WHEREAS Dar Ray Farms wishes to develop an Agri-Business Park on Lots 1-3, Block 1, Plan 0814065.

AND WHEREAS the County's Municipal Development Plan requires that developers prepare an Area Structure Plan to ensure sound development occurs within the County;

AND WHEREAS the total area of the development will be 138 acres with consideration for the lands to the north (portion of NW 5-8-20-W4).

AND WHEREAS the landowner/developer have prepared the "508 Agri-Business Park - Area Structure Plan" which contains engineering, survey, and geotechnical information to support the above conditions.

NOW THEREFORE BE IT RESOLVED, under the Authority and subject to the provisions of the Municipal Government Act, Revised Statutes of Alberta, 2000, Chapter M-26, as amended, the Council of Lethbridge County in the Province of Alberta duly assembled does hereby enact the following:

1. The "508 Agri-Business Park Area Structure Plan" Bylaw No.1426, attached as "Appendix A".

Reeve Chief Administrative Officer

GIVEN first reading this 7th day of August, 2014.

GIVEN second reading this 18th day of September 2014

Reeve

Chief Administrative Officer

GIVEN third reading this and day of October, 2014

Reeve

Chief Administrative Officer

AREA STRUCTURE PLAN

508 AGRI-BUSINESS PARK in Sec. 05-008-20-W4 Lethbridge County, AB

Submitted to Lethbridge County

PREPARED FOR:

Ray Taylor Dar Ray Farms RR 8 – 18 – 5 Lethbridge, AB T1J 4P4

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1.0 INTRODUCTION

This Area Structure Plan has been prepared by Hasegawa Engineering Ltd. on behalf of Dar Ray Farms Ltd. to describe the development concept and municipal servicing strategy to be provided for the 508 Agri-Business Park. The site lies at the junction of Highway 4 and Highway 508 in the south of Lethbridge County. (Figure 1) The Area Structure Plan describes the ultimate development of the subject lands, which include portions of Section 5, Range 8, Township 20, west of the 4th Meridian.

As the intended purpose is the development of an industrial area, an Area Structure Plan is required under Section 6.2 of the Municipal Development Plan of Lethbridge County.

This Area Structure Plan is submitted as support for the application to adopt the Plan as a By-Law of Lethbridge County and the subsequent change to the Land Use By-Law. The Area Structure Plan will provide a basis for evaluation of future applications for subdivision of parcels and building development.

Dar Ray Farms Ltd. (Dar Ray Farms) has previously subdivided two lots and created a new public roadway within this quarter. The remaining lands owned by Dar Ray include approximately 39 hectares (90 acres) of land which is actively farmed. The remaining lands also include remnants of the adjacent NE ¼ of Section 5-8-20-4 and the SW ¼ of Section 5-8-20-4.

2.0 PLANS AND DRAWINGS

In order to illustrate the location of the property, site drainage, and the proposed subdivision layout, five figures have been prepared. The figures are provided in Appendix A and are as follows:

- 1.1 Location Plan
- 2.1 Proposed Development Phasing Plan
- 3.1 Proposed Land Use
- 4.1 Existing Features & Topography
- 4.2 Section AA Plan & Profiles
- 4.3 Section BB Plan & Profiles
- 4.4 Section CC Plan & Profiles

These maps are conceptual in nature and are to be used for planning purposes only. Upon ASP acceptance, detailed design plans will be prepared and submitted with any subdivision application.

3.0 LAND USE CONCEPT

3.1 Existing Conditions

The lands within the boundaries of the proposed Area Structure Plan are currently used for an agri-business development and the major portion is cropped agricultural land. The lands are bordered by the railway and Highway 4 to the east and by Highway 508 to the south. The western edge of the property lies adjacent to a major canal belonging to the St. Mary River Irrigation District. To the north lies agricultural land under irrigation. Acreages lie beyond the border areas to the north, south and west.

3.2 Development Objectives

The objective of the Developer of the 508 Agri-Business Park is:

"To create a high quality environment that will provide a location for the establishment and growth of businesses which provides services to the agricultural base of Lethbridge County".

Preferred Development Concept

The preferred development concept appears in Figures 2 and 3. The ultimate development will create approximately 55 ha (137 acres) of net developable area. The remainder of the land is dedicated to roads, a public utility lot for a pond providing stormwater retention and fire protection and a green strip along the canal.

Lot sizes will range from 0.8-2.8 ha (2-7 acres) in size. Larger lots may be considered. Based on an average lot size of 1.8 hectares (3.0 acres), this will result in approximately 25 lots.

Figures 2 and 3 indicate the parcel to the northwest as future development. This landowner has expressed interest in being part of the development but at this time this northern area is <u>not</u> part of this Area Structure Plan.

Land Use Classification

The proposed land use classification of the subdivision is Rural General Industrial (RGI) and Business Light Industrial (BLI) per Lethbridge County Land Use Bylaw. A figure depicting the anticipated land use designations within the development is provided on Figure 3.

The intent is to provide developable land for industry and businesses that support the local agricultural sector and to a lesser extent the evolving resource development sector. The western portion is proposed to receive the BLI classification as opposed to the RGI classification to reduce the impact on acreages west of the canal.

Lethbridge County Municipal Development Plan

The Lethbridge County Municipal Development Plan contains policies for industrial development. The location of the proposed development meets these policies for the following reasons:

- The site is located adjacent to the junction of major transportation routes (Highway 4 and Highway 508)
- The site does not contain any sensitive environmental, cultural or historical features
- While the lands involved have been farmed historically, they are not considered high quality. The soils are mapped as class three, but they are not irrigated, the property is an irregular shape and the property contains unusable low areas.
- The site already contains businesses dedicated to supporting the agricultural community

3.3 Proposed Land Use Areas

The distribution of land use within the proposed ASP is shown in Table 1 below.

Table 1: Land Use Statistics

	Hectares (Acres)	Percent of Gross Area
Net Developable Area	44.6 (110.2)	80%
Rural General Industrial	35.9 (88.7)	64%
Business Light Industrial	8.7 (21.5)	16%
Public Utility Lot - Ponds	5.0 (12.3)	9%
Roads and Right-of-ways	4.8 (11.8)	9%
Municipal Reserve – Parks/Green-space	1.0 (2.4)	2%
Gross Developable Area	55.7 (137.7)	100%

4.0 SERVICING

In order to determine the viability of this development, preliminary evaluations have been performed with respect to servicing. Key service items include sewer, water, natural gas, telephone, television, and electric. Additional information on key services is included in this section.

4.1 Sanitary Sewer System

Sanitary sewage will be handled by a communal sewage disposal system and installed in accordance with the Alberta Private Sewage System Standard of Practice.

A preliminary soil study has been performed for this property (refer to Appendix B). As part of that study soil samples were collected and sent for grain size and hydrometer analysis. Four sites were selected and six samples were submitted to AMEC for analysis and the results are included in Table 2 below.

Table 2 Soil Analysis Results

Sample ID	Soil type	Suitable for Septic Field
TH1 8 ft	Silty Clay Loam	possibly
TH1 10 ft	Clay Loam	possibly
TH2 6 ft	Clay Loam	possibly
TH3 4 ft	Silty Clay Loam	possibly
TH3 8 ft	Loam	yes
TH4 4 ft	Silt Loam	possibly

Groundwater was detected at two sites close to the canal at a depth of 1.5 metres. Groundwater was not detected at the other two sites.

The suitability of the soils for a septic field is listed in Table 2 as possibly suitable for septic fields because it was found that the soil structure for the profiles sampled was undeterminable.

The soil types found have high clay content and generally be of medium grade. The soil structure determines the ability of a clay soil to allow infiltration. If the soil structure is platy it is unsuitable for septic fields. If the soil structure is prismatic or blocky it is suitable for septic fields. Further testing is required to determine conclusively the soil structure at the location of a proposed sewage system.

The soils closer to the surface were noted as being of a looser composition and therefore more suitable but are of an insufficient depth for septic fields.

In order to take a conservative approach, it is assumed the soil will be unsuitable for a septic field. The communal septic system will be a treatment mound type of system. This method of sewage treatment will also provide extra protection of the shallow groundwater by increasing the separation distance between the elevation of the sewage treatment area and the groundwater table.

Lethbridge County will assume ownership and responsibility of the sewage treatment system upon completion of the infrastructure.

4.2 Water Systems

It is proposed that each lot will be serviced with limited potable water and non-potable water. This section covers how each of these water supply issues will be addressed.

4.2.1 Potable Water

Potable water services are provided by the Lethbridge South County Rural Water Association to the two existing lots. The developer currently owns three shares from the co-op. Presently, the co-op has no ability to provide new potable water to non-residential users. Therefore the existing shares will be used to provide limited amounts of potable water to the development. It will not be permitted to use this potable water for intensive water operations (truck washing etc.). For the initial phases the existing co-op shares will be a sufficient water supply. If the existing shares are an insufficient supply for the later phase, water will be hauled until additional water becomes available from the co-op.

Cisterns with pressure systems will be required for each property. Provision of individual cisterns for each lot with in the development will allow potable water to be delivered to the lots by truck in the event that the water co-op cannot provide sufficient volumes.

As the development area would be served by the Association, a new water licence would not be required by AESRD.

Since the treated water supply has a definite limit, high water use businesses that require large amounts of treated water should not be permitted within the development area unless a more substantial water supply is established.

Lethbridge County will assume ownership and responsibility of the potable water system upon completion of the infrastructure.

4.2.2 Non-Potable Water / Fire Protection

The proposed development concept will include a non-potable water system with conventional fire hydrants distributed throughout the development. The non-potable water system will include a raw water reservoir (separate from the stormwater management pond) adjacent to the SMRID canal, a pumping station, and distribution piping within the development. The non-potable water system will distribute non potable water to each lot in the subdivision for non-potable use. A stationary pumping system will be provided to maintain pressure in the non-potable water distribution system and to supply water to hydrants for fire-fighting. Fire hydrants will be placed along the public roadways for use by responding emergency services personnel. This pond will also provide water for irrigation of the landscaped area adjacent to the ponds and the green strip along the canal.

An agreement will be required for the use of water from the SMRID canal to maintain volumes within the raw water reservoir. The SMRID has the capacity and legal ability to deliver water for other purposes and an agreement will dictate when and how that operation can occur.

Lethbridge County will assume ownership and responsibility of the raw water system upon completion of the infrastructure.

4.3 Gas

Natural gas distribution infrastructure in the area surrounding the site is operated by Triple W Gas. The developer will pay for the installation of natural gas distribution infrastructure to each lot. Triple W Gas will distribute natural gas within the development and lot purchasers will be able to select a retailer for natural gas supply.

4.4 Electrical Power

Fortis Alberta Inc. will provide services to the proposed subdivision and underground services to each property line.

4.5 Telephone

Telus will provide services to the lots, but each individual owner must apply for the service when building.

4.6 Shaw Cable

There is no cable television available in the area, however, small satellite dishes may be installed by the lot owner.

5.0 ROADS AND TRANSPORTATION

The existing entrance to the area to be developed lied across from the junction of Range Road 20-4 with Highway 508. Alberta Transportation has indicated that it will not support the utilization of this entrance for a new subdivision. Therefore the entrance to the subdivision will be further west closer to the canal. (Figure 2)

A looped road will run through the area to provide access to each lot. Roads within the subdivision will comply with Lethbridge County Engineering Guidelines. The road will consist of a 20 m right-of-way with open drainage to the sides. Roads will be paved and meet County standards to allow for truck access.

Lethbridge County will assume ownership and responsibility of the internal road system upon completion of the infrastructure.

A Traffic Impact Assessment (Appendix C) has been completed to analyze the impact of the development on the adjacent road network.

The TIA also indicated upgraded safety measures are warranted at the railway crossing on Highway 508 and the creation of a right turn lane into the development area is required. It also indicated illumination at the Highway 5/Highway 508, the Highway 4/Highway 508 and the development entrance is warranted.

6.0 SITE DRAINAGE AND GRADING

All drainage onsite must conform to Lethbridge County and Alberta Environment and Sustainable Resource Development requirements. The intent of stormwater management for the development is to contain runoff in a stormpond until it can be released into the SMRID drainage channel leading to Six Mile Coulee located on the west side of the canal. A Site Drainage Analysis was completed for the site (Appendix D) and is summarized below.

6.1 Site Drainage

Stormwater runoff from the subject lands presently flows into the existing roadside ditches or is trapped against the canal and ponds in low areas. Figures 4-7 show the topography of the site.

A storm water management pond will be located in the area of the existing topographic low area along the east side of the irrigation canal. The pond will receive storm water runoff from the subdivision by means of an overland drainage system constructed within the development area. The overland drainage system will consist of roadside ditches and lot line swales to collect and convey storm water runoff to the pond. Roadside ditches will be contained in the road right-of-way. Right-of-ways will be established for the drainage swales along property boundaries.

6.2 Drainage Modeling

As stormwater may not be able to be released immediately into the drainage channel, the pond will be designed to contain the volume generated by the design storms. To determine the required active storage volume of the pond, a hydrologic model of the site was prepared using the PC SWMM hydrologic modeling software package. The hydrologic model of the site post-development was then analyzed using a 1:100 year 24 hour design storm event.

The results of the hydrologic modeling indicate a required storage volume of 57,187 cubic meters to attenuate the runoff from the site. The stormwater management facility was sized to detain runoff volume generated. The hydrologic model will be reviewed during the detailed design stage to confirm the required capacity of the overland drainage system and culverts. Detailed design will also determine sizing and location of pumps and pipes accessing the canal.

6.3 Stormwater agreements and approvals

Storm water runoff collected in the pond will be released to the SMRID drainage channel located to the west of the canal. The County currently has an agreement with the SMRID for the release of stormwater into irrigation canals. (Appendix E) It is assumed this pond can be operated under this agreement.

The storm water management pond will be created on a public utility lot and will be operated by the Lethbridge County

Authorization and/or agreements will have to be obtained from the SMRID and the landowner to the east to install and operate a drainage system for the pond. A pipe will lead under the canal and either directly connect with the drainage channel or be connected with the drainage channel by a new local drainage channel. The drainage system will be operated such that stormwater runoff will be held in the pond and only released when there is downstream capacity to receive the water.

The storm water detention pond will require an approval under the Water Act and a registration under EPEA from AESRD as a municipal storm water management pond prior to construction.

7.0 SOLID WASTE DISPOSAL

Lot purchasers will be responsible for making arrangements for solid waste disposal. The City of Lethbridge Regional Solid waste facility is located approximately 23km driving distance from the development. Alternatively, lot purchasers may contract with a private solid waste hauler.

8.0 OPEN SPACES

The area around the pond will be landscaped so that it can be used as open space by members of the public. This will include grouped areas of trees and shrubs with low moisture demands. There will be a minimum of 1 tree per 130 sq m of greenspace (three shrubs equaling one tree)

Additionally a 15 metre wide green strip will be established between the canal right of way and the nearest lot boundary. Trees and a walkway will be established along this boundary. Tree species will be selected for characteristics of climate tolerance, speed of growth and significant height. Size of trees planted will large as defined in the Lethbridge County Land Use Bylaw Part 3, Section 25 (10) (a)

(vii). The trees will be spaced appropriately to create a sound and visual barrier between the development and acreages to the west.

The green strip along the canal will be applied to the Municipal Reserve requirements for the development. The remainder will be supplied through direct payment. The decision on if the green strip is taken as municipal reserve is made at the time of subdivision. If the green strip is taken as municipal reserve, maintenance of the landscaped area will be the responsibility of Lethbridge County. If the green strip is not taken as municipal reserve maintenance of the landscaped area will be the responsibility of the owner association.

9.0 ARCHITECTURAL CONTROLS

The following controls are designed to ensure an environment that reflects the values of the community. These controls will be expanded and detailed at the subdivision stage of the development process. The following criteria will apply:

1. Entrance

- The entrance to the development will be landscaped with a mix of shrubs and xeriscaping
- The entrance will have signage of neat and attractive appearance

2. Property Design

- Each property owner is to be responsible for upkeep of utility right-ofway along property frontage
- A mandatory area of landscaping will be established for property frontages and will follow the guidelines of the Lethbridge County Land Use Bylaw Part 3 Section 25(10)
- Signage parameters will be established to enhance the development
- Parameters for permissible fencing and lighting will be developed
- Low impact lighting will be used to minimize light pollution

3. Building Design

- Lots adjacent to the canal will have a 30.5m building setback from the canal
- Consistent set back distances will be established from front and back property lines
- Concepts of green building design shall be encouraged
- Fronts of buildings will have to contain enhancements of color and material so that there is not continuous gray metal building fronts.

APPENDIX A - FIGURES



R APPROVAL
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Contrador to check and verify all dimensions before construction, any errors and omissions shall be reported to the engineer immediately

Drawing shall not be used for construction approved

Do not scale the drawing
All construction shall be in accordance with the latest codes, may it be construction, mechanical,

HABEGAWA
NO. 1370 - 2300 Sevet Bouth
Lehbridge, Menta 11K 784
Pr. 403-230-2068
Fax. 403-230-2728
Ernalt office@hasegarer ca

RAY TAYLOR

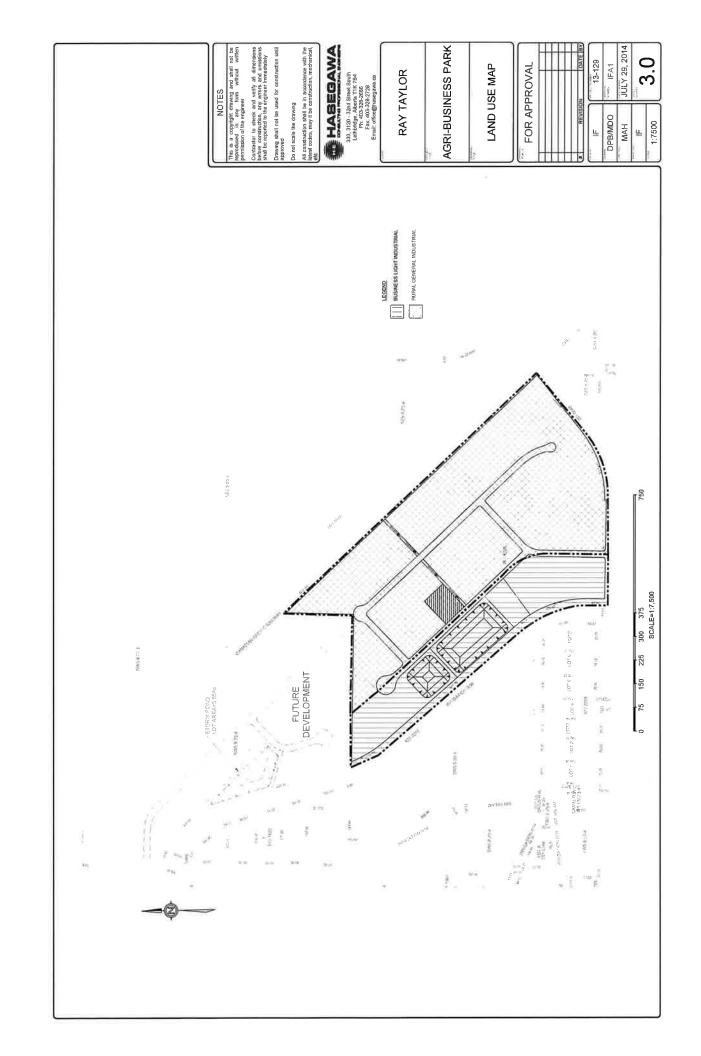
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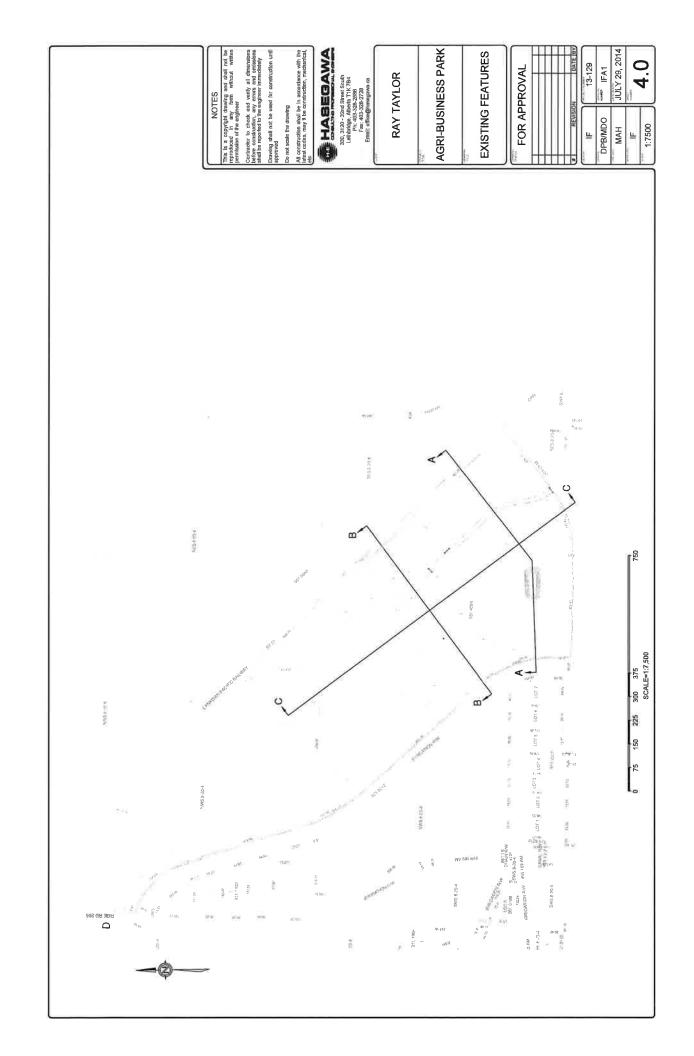
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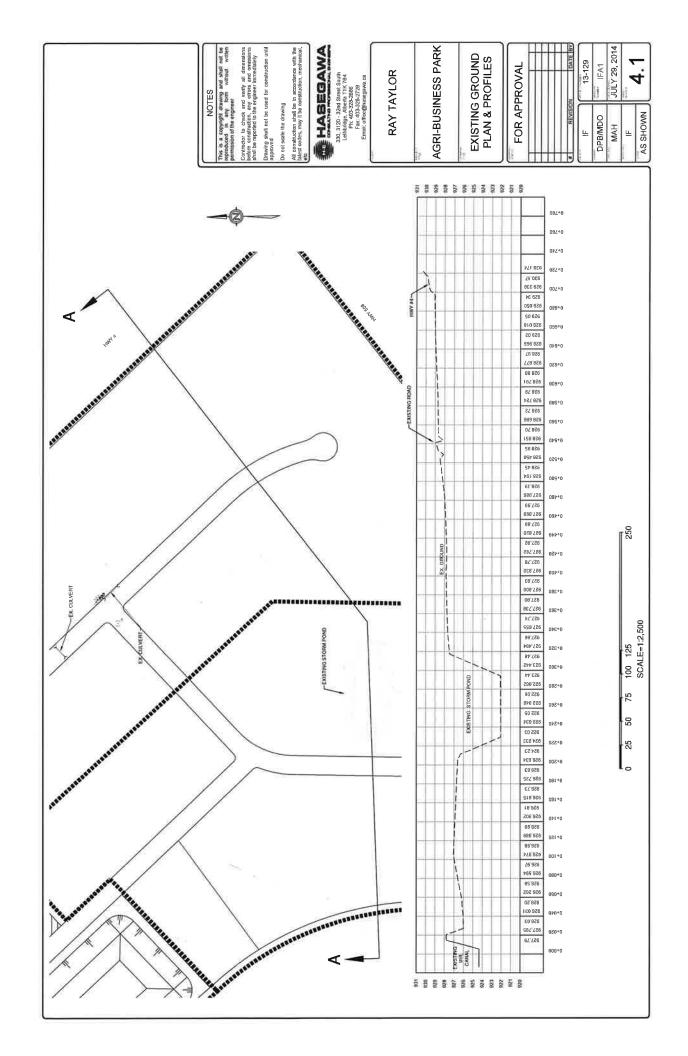
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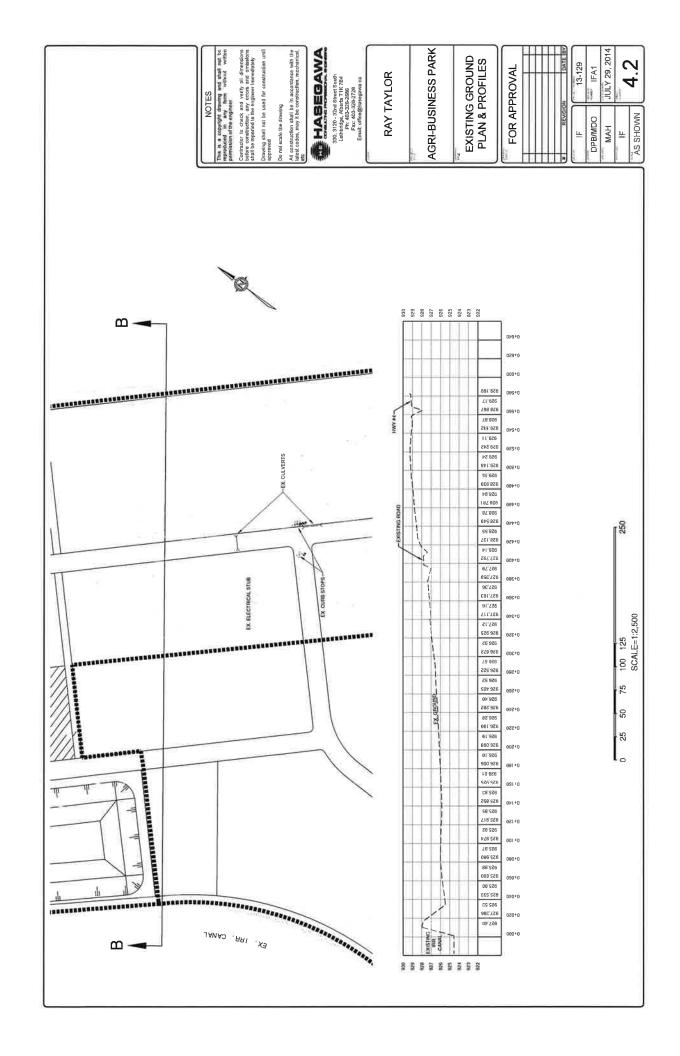
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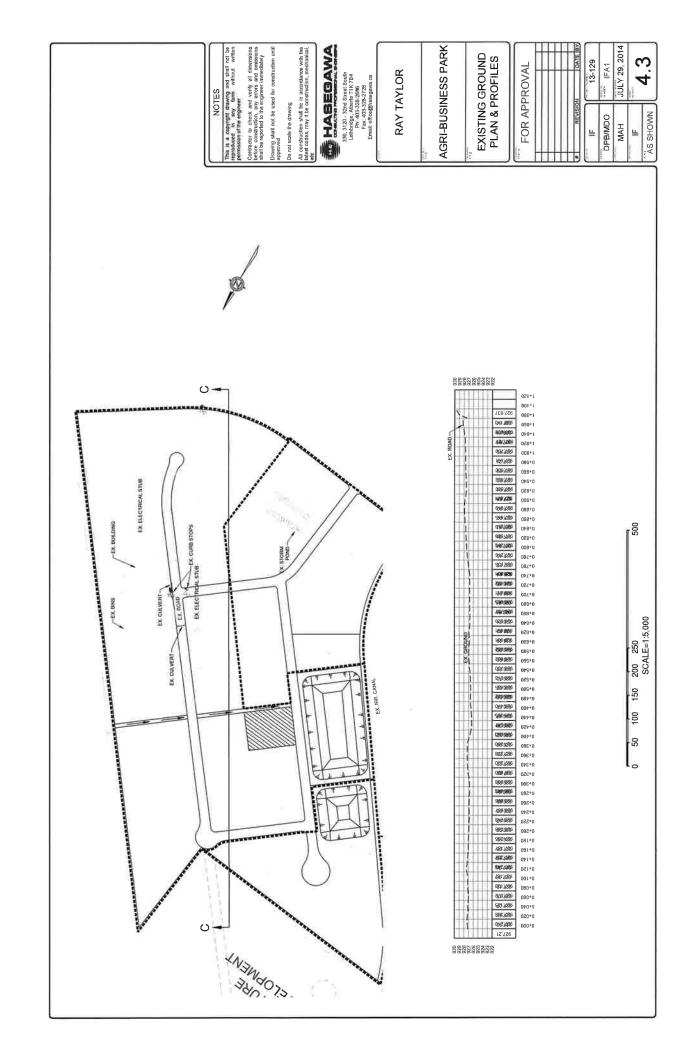
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APPENDIX B – SOIL TESTS RESULTS



330, 3120-32 Street South, Lethbridge, AB. T1K 7B4

Bus: 403-328-2686 Fax: 403-328-2728

E-mail: office@hasegawa.ca

Job #: 13-129

May 5, 2014

Dar Ray Farms Ltd. Attn: Ray Taylor RR 8-18-5 Lethbridge, AB T1J 4P4

By Email to: darrayfarms@yahoo.ca

Re: Soil testing for Agri Business Park Subdivision

Dear Ray:

On April 3 and 4, 2014 Hasegawa Engineering collected soil samples for the purpose of determining the suitability of the soil for the installation of septic fields, as well as for the building of roads and houses. The subject property is approximately 140 acres in size and is located in portions of the SE and SW 1/4 of Sec 5-T8-R20 West of the 4th Meridian. It is proposed that the land be subdivided into agri-business lots.

A backhoe and an auger attachment were used to drill three boreholes on the property. Three of the boreholes (BH1, BH2 and BH4) were drilled to a depth of 10 feet, while borehole three (BH3) was drilled to a depth of almost 15 feet. Soil samples were collected at eight and ten feet from BH1, six feet from BH2, four and eight feet from BH3, and four feet from BH4. All samples collected were submitted to AMEC Earth and Environmental for lab analysis to determine the soil composition and properties.

The lab test results are attached as well as copies from two pages of the Alberta Private Sewage Systems Standard of Practice (2009). The results show that the 8' sample from BH1 is 17% sand, 54% silt and 29% clay, which according to Figure 8.1.1.10. "Soil Texture Classification Triangle" classifies the soil as silty clay loam. The 10' sample from BH1 was 21% sand, 51% silt and 28% clay and would be classified as clay loam. The 6' sample from BH2 was 20% sand, 51% silt, and 29% clay which is classified as clay loam. The 4' sample from BH3 was 18% sand, 51% silt and 31% clay which is classified as silty clay loam. The 8' sample from BH3 was 25% sand, 50% silt and 25% clay and is classified as loam. The 4' sample from BH4 had 11% sand, 67% silt and 22% clay and is classified as silt loam.

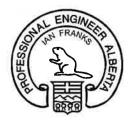
Table A.1.E.1. "Effluent Soil Loading Rates and Linear Loading Rates" from the Standards lists silty clay loam, clay loam and silt loam as having an infiltration rate that is possibly not suitable for use in a private septic field system. The effectiveness of these soils is dependent on the soil structure at a particular location in terms of both shape and grade. Soil structure will have to be determined for each individual site.

Loam is suitable for use in septic field systems. For these soil types if the soil structure is suitable, the effluent loading rate would be a minimum of 7.3 L/day/sq. metre. Different soil structures will yield different loading rates or possibly no permitted rates.

Further testing at specific potential septic field locations will be required to determine the suitability of the soils. It may be found that some sites are unsuitable for septic fields or septic mounds. In these locations other methods of sewage disposal would have to be considered.

The purpose of this letter is to only inform that the tests performed show if the soil on site will be suitable for a septic field. Further design work will need to be done by a certified individual to size an appropriate septic field for an individual property.

Yours truly,



lan Franks, P. Eng HASEGAWA ENGINEERING Consulting Professional Engineers IF

encl: AMEC test results (7 pages), Alberta Private Sewage Systems Standard of Practice (2 pages), BH Drilling Logs (2 pages)

Project Name:	Dar Ray Farms Agri Business F	Park	Project #:	13-129
Hole Description:	BH1		Bore Hole #:	1
Drilling Procedure:	Backhoe/auger		Hole Size:	6"
SPT Procedure:		SPT Size:	OD=	ID=
Sampling Procedure	Bucket/auger	Sampler Size	OD=	ID=
Logged By:	Ryan Olsen		Date:	April 3, 2014

Depth (FT)	WT	nses	Soil Sample Description	Moisture Content, w	Plasticity Index, PI	Dry Unit Weight, γ (pcf)	Friction Angle,	Penetro-meter (psf)	SPT	Cou N	unt,	Compressive Strength, Cu(psf)
0			Black, wet, top soil/stubble									
6"			Brown, damp, sandy clay till, loose									
4			Brown, moist, sandy clay till, some plastic									
5			to the state of th								_	
6			Brown, very moist, sandy clay till, soft									
10			End of Borehole									
10												

Project Name:	Dar Ray Farms Agri Business	Park	Project #:	13-129
Hole Description:	BH2		2	
Drilling Procedure:	Backhoe/auger		Hole Size:	6"
SPT Procedure:		SPT Size:	OD=	ID=
Sampling Procedure	Bucket/auger	Sampler Size	OD=	ID=
Logged By:	Ryan Olsen		Date:	April 3, 2014

Depth (FT)	WT	USGS	Soil Sample Description	Moisture Content, w	Plasticity Index, PI	Dry Unit Weight, γ (pcf)	Friction Angle, Ф	Penetro-meter (psf)	SPT (Compressive Strength, Cu(psf)
0			Black, wet, top soil/stubble							
6"			Brown, damp, sandy clay till, loose							
4			Brown, moist, sandy clay till, slightly firm, some plastic							
5										
8			Brown, very moist, sandy clay till, slightly firm End of Borehole							
10										

Project Name:	Dar Ray Farms Agri Business	Park	Project #:	13-129
Hole Description:	ВН3		Bore Hole #:	3
Drilling Procedure:	Backhoe/auger		Hole Size:	6"
SPT Procedure:		SPT Size:	OD=	ID=
Sampling Procedure	Bucket/auger	Sampler Size	OD=	ID=
Logged By:	Ryan Olsen		Date:	April 4, 2014

Depth (FT)	wT	nses	Soil Sample Description	Moisture Content, w	Plasticity Index, PI	Dry Unit Weight, γ (pcf)	Friction Angle, Φ	Penetro-meter (psf)	Count, N	Compressive Strength, Cu(psf)
0			Black, wet, top soil/stubble							
6"			Medium brown, moist, sandy clay, loose							
4			Brown, moist, silty sandy clay, soft, some plastic							
5										
10			End of Borehole							

Project Name:	Dar Ray Farms Agri Business Pa	Project #:	13-129	
Hole Description:	BH4		Bore Hole #:	4
Drilling Procedure:	Backhoe/auger		Hole Size:	6"
SPT Procedure:		SPT Size:	OD=	ID=
Sampling Procedure	Bucket/auger	Sampler Size	OD=	ID=
Logged By:	Ryan Olsen		Date:	April 4, 2014

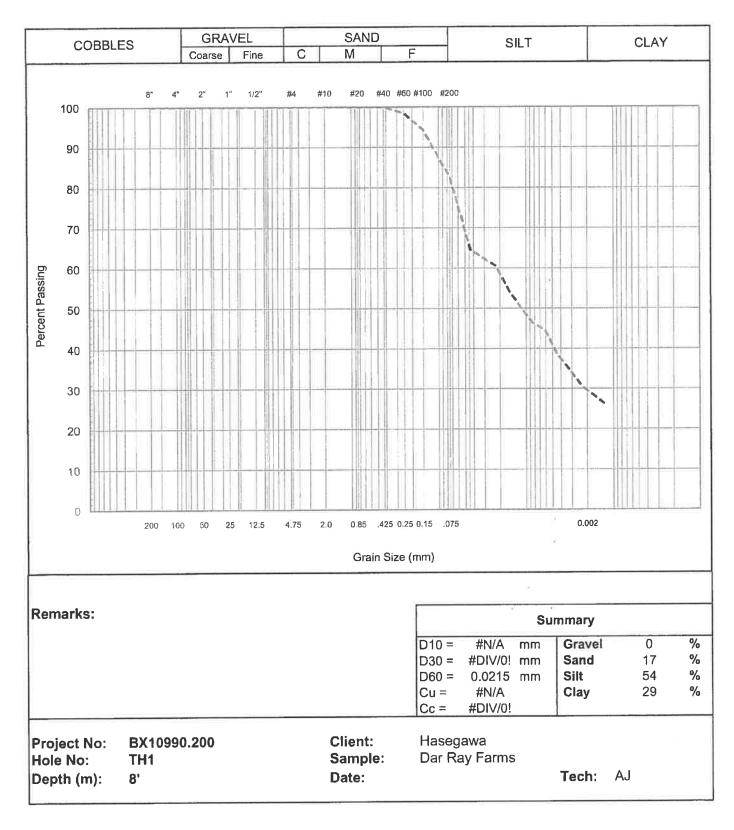
Depth (FT)	wt	nses	Soil Sample Description	Moisture Content, w	Plasticity Index, PI	Dry Unit Weight, γ (pcf)	Friction Angle, Φ	Penetro-meter (psf)	SPT	Cou N	ınt,	Compressive Strength, Cu(psf)
0			Black, wet, top soil/stubble									
6"			Brown, damp, sandy silty clay, loose									
3			Medium brown, moist, sandy clay, slightly loose									
5										_		
6			Medium brown, very moist, silty sandy clay, soft									
10			End of Borehole									
10												

MOIST	UKE	CUN	ICITI

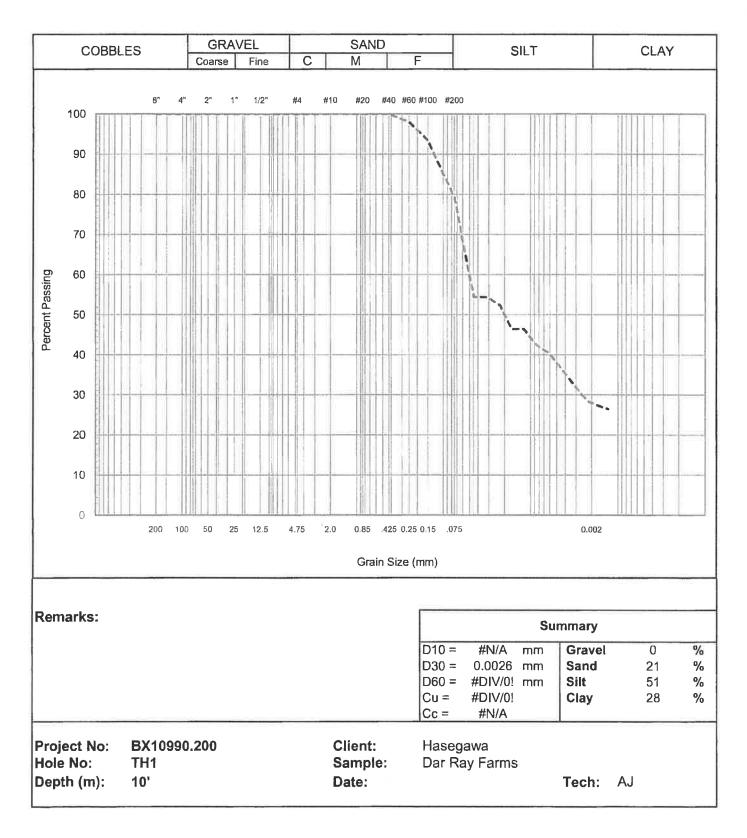
Project: Dar Ray Farms
Project #: BX10990.200
Technician: Date: 7-Apr-2014

Hole #	TH1	TH1	TH2	TH3	TH3	TH4
Depth (m)	8'	10'	6'	4'	8'	4'
Sample						
Tare No.	404.4	154.3	206.8	100.9	109.3	134.4
Vt. Semple Wet	134.1		173.8	84.2	91,3	113.7
Nt. Sample Dry	115.0	129.1		16.7	18.0	20.7
Wt. Water	19.1	25.2	33.0	- control of the cont		0.0
Tare Container	0.0	0.0	0.0	0.0	0.0	4 **
Wt. Dry sample	115.0	129.1	173.8	84.2	91.3	113,7
Molst. Content	16.6%	19.5%	19.0%	19.8%	19.7%	18.2%
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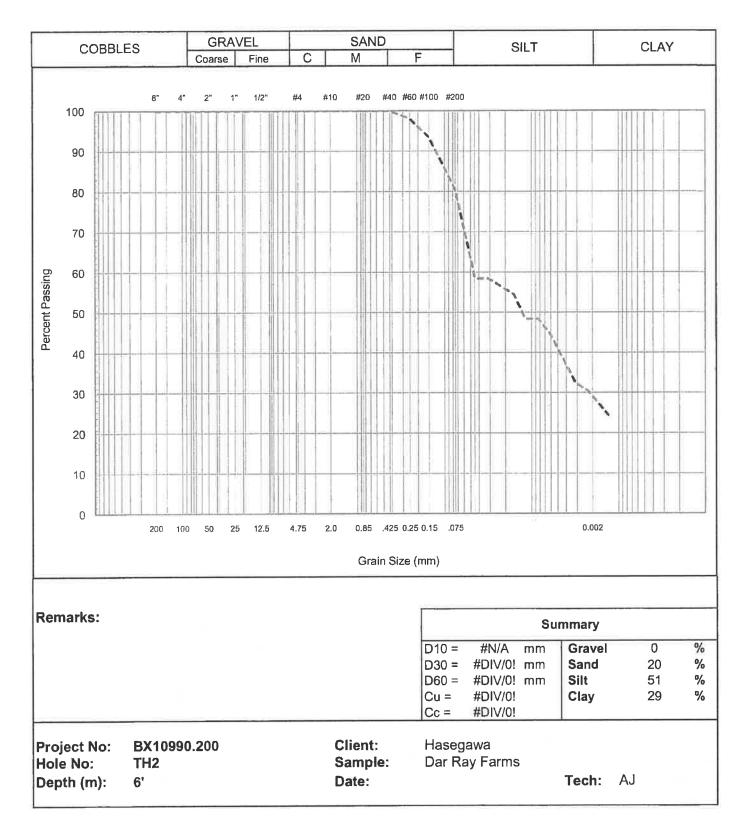




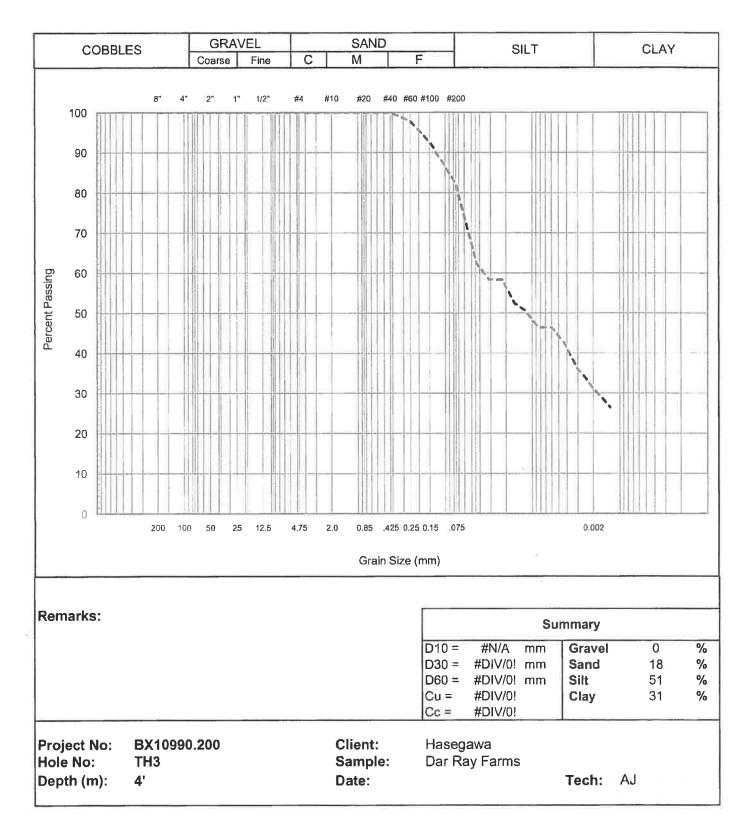




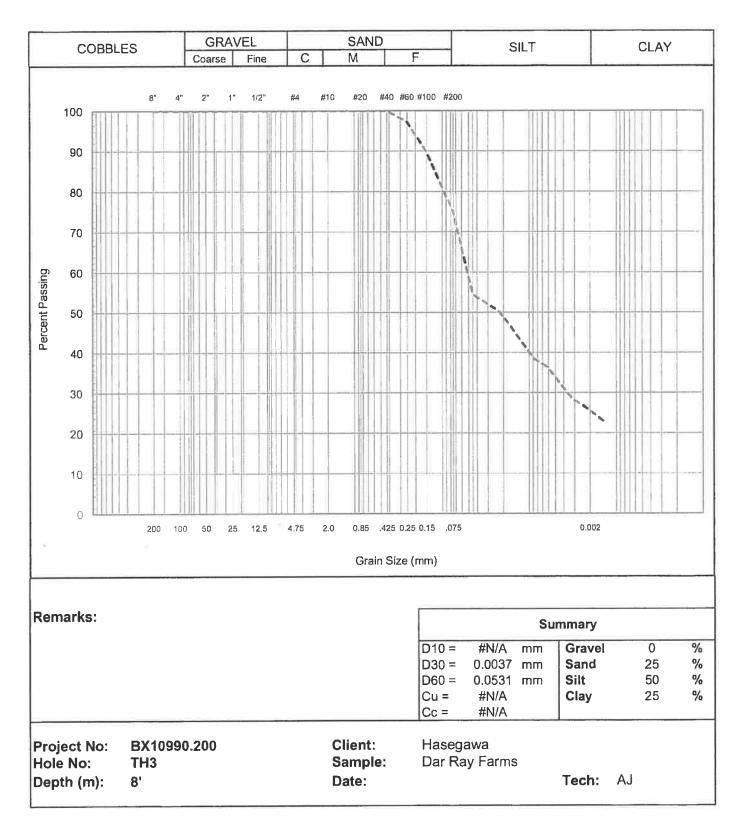




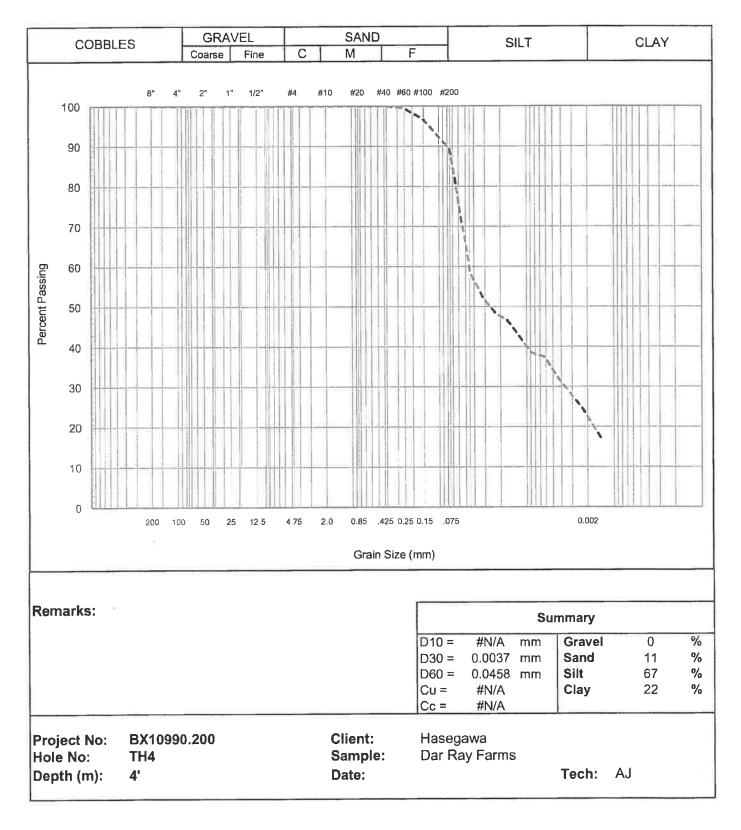














AMEC Earth & Environmental

a Division of AMEC Americas Limited 1430B, 31 Street North Lethbridge, Alberta Canada, T1H 5J8

Tel: (403) 327-7474 Fax: (403) 327-7682

Attention:

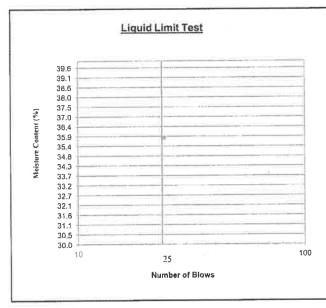
Project: Dar Ray Farms

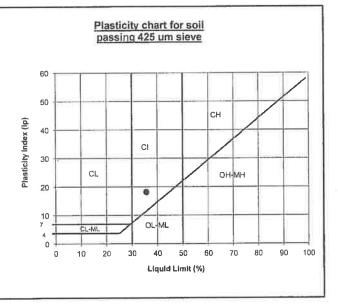
Project No: BX10990.200

Date: 10-Apr-14

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Lic	quid Limit Test	Pla	Plastic Limit Test		
# of Blows	24				
Tare #	26	Tare #	14		
Wet Wt + Tare	32.0533	Wet Wt + Tare	17.1079		
Dry Wt + Tare	27.0434	Dry Wt + Tare	16.5488		
Wt of Tare	13.0507	Wt of Tare	13.3492		
% Moisture	35.8	% Moisture	17.5		





Liquid Limit (%): 35.6 Plastic	: Limit (%):17.5	Plasticity Index:	18.2
Classification : Cl	Depth: 4'	Sample ID:	TH 3
Technician: TH			
= Input Data		Per:	



AMEC Earth & Environmental

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> Canada, T1H 5J8 Tel: (403) 327-7474 Fax: (403) 327-7682

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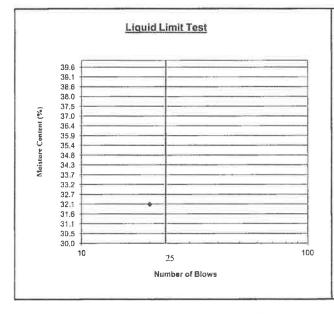
Project No: BX10990.200

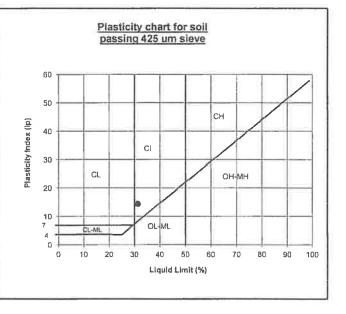
Date: 10-Apr-14

CC:

Project: Dar Ray Farms

Lie	quid Limit Test	Pla	Plastic Limit Test			
# of Blows	20					
Tare #	27	Tare #	13			
Wet Wt + Tare	37.6851	Wet Wt + Tare	16.8950			
Dry Wt + Tare	31.7585	Dry Wt + Tare	16.3739			
Wt of Tare	13.3162	Wt of Tare	13.2944			
% Moisture	32.1	% Moisture	16.9			





Liquid Limit (%): 31.3 Plas	tic Limit (%):16.9	Plasticity Index:	14.4
Classification : Cl	Depth:4'	Sample ID:	TH 4
Technician: TH			
= Input Data		Per:	

Appendix C – Traffic Impact Assessment



Lethbridge Agri-Business Park Transportation Impact Assessment

Final Report

Prepared for: Hasegawa Consulting Professional Engineers

Date: June 20, 2014

Prepared by: Bunt & Associates Engineering (Alberta) Ltd.

Permit No.: P 7694

Project No. 1283-09





June 20, 2014 1283-09

Ian Franks, P.Eng.

Hasegawa Consulting Professional Engineers 330, 3120 32nd Street South Lethbridge, AB T1K 7B4

Dear lan,

Re: Lethbridge Agri-Business Park Development - Traffic Impact Assessment

Please find attached our traffic impact assessment for the Lethbridge Agri-Business Park Development. The analysis summarized in this report was undertaken in accordance with the requirements of Alberta Transportation, and the conclusions and recommendations identify the impacts associated with the projected traffic volumes on the adjacent road network.

Please call if you have any questions or wish to discuss any issue in further detail.

Sincerely,

BUNT & ASSOCIATES

Amanda Leibel, P.Eng. Transportation Engineer ENGINE DE LA CONTRACTION DEL CONTRACTION DE LA C

PERMIT TO PRACTICE
Bust & Associates Engineering (Alberta) Ltd.

Signature

Date

JINE 20/14

PERMIT NUMBER: P 7694

The Association of Professional Engineers,
Geologists and Geophysicists of Alberta

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EXECUTIVE SUMMARY

Hasegawa Engineering is directing the development process for an Agri-Business Park located south of the City of Lethbridge in the northwest corner of the Highway 4/ Highway 508 intersection. The development consists of approximately 120 acres that will be developed as light to medium industrial land use servicing the agriculture and oilfield industries. Within the 120 acres of proposed development, approximately 10 acres are already developed with existing businesses in operation and as such the remaining 110 acres of undeveloped land will only be assessed as part of this transportation analysis.

As part of the permit application process, the County of Lethbridge (County) and Alberta Transportation (AT) required that a Transportation Impact Assessment (TIA) be completed in support of the development. Bunt & Associates was retained by Hasegawa Engineering to determine the necessary roadway improvements required to incorporate the proposed development.

Key Findings and Recommendations

The key findings and recommendations are summarized here, as follows:

Existing Traffic Conditions

All study area intersections are currently operating within the acceptable capacity parameters and study area roadways are currently functioning within their respective environmental capacities.

Bunt & Associates also completed an illumination warrant for the three study area intersections. The intersections on Highway 508 at both Highway 4 and Highway 5 warrant either partial and/or delineated lighting; however, the warrant did not determine which specific or if both types of illumination are warranted and as such it is recommended that further review is undertaken to determine the specific illumination required.

A railway crossing warrant was also completed for the Canadian Pacific rail line that runs parallel to Highway 4 and intersects Highway 508. Based on the cross product of the daily traffic volumes and the maximum number of trains expected to cross at this location, flashing warning lights are to be implemented at the rail crossing on Highway 508.

20-Year Background Traffic Conditions

The 20-year background traffic conditions exhibits the same results as under the existing traffic conditions. As such, all study area intersections and roadways are expected to operate within the acceptable capacity parameters. The intersections of Highway 508 with both Highway 4 and Highway 5 both warrant partial and/or delineation lighting. Flashing warning lights are warranted at the CP rail crossing on Highway 508 just west of Highway 4.

Proposed Development

The proposed Agri-Business Park that will service both agricultural and oil field sectors and is expected to generate 829 trips (688 inbound/ 141 outbound) during the AM peak hour and 802 trips (176 inbound/ 626 outbound) during the PM peak hour.

Post Development Traffic Conditions

Opening Day Post Development Traffic Conditions

Based on the Opening Day post development traffic conditions, Highway 508 at both Highway 5 and the realigned proposed site access requires a westbound right turn lane. The new proposed intersection at the realigned site access with Highway 508 requires a Type IV intersection treatment.

With these additions in place, the west intersection of Highway 4/ Highway 508 is expected to operate at v/c ratio of 0.93 and LOS E. It is highly unlikely that a traffic signal would be implemented at this location due to the high speed on the roadway and based on TAC signal warrant, a traffic signal is in fact not warranted.

With that said, delays will be experienced at this intersection and as such it is likely that traffic will utilize Highway 5 versus Highway 4 to access the south end of the City of Lethbridge. With only a 5-10% shift in traffic from the eastbound movements at Highway 4 to the westbound movements at Highway 5, both intersections will be expected to operate within acceptable capacity parameters.

Even with this shift in traffic, the 95th percentile queue length is expected to extend across the CP railway tracks and as such causes a safety concern. Therefore, Bunt & Associates recommends that warning gates be installed at the railway crossing to ensure safety to eastbound vehicles at this crossing. Given the low number of daily train traffic, the impact of the gates would not decrease the capacity of Highway 508 beyond what would be experienced without the gate.

Based on the road link analysis, all study area roadways are expected to operate within the environmental capacities for their specific road classification. The proposed site access is recommended to be upgraded from gravel to a paved surface.

Illumination warrant was completed for the three study area intersections along Highway 508 and under opening day post development traffic conditions, all three intersections warrant delineated lighting based on operational factors.

The railway crossing warrant was completed for the Canadian Pacific rail line that runs parallel to Highway 4 and intersects Highway 508 based on the opening day traffic conditions. Based on the cross product of the daily traffic volumes and the maximum number of trains expected to cross at this location, warning gates are warranted at the rail crossing on Highway 508. As previously stated, warning gates are also recommended to ensure the safety of vehicles what will queue beyond the railway crossing.

20-Year Post Development Traffic Conditions

The 20-year post development traffic conditions exhibited much the same results as the Opening Day traffic conditions. The new proposed intersection at the realigned site access with Highway 508 warrants a Type IV intersection treatment.

The west intersection of Highway 4/ Highway 508 will continue to operate at v/c ratio of 0.94 and LOS E. Based on TAC signal warrant analysis, a traffic signal is not warranted. However, some delays will be experienced at the intersection and as such it is likely that some non-captive traffic will shift to Highway 5 from Highway 4 to access the south end of the City of Lethbridge. With only a 5-10% shift in traffic from the eastbound movements at Highway 4 to the westbound movements at Highway 5, both intersections are expected to operate within acceptable capacity parameters. Again, even with the shift in traffic, the 95th percentile queue length is expected to extend across the CP railway tracks and as such causes a safety concern. Therefore, Bunt & Associates recommends that warning gates be installed at the railway crossing at the Opening Day to ensure safety of vehicles at this crossing.

Based on the road link analysis, all study area roadways are expected to operate within the environmental capacities for their specific road classification assuming the proposed access has been upgraded to a paved surface based on the Opening Day traffic conditions.

Once again, an illumination warrant was completed for the three study area intersections along Highway 508 and under opening day post development traffic conditions, all three intersections warrant delineated lighting based on operational factors.

The railway crossing warrant was again completed for the Canadian Pacific rail line that runs parallel to Highway 4 and intersects Highway 508 based on the opening day traffic conditions. Based on the cross product of the daily traffic volumes and the maximum number of trains expected to cross at this location, warning gates are warranted at the rail crossing on Highway 508. As previously stated, warning gates are recommended to ensure the safety of vehicles what will queue beyond the railway crossing.

Summary

The proposed Agri-Business Park is anticipated to add a significant amount of traffic to the surrounding road network resulting in road network improvements at each horizon year. With that said **Table E.1** summarizes the improvements required to accommodate the proposed site generated traffic volumes as discussed above.

Table E.1 Summary of Road Network Improvements

Horizon Year		Recommended I	Recommended Intersection Improvements		
Traffic Conditions	Highway 508/ Highway 4 (west intersection)	Highway 508/ Highway 4 (east intersection)	Highway 508/ Highway 5	Highway 508/ Site Access	Highway 508 CP Rail Crossing
Existing	 No intersection improvements required Partial and/or delineated illumination is warranted 	 No intersection improvements required Partial and/or delineated illumination is warranted 	 No improvements are required 	 No improvements are required 	 Flashing warning lights are warranted
20-Year Background	 No intersection improvements required Partial and/or delineated illumination is warranted 	 No intersection improvements required Partial and/or delineated illumination is warranted 	 No improvements are required 	 No improvements are required 	 Flashing warning lights are warranted
Opening Day Post Development	 Eastbound movement does not operate within acceptable capacity parameters; however a traffic signal is not warranted. Traffic may utilize alternate route of Hwy 5 to avoid congestion at Hwy 4, thus a 5-10% shift in traffic will bring the intersection within acceptable parameters. The queue length extends beyond the rail line and as such warning gates are to be implemented based on the warrant and for safety reasons. Delineation illumination is warranted 	 No intersection improvements required Delineation illumination is warranted 	Westbound right turn lane required Delineation illumination is warranted	 Type IV intersection treatment required Westbound right turn lane required Site access roadway requires a paved surface Delineation is warranted 	Rail Crossing Cates are warranted

Table E.1 Summary of Road Network Improvements - Continued

	Highway 508 CP Rail Crossing	Rail Crossing Gates are warranted
	Highway 508/ Site Access	 Type IV intersection treatment required Westbound right turn lane required Site access roadway requires a paved surface Delineation is warranted
Recommended Intersection Improvements	Highway 508/ Highway 5	Westbound right turn lane required Delineation illumination is warranted
Recommended Inte	Highway 508/ Highway 4 (east intersection)	 No intersection improvements required Delineation illumination is warranted
	Highway 508/ Highway 4 (west intersection)	 Eastbound movement does not operate within acceptable capacity parameters; however a traffic signal is not warranted. Traffic may utilize alternate route of Hwy 5 to avoid congestion at Hwy 4 and thus a 5-10% shift in traffic will bring the intersection within acceptable parameters. The queue length extends beyond the rail line and as such warning gates are to be implemented based on the warrant and for safety reasons. Delineation illumination is warranted
Horizon Year	Traffic Conditions	20-Year Post Development



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1. INTRODUCTION

1.1 Background

Hasegawa Engineering is directing the development process for an Agri-Business Park located south of the City of Lethbridge in the northwest corner of the Highway 4/ Highway 508 intersection. The development consists of approximately 120 acres that will be developed as light to medium industrial land use servicing the agriculture and oilfield industries. Within the 120 acres of proposed development, approximately 10 acres is already developed with existing businesses in operation and as such the remaining 110 acres of undeveloped land will only be assessed as part of transportation analysis.

As part of the permit application process, the County of Lethbridge and Alberta Transportation (AT) required that a Transportation Impact Assessment (TIA) be completed in support of the development. The primary objective of the assessment was to confirm that the development could be supported by the existing infrastructure and to determine if any improvements are required. Bunt & Associates was retained by Hasegawa Engineering to determine the necessary roadway improvements required to incorporate the proposed development.

1.2 Study Objectives

The following scope of work for the assessment was agreed upon in discussion with Alberta Transportation:

- Conduct intersection capacity analysis for the AM and PM peak hour for the existing traffic conditions
 at the current access with Highway 508. The intersections of Highway 508 with both Highway 4 and
 Highway 5 will also be analyzed; however the traffic counts from Alberta Transportation's website will
 be utilized.
- Conduct intersection capacity analysis for the AM and PM peak hour for the 20-year horizon traffic conditions at the following intersections:
 - o Highway 508/ Highway 4
 - o Highway 508/ Highway 5
 - o Highway 508/ Future Access
- Develop trip generation forecasts for the proposed development.
- Develop distribution patterns for the site based on a combination of review of the existing
 distribution of the on-site businesses, the anticipated market draw for the area as well as travel times
 completed on site.

- Analyse the study area intersections to confirm operating conditions and the lane requirements for the existing, Opening Day and 20-year horizon post-development traffic conditions.
- Complete an illumination warrant for the intersections of Highway 508/ Highway 4 and Highway 508/
 Highway 5 for the existing, Opening Day and 20-year horizons.
- Complete a railway crossing warrant for the intersection of Highway 508/ Highway 4 for the existing, Opening Day and 20-year horizons.
- Review daily traffic volumes on Highway 4, Highway 5 and Highway 508 for existing, Opening Day and 20-Year background and post development traffic conditions.

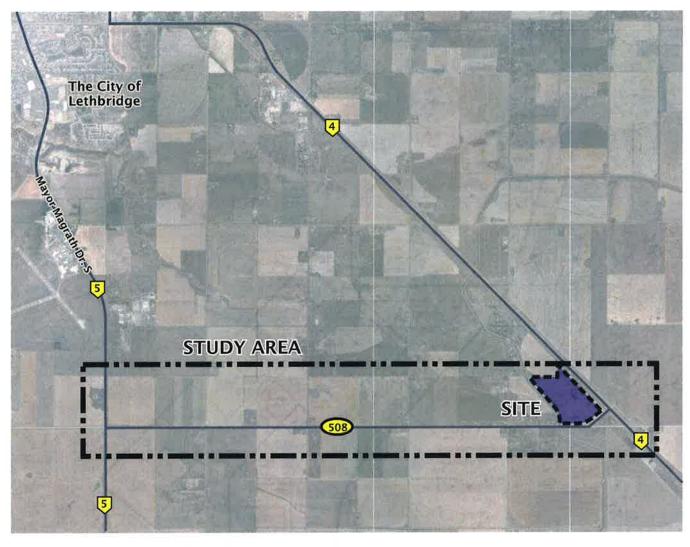
The approved scope and correspondence with Alberta Transportation is attached in Appendix A.

1.3 Subject Site Description

The proposed site is located west south of the City of Lethbridge on the west side of Highway 4 and north of Highway 508. The development includes approximately 120 acres of light to medium industrial uses, which are anticipated to service the agricultural and oilfield sectors. There is approximately 10 acres of land, which are already occupied by existing buildings and as such only 110 acres will be analyzed as part of the proposed future development.

The subject site and surrounding area is illustrated in **Exhibit 1.1.** Access to the site will be provided at one intersection along Highway 508. The proposed site plan is shown in **Exhibit 1.2.**





Base Map Source: Google Maps

Subject Site & Surrounding Area

Lethbridge Agri-Business Park June 2014 Scale NTS





Base Map Source: Hasegawa Consulting Professional Engineers

LEGEND

EXISTING PROPERTY LINES

PROPOSED LOTS

FUTURE DEVELOPMENT

Exhibit 1.2 Proposed Site

Lethbridge Agri-Business Park June 2014 Scale NTS



EXISTING TRAFFIC CONDITIONS

2.1 Study Area Road Network

The adjacent road network within the vicinity of the subject site is as follows:

Highway 4 is a four-lane divided highway within the vicinity of the site, which runs in the north-south direction on the east side of the site. Highway 4 intersects with Highway 508 at an unsignalized intersection and exhibits left and right turn bays in both the north and south directions, thus exhibiting a Type IV intersection treatment. The posted speed limit is 110 km/hr. There is also a Canadian Pacific Railway line that runs adjacent to the highway within the vicinity of the site. Highway 4 within the vicinity of the site is currently carrying approximately 6,200 vehicles per day (vpd).

Highway 5 is a two lane undivided highway, which runs in the north-south direction. This road intersects with Highway 508 at an unsignalized intersection and exhibits a southbound left turn lane and a northbound right turn lane, which reflects a Type IV intersection treatment. The posted speed limit is 100 km/hr. Highway 5 is currently carrying approximately 5,400 vpd in the vicinity of the proposed site.

Highway 508 is a two-lane undivided highway, which runs in the east-west direction. The road provides a connection to the proposed site from both the east and the west side. The posted speed limit is 100 km/hr, with a speed reduction to 85 km/hr through the horizontal curve adjacent to the site and reduces further to 45 km/hr at the railway crossing. Highway 508 is currently carrying approximately 400 vpd within the vicinity of the proposed site.

Existing Access is a two-lane gravel local roadway, which runs in the north-south direction. The existing access is located on the horizontal curve located prior to the Highway 4 intersection and exhibits a Type I intersection treatment. Based on discussions with Alberta Transportation it was recommended that the access is moved further west along the tangent of the curve and as close to the canal as possible. As such, the client has relocated the access in the proposed plans for the future development.

The existing lane configurations and traffic control arrangements within the study area are summarized in **Exhibit 2.1.**

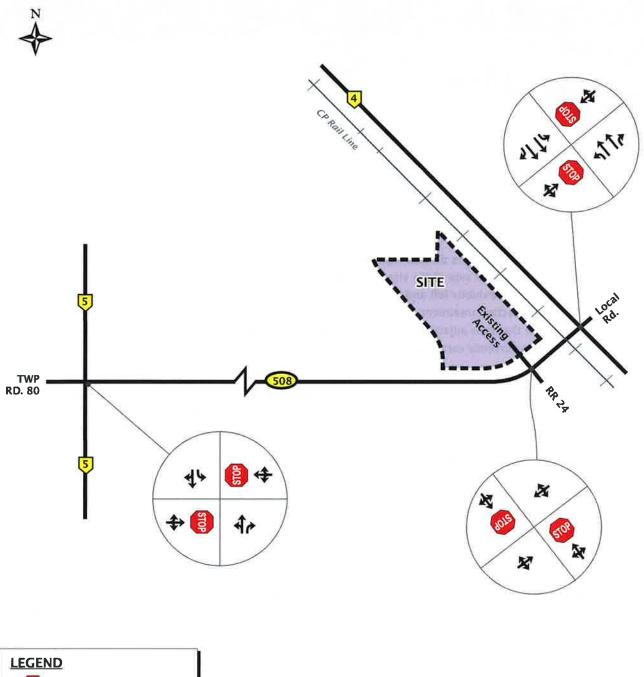




Exhibit 2.1 **Existing Lane Configuration & Traffic Controls**

Lethbridge Agri-Business Park June 2014 Scale NTS



2.2 Existing Traffic Volumes

2.2.1 Traffic Volumes

Bunt & Associates conducted obtained the traffic count information from the Alberta Transportation website for the intersections of Highway 508/ Highway 4 and Highway 508/ Highway 5. A manual intersection turning movement counts for both the AM and PM peak periods was completed at the Highway 508/ existing access intersection for the turning movements only on Tuesday, May 20th, 2014, The through volumes at the intersection were determined based on the traffic count at Highway 508/ Highway 4.

The existing turning movement volumes are shown in **Exhibit 2.2.** The raw count data is included in **Appendix B.**

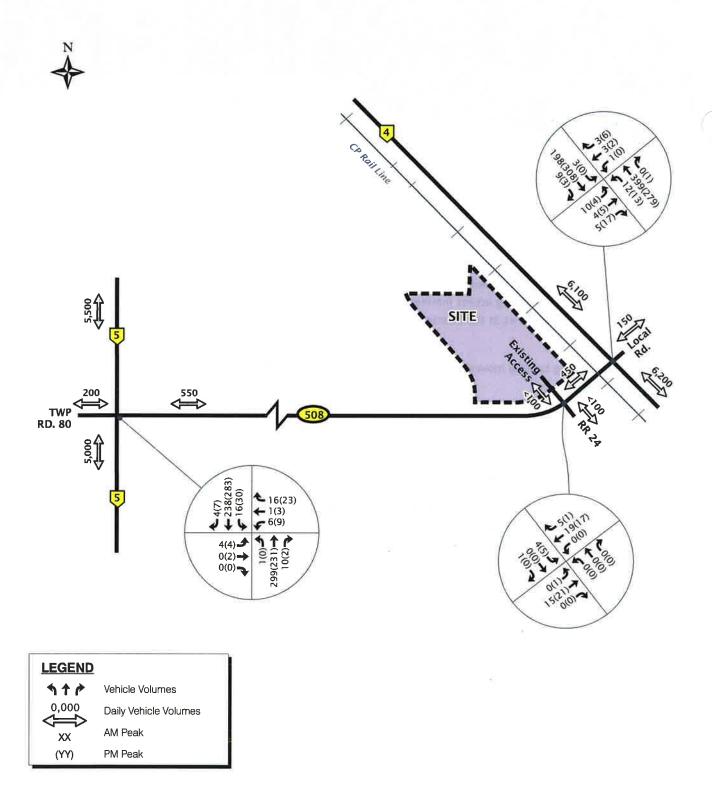
2.2.2 Intersection Capacity Analysis

To evaluate the existing traffic operation conditions during the peak hour periods, an intersection capacity analysis was undertaken for the study area intersections using Synchro 8.0, a traffic analysis software package based on the methods outlined in the Highway Capacity Manual.

Individual critical movements are assessed based on proportion of utilized capacity (a volume to capacity or v/c ratio) and on delay (the level of service or LOS). In general terms, a v/c of 0.90 or less is acceptable, as is a LOS of D or better, which represents optimized conditions. If the volume-to-capacity ratios are greater than 0.90 or the movements have LOS values of D, E or F, then intersection/road improvements may be warranted. With respect to delay, a Level of Service of "A" represents minimal delay, and a LOS of "F" represents significant delay to the critical movement.

The results for the existing intersection capacity analysis are summarized in **Table 2.1**; the existing lane configurations and traffic control arrangements were applied. Additionally, the analysis followed the methodologies and incorporated the traffic factors as outlined by the Alberta Transportation TIA Guidelines and Synchro parameters are based on the City of Lethbridge TIA Guidelines due to the close proximity to the City.

The Synchro output summaries are included in Appendix C.



Existing Traffic Volumes

Lethbridge Agri-Business Park June 2014 Scale NTS



Table 2.1: Existing Intersection Capacity Analysis

		AM Peak				PM Peak			
Intersection	Movement	v/c	LOS	Delay (s)	Queue (m)	v/c	LOS	Delay (s)	Queue (m)
	EBT	0.02	В	10.2	0.6	0.02	В	10.2	0.6
	EBR	0.02	В	10.2	0.6	0.02	В	10.2	0.6
Highway 508/Highway 4	WBL/T	0.03	В	10.6	0.7	0.03	В	11.5	0.7
(west intersection)	SBL	< 0.01	A	7.3	0.1	< 0.01	A	0.0	0.0
	SBT	0.07	Α	0.0	0.0	0.10	Α	0.0	0.0
	SBR	0.01	A	0.0	0.0	< 0.01	Α	0.0	0.0
	EBL/T	0.03	В	11.6	0.9	0.02	В	10.9	0.4
Highway 508/Highway 4 (east intersection)	WBT/R	0.01	В	11.5	0.3	0.01	A	9.8	0.3
	NBL	0.01	Α	7.3	0.2	0.01	Α	7.4	0.2
	NBT	0.13	A	0.0	0.0	0.09	A	0.0	0.0
	NBR	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0
notice the second review	EB	< 0.01	A	0.0	0.0	< 0.01	Α	0.3	0.0
	WB	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0
Highway 508/Existing Access	NB	< 0.01	Α	0.0	0.0	< 0.01	A	0.0	0.0
	SB	0.01	Α	8.8	0.1	0.01	Α	8.9	0.1
	EB EB	0.01	С	15.3	0.3	0.02	C	15.5	0.5
	WB	0.05	В	11.9	1.2	0.07	В	11.9	1.8
	NBL/T	< 0.01	Α	0.0	0.0	< 0.01	A	0.0	0.0
Highway 508/Highway 5	NBR	0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0
	SBL	0.02	A	8.1	0.4	0.03	A	7.9	0.6
- Igi Diigil somerifes (1'-b)	SBT/R	0.16	Α	0.0	0.0	0.19	Α	0.0	0.0

As shown in Table 2.1, the results indicated that all study area intersections are currently operating within acceptable capacity parameters, therefore no improvements are required to accommodate the existing traffic volumes.

2.2.3 Illumination Warrant

Bunt & Associates undertook an illumination warrant for the three existing intersections based on the Transportation Association of Canada (TAC) methodology for Illumination of Isolated Rural Intersections¹. The illumination warrant review the geometric, operational, environmental and collision factors for the study area intersections. Illumination is warranted based on the following criteria:

- Total Points ≥ 240 points: Full illumination is warranted
- 120 ≤ Total Points < 240: Partial and/or delineation lighting warranted:
 - o if Geometric Factors Subtotal ≥ 80 points: partial lighting to illuminate key decision areas, potential conflict points, and/or hazards,
 - o if Operational Factors Subtotal ≥ 120 points: delineation lighting to illuminate pedestrians or cross street traffic,
 - if Collision History Subtotal = 120 points: review collisions to determine appropriate lighting strategy.
- < 120 Points: Illumination is not warranted</p>

Based on Bunt & Associates site visit along with traffic data and collision data from Alberta Transportation, the illumination warrants were completed based on the above criteria.

Highway 508/ Highway 4

Based on the illumination warrant under existing traffic conditions, the intersection of Highway 508/ Highway 4 scored 156 points. As a result, the intersection warrants partial and/or delineation lighting; however the individual criteria for geometric, operational and collision history are not met to determine whether partial and/or delineated lighting is warranted. As such, it is recommended that the intersection is reviewed and that partial and/or delineated lighting is implemented.

Highway 508/ Highway 5

Based on the illumination warrant under existing traffic conditions, the intersection of Highway 508/ Highway 4 scored 131 points. As a result, the intersection warrants partial and/or delineation lighting; however the individual criteria for geometric, operational and collision history are not met to determine whether partial and/or delineated lighting is warranted. As such, it is recommended that the intersection is reviewed and that either partial and/or delineated lighting is implemented.

¹ Illumination of Isolated Rural Intersections, Transportation Association of Canada (TAC), February 2001.

Highway 508/ Existing Access

Based on the illumination warrant under existing traffic conditions, the intersection of Highway 508/ Highway 4 scored 46 points. As a result, no illumination is warranted at the intersection.

The illumination warrant summaries are included in Appendix D.

2.2.4 Rail Crossing Warrant

The Canadian Pacific (CP) Railway has a line that runs adjacent to Highway 4 on the west side. Based on information obtained from CP, this rail line is considered to be a part of the main line, which has unscheduled traffic but has an estimated frequency of 3 to 8 fright trains per 24-hour period and can be expected any time during the day or night. A typical train is 125 railcars in length with 2-4 engines and operates at a speed of 55 km/h (35mph) along this section of track.

Rail/road crossings are classified as either grade-separated or at-grade; and at-grade rail/road crossings can be further classified into two separate categories, passive or active. A review of the existing conditions confirmed that the Highway 508 at-grade rail/road crossings exhibit passive control (i.e., no warning signal or gate arms).

A review of Transport Canada's² requirements for rail crossings determines that lights are required at a rail crossing when the forecast cross product³ is 1,000 or more and gates are required when the forecast cross product is 50,000 or more. The cross product for the crossing at Highway 508 is 3,600⁴, therefore, warning lights are warranted as the cross product is greater than 1,000 based on existing conditions at the Highway 508 crossing.

2.2.5 Stopping Sight Distance

Bunt & Associates completed a stopping sight distance (SSD) review based on Alberta Transportation's Highway Geometric Design Guide. The minimum stopping sight distance is the length of roadway ahead visible to the driver. The minimum sight distance available on a roadway should allow a vehicle to stop prior to reaching a fixed object such as a stop sign when travelling at an assumed speed, which is based on the design speed of the roadway.

² RTD 10 Road/Railway Grade Crossings Technical Standards and Inspection, Testing and Maintenance Requirements, Transport Canada, March 2002.

³ Forecast cross product = number of trains per day * daily traffic volume on the roadway

⁴ The cross product was calculated on the maximum number of expected trains per day (8 trains per day) to utilize the most conservative estimate.

Highway 4

The posted speed limit on Highway 4 is 110 km/hr and as such the design speed is likely 120 km/hr, which requires a minimum SSD of 270 metres. Based on Bunt & Associates site visit, the minimum stopping sight distance was observed at greater than 500 metres in both the north and south directions at the intersection with Highway 508. As such, the minimum stopping sight distance is achieved and therefore no improvements are required at this time.

Highway 508

The posted speed limit on Highway 508 as it approaches is 45 km/h due to the railway crossing which, is approximately 35-40 metres from the intersection with Highway 4. Based on a design speed of 50-60 km/hr, the minimum SSD is 65-85 metres. Based on Bunt & Associates site visit, the minimum stopping sight distance was observed at greater than 100 metres in the eastbound direction at the intersection with Highway 4. As such, the minimum stopping sight distance is achieved and therefore no improvements are required at this time.

The posted speed limit on Highway 508 in the vicinity of Highway 5 is 100 km/hr and as such the design speed is likely 110 km/hr which requires a minimum SSD of 235 metres. Based on Bunt & Associates site visit, the minimum stopping sight distance was observed at greater than 500 metres in both the east and west directions at the intersection with Highway 5. As such, the minimum stopping sight distance is achieved and therefore no improvements are required at this time.

The intersection of Highway 508 at the existing access has a posted speed limit of 85km/hr due to the horizontal curve within the vicinity of the access location. The minimum SSD for a design speed of 90-100km/hr which is typical for a 85km/h posted speed limit is 170 – 200 metres. Again, based on Bunt & Associates site visit, the minimum stopping sight distance was observed at greater than 200 metres in both the east and west directions at the intersection of Highway 508 and the existing access. As such, the minimum stopping sight distance is achieved and therefore no improvements are required at this time.

Highway 5

The posted speed limit on Highway 5 is 100 km/hr and as such the design speed is likely 110 km/hr., which requires a minimum SSD of 235 metres. Based on Bunt & Associates site visit, the minimum stopping sight distance was observed at greater than 500 metres in both the north and south directions at the intersection with Highway 508. As such, the minimum stopping sight distance is achieved and therefore no improvements are required at this time.

2.2.6 Road Link Analysis

The existing link volumes were assessed based on typical Alberta Transportation highway standards. In general terms, this analysis was intended to assess the daily traffic volumes on all germane roadway links in the study area and to confirm the current roadway classification and/or identify any need for reclassification based solely on existing traffic. The results of the assessment are summarized in **Table 2.2**.

Table 2.2: Existing Road Link Analysis

Road Link	Road Classification	Recommended Daily Traffic Volume (vehicles per day)	Existing Daily Traffic Volume ^s (vehicles per day)
Highway 4	4-lane Primary Highway	> 12,000	6,200
Highway 508	2-lane Secondary Highway	< 12,000	450 - 550
Highway 5	2-lane Primary Highway	< 12,000	5,500
Existing Access	Rural Local Road (gravel)	< 500	< 100

Based on the road link analysis, all of the road links within the vicinity of the site are within the recommended daily traffic volume design guidelines for the various classifications of roadways.

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⁵ Traffic volumes are rounded to the nearest 100 for volumes greater than 1,000 vpd and to the nearest 10 for volumes less than 1,000vpd.



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20-YEAR BACKGROUND TRAFFIC CONDITIONS

3.1 Study Area Road Network

The adjacent road network within the vicinity of the subject site at the 20-Year horizon is anticipated to remain the same as under existing conditions with the exception of the proposed access shifting to the west as previously discussed.

3.2 20-Year Horizon Traffic Volumes

3.2.1 Forecast Traffic Volumes

Bunt & Associates determined the 20-year target forecast traffic volumes based on the highway growth that has occurred over the last 5 years based on the traffic counts from the AT website. Based on that information, Highway 4 has an average of 2.01% yearly growth over the last five years and thus a 2% yearly linear growth rate was applied. Hwy 5 yearly data only increased in 2012 over the last five years when an update count was completed and as such had a large increase of roughly 13% with no growth in the other previous years. As such an average of 3.44% was found over the last five years. Therefore a linear growth rate of 3.5% was applied on Highway 5. It should be noted that this growth rate is higher than the typical growth rate that Alberta Transportation applies (2.5% is typical) on most highways and ambient traffic likely cannot increase as much as 3.5%; however since this is the observed increase Bunt & Associates chose to use the 3.5% and thus through traffic on Highway 5 is likely on the conservative side. Highway 508 showed a yearly growth rate of 0.46% over the last year; however Bunt feels it is prudent to utilize a more conservative growth rate of 2% per year on Highway 508.

The 20-year horizon forecast background traffic turning movement volumes are shown in **Exhibit 3.1**. The background traffic growth calculations are included in **Appendix E**.

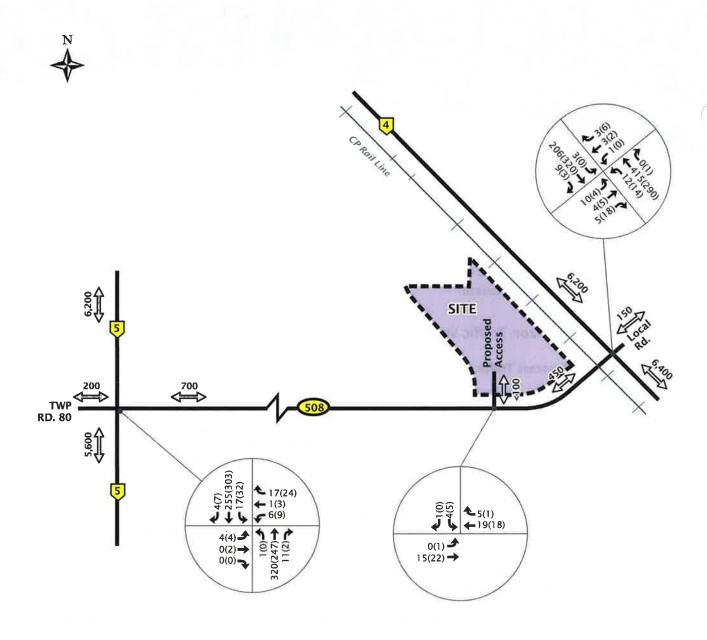
3.2.2 Intersection Treatment Type

The Alberta Transportation Intersection Treatment type was determined for Highway 508 at both the realigned proposed site access and at Highway 5.

Highway 508 at Realigned Proposed Site Access

Left Turn Lane Warrant

Based on the Alberta Transportation Highway Geometric Design Guide, the warrant for left turns lanes on a two-lane highway determines the intersection treatment type that should be applied.



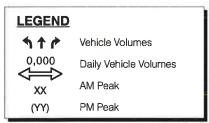


Exhibit 3.1
20 Year Background Traffic Volumes

Lethbridge Agri-Business Park June 2014 Scale NTS



Utilizing the 20-year background traffic volumes at the intersection of Highway 508 and the realigned proposed site access, the PM peak hour traffic volumes are the worst case scenario and as such were the traffic volumes used for this analysis. The volume of left turn vehicles is 1 vph, the approaching volume is 23 vph, resulting in 4% left turn vehicles in the approaching volume and the opposing traffic is 19 vph. Based on D-7.6-7a with a design speed of 110 km/hr on Highway 508, a Type I intersection is warranted.

Right Turn Lane Warrant

An exclusive right turn lane is warranted when all of the following criteria are met:

- Main (or through) road AADT ≥ 1800
- Intersecting road AADT ≥ 900, and
- Right turn daily traffic volume ≥ 360 for the movement in question

Based on the above criteria a right turn lane is not warranted for the westbound direction as the main road AADT is 450 vpd, the intersecting road AADT is less than 100 and the right turn lane volume is 10 vpd.

Highway 508 at Highway 5

Left Turn Lane Warrant

Utilizing the 20-year background traffic volumes on Highway 508 at the intersection with Highway 5, the AM peak hour traffic volumes are the worst case scenario and as such were the traffic volumes used for this analysis. The volume of left turn vehicles is 6 vph, the approaching volume is 24 vph, resulting in 25% left turn vehicles in the approaching volume and the opposing traffic is 4 vph. Based on D-7.6-7c with a design speed of 110 km/hr on Highway 508, a Type I intersection is warranted.

Right Turn Lane Warrant

Based on the right turn lane warrant stated earlier, a right turn lane is not warranted for the westbound direction on Highway 508 at Highway 5 as the main road AADT is 6,200 vpd, the intersecting road AADT is 700 vpd and the right turn lane volume is 240 vpd.

3.2.3 Intersection Capacity Analysis

To evaluate the 20-year horizon total background traffic operation conditions during the peak hour periods, an intersection capacity analysis was undertaken for the study area intersections using Synchro 8.0, a traffic analysis software package based on the methods outlined in the Highway Capacity Manual.

The results for the 20-year horizon background intersection capacity analysis are summarized in **Table 3.1**. The analysis was based on the existing intersection lane configurations with the shifted access point and traffic controls. Additionally, the analysis followed the methodologies and incorporated the traffic factors as outlined by the Alberta Transportation TIA Guidelines and Synchro parameters are based on the City of Lethbridge TIA Guidelines due to the close proximity to the City.

The Synchro output summaries are included in Appendix C.

Table 3.1: 20-Year Total Background Intersection Capacity Analysis

		AM Peak			PM Peak				
Intersection	Movement	v/c	LOS	Delay (s)	Queue (m)	v/c	LOS	Delay (s)	Queue (m)
	EBT	0.02	В	10.2	0.6	0.02	В	10.2	0.6
Highway 508/Highway 4 (west intersection)	EBR	0.02	В	10.2	0.6	0.02	В	10.2	0.6
	WBL/T	0.03	В	10.7	0.7	0.03	В	11.6	0.8
	SBL	< 0.01	Α	7.3	0.1	< 0.01	Α	0.0	0.0
	SBT	0.07	Α	0.0	0.0	0.11	Α	0.0	0.0
	SBR	0.01	Α	0.0	0.0	< 0.01	A	0.0	0.0
	EBL/T	0.03	В	11.7	0.9	0.02	В	11.0	0.4
Highway 508/Highway 4 (east intersection)	WBT/R	0.01	В	11.6	0.3	0.01	A	9.8	0.3
	NBL	0.01	Α	7.3	0.2	0.01	Α	7.4	0.3
	NBT	0.14	A	0.0	0.0	0.10	A	0.0	0.0
	NBR	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0
	EB	< 0.01	Α	0.0	0.0	< 0.01	Α	0.3	0.0
Highway 508/ Future Realigned Access	WB	0.02	Α	0.0	0.0	0.01	Α	0.0	0.0
ruture Realigned Access	SB	0.01	Α	8.8	0.1	0.01	Α	8.9	0.1
	EB	0.01	С	16.1	0.3	0.02	С	16.3	0.5
	WB	0.05	8	12.2	1.3	0.08	8	12.2	2.0
	NBL/T	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0
Highway 508/Highway 5	NBR	0.01	Α	0.0	0.0	< 0.01	A	0.0	0.0
	SBL	0.02	Α	8.2	0.4	0.03	Α	7.9	0.7
	SBT/R	0.17	Α	0.0	0.0	0.21	Α	0.0	0.0

As shown in Table 3.1, the results indicated that all study area intersections continue to operate within acceptable capacity parameters based on the increase in traffic for the 20-year background traffic volumes; as such no improvements are required to accommodate the 20-year background traffic volumes.

3.2.4 Illumination Warrant

Once again, Bunt & Associates undertook an illumination warrant for the three existing intersections based on the Transportation Association of Canada (TAC) methodology for Illumination of Isolated Rural Intersections⁶ utilizing the 20-year background traffic volumes. The illumination warrant again reviewed the geometric, operational, environmental and collision factors for the study area intersections.

Highway 508/ Highway 4

Based on the illumination warrant under 20-year background traffic conditions, the intersection of Highway 508/ Highway 4 continued to score 156 points based on the 20-year background traffic volumes. One again as a result, the intersection warrants partial and/or delineation lighting; however the individual criteria for geometric, operational and collision history are not met to determine whether partial and/or delineated lighting is warranted. As such, it is recommended that the intersection is reviewed and that partial and/or delineated lighting is implemented.

Highway 508/ Highway 5

Based on the illumination warrant under 20-year background traffic conditions, the intersection of Highway 508/ Highway 4 continues to score 131 points based on the 20-year background traffic volumes. Once again as a result, the intersection warrants partial and/or delineation lighting; however the individual criteria for geometric, operational and collision history are not met to determine whether partial and/or delineated lighting is warranted. As such, it is recommended that the intersection is reviewed and that partial and/or delineated lighting is implemented.

Highway 508/ Existing Access

Based on the illumination warrant under 20-year background traffic conditions, the intersection of Highway 508/ Highway 4 scored 46 points based on the 20-year background traffic volumes. As a result, no illumination is warranted at the intersection.

The 20-year background traffic illumination warrant summaries are included in Appendix D.

3.2.5 Rail Crossing Warrant

The rail crossing warrant was once again completed based on the 20-year background traffic volumes. Again, Transport Canada's⁷ requirements for rail crossings determines that lights are required at a rail crossing when the forecast cross-product⁸ is 1,000 or more and gates are required when the forecast cross product is 50,000 or more. The cross product for the crossing at Highway 508 remains at 3,600° based on

fillumination of Isolated Rural Intersections, Transportation Association of Canada (TAC), February 2001.

⁷ RTD 10 Road/Railway Grade Crossings Technical Standards and Inspection, Testing and Maintenance Requirements, Transport Canada, March 2002.

⁸ Forecast cross product = number of trains per day * daily traffic volume on the roadway

⁹ The cross product was calculated on the maximum number of expected trains per day (8 trains per day) to utilize the most conservative estimate.

the 20-year background traffic volumes, thus once again warning lights continue to be warranted as the cross product remains greater than 1,000 based on the 20-year background traffic conditions at the Highway 508 crossing.

3.2.6 Road Link Analysis

The 20-year background link volumes were assessed based on typical Alberta Transportation highway standards. In general terms, this analysis was intended to assess the daily traffic volumes on all germane roadway links in the study area and to confirm the current roadway classification and/or identify any need for reclassification based solely on background traffic. The results of the assessment are summarized in **Table 3.2** and also illustrated previously on Exhibit 3.1.

Table 3.2: 20-Year Background Road Link Analysis

Road Link	Road Classification	Recommended Daily Traffic Volume (vehicles per day)	20-Year Background Daily Traffic Volume ¹⁰ (vehicles per day)
Highway 4	4-lane Primary Highway	> 12,000	6,400
Highway 508	2-lane Secondary Highway	< 12,000	450 - 700
Highway 5	2-lane Primary Highway	< 12,000	6,200
Re-aligned Access	Rural Local Road (gravel)	< 500	< 100

Based on the road link analysis, all of the road links within the vicinity of the site are within the recommended daily traffic volume design guidelines for the various classifications of roadways.

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¹⁰ For the purpose of this study, the daily traffic volumes estimates were based on ten times the PM peak hour volumes. Again rounding took place as under existing traffic conditions.

4. SITE TRAFFIC VOLUMES

4.1 Proposed Land Use

The proposed development concept is expected to contain approximately 120 acres that will be developed as light to medium industrial land use servicing the agriculture and oilfield industries. Within the 120 acres of proposed development, approximately 10 acres is already developed with existing businesses in operation and as such the remaining 110 acres of undeveloped land will only be assessed as part of the transportation analysis.

The development will have one access location as previously discussed; the existing access will be shifted to the west along the tangent on the curve closer to the canal crossing.

4.2 Site Traffic Generation

The trip generation rates used in this study were sourced from the Institute of Transportation Engineers (ITE) Trip Generation Handbook, 8th Edition Land Use Code 110, General Light Industrial. The AM Peak hour trip rate utilized was 7.51 trips / acre (83% inbound/ 17% outbound) while the PM peak hour rate utilized was 7.26 trips / acre (22% inbound/ 78% outbound).

The selected trip generation rates were applied to the proposed land use, and the results of trip generation calculations are summarized in **Table 4.1**.

Table 4.1: Peak Hour Site Traffic Generation

Land Use	Size	Trip Generation Rate	Inbound Trips	Outbound Trips	Total Trips
AM Peak Hour					
General Light Industrial	110.4 acres	7.51 trips/acre	688	141	829
PM Peak Hour					
General Light Industrial	110.4 acres	7.26 trips/acre	176	626	802

4.3 Site Traffic Distribution

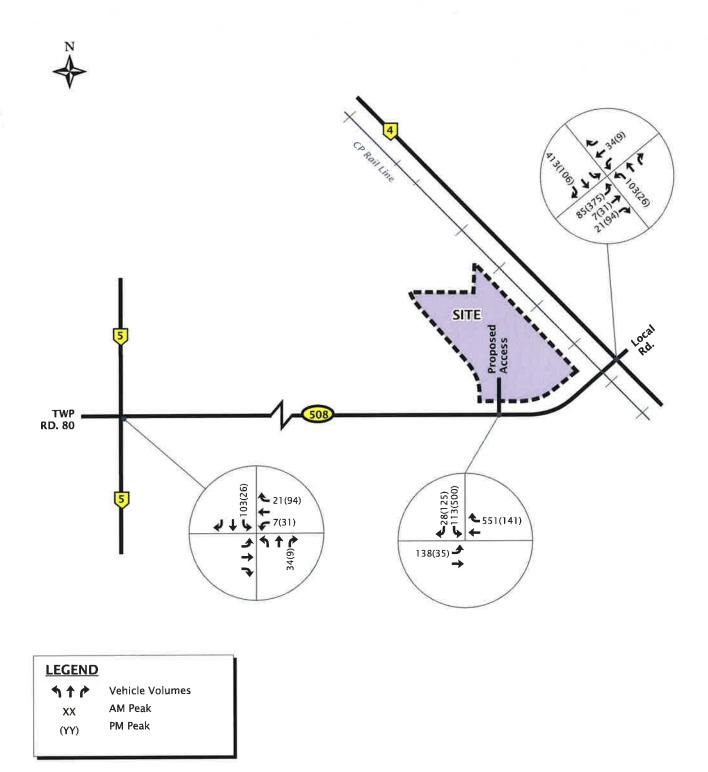
The site traffic trip distribution was based on several factors. Based on the existing traffic count for the few businesses on site, the majority of traffic is coming from the north on Hwy 4, traffic coming from Hwy 5 and from the south on Hwy 4 is about the same and a small portion is coming from the east. With that said, the client has stated that employees will likely come from south Lethbridge and customers will likely come from outside of Lethbridge and/or have interactions with the industrial area. Bunt & Associates also completed time trials during the site visit and from the proposed site to the intersection of Mayor Magrath Drive and 24th Avenue S, which is common point in the south part of Lethbridge, it is faster to take Hwy 4 to this location versus Hwy 5 by approximately 3 minutes.

Based on a combination of these factors and in Bunt & Associates experience, the site traffic distribution is shown in **Table 4.2.**

Table 4.2: Site Traffic Distribution

	Direction	Distribution
To/from the north	on Highway 4	60%
To/from the south	on Highway 4	15%
To/from the west o	n Highway 5 via Highway 5 North	15%
To/from the west o	n Highway 5 via Highway 5 South	5%
To/from the east H	n highway 508	5%
Total		100%

The resulting site generated traffic volumes are illustrated in Exhibit 4.1.



Site Generated Traffic Volumes

Lethbridge Agri-Business Park June 2014 Scale NTS





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5. POST DEVELOPMENT TRAFFIC CONDITIONS

The post development traffic volumes were developed by adding the site generated traffic to both the existing traffic and 20-year background traffic volumes.

5.1 Opening Day Post Development Conditions

The Opening Day post development traffic volumes were developed by adding the site generated traffic volumes to the existing traffic volumes. The Opening Day Post Development traffic volumes are illustrated in **Exhibit 5.1**

5.1.1 Intersection Treatment Type

The Alberta Transportation Intersection Treatment type was determined on Highway 508 at both the realigned proposed site access and at Highway 5 based on the Opening Day post development traffic volumes.

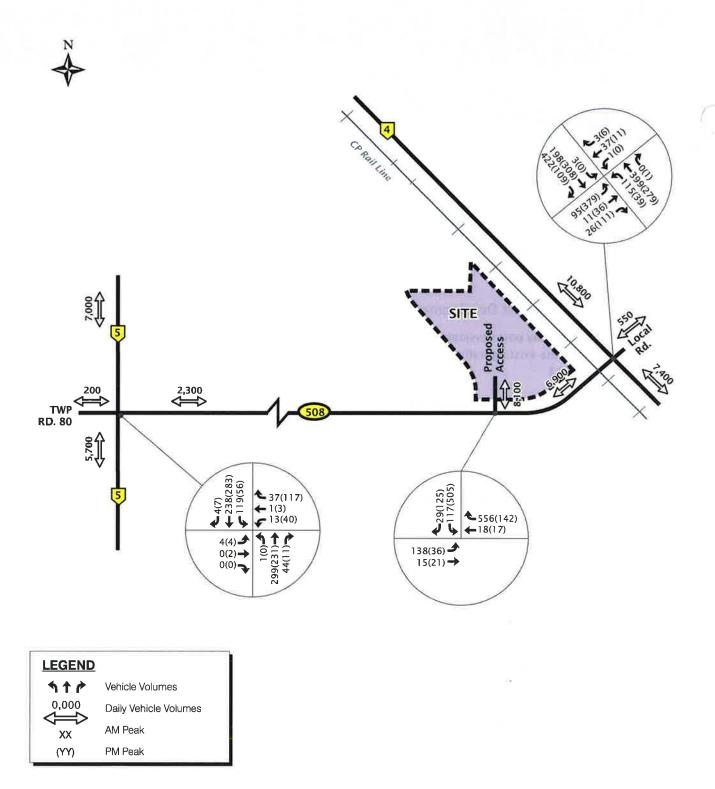
Highway 508 at Realigned Proposed Site Access

Left Turn Lane Warrant

Utilizing the Opening Day post development traffic volumes at the intersection of Highway 508 and the realigned proposed site access, the AM peak hour traffic volumes are the worst case scenario and as such were the traffic volumes used for this analysis. The volume of left turn vehicles is 138 vph, the approaching volume is 153 vph, resulting in 90% left turn vehicles in the approaching volume and the opposing traffic is 574 vph. Based on D-7.6-7d (the highest left turn lane volume graph is for 40%) with a design speed of 110 km/hr on Highway 508, a Type IV intersection is warranted.

Right Turn Lane Warrant

Based on the right turn lane warrant stated earlier, a right turn lane is warranted for the westbound direction on Highway 508 at the realigned proposed site access because the main road AADT is 6,900 vpd, the intersecting road AADT is 8,100 vpd and the right turn lane volume is 1,420 vpd.



Opening Day Post Development Traffic Volumes

Lethbridge Agri-Business Park June 2014 Scale NTS



Highway 508 at Highway 5

Left Turn Lane Warrant

Utilizing the Opening Day post development traffic volumes on Highway 508 at the intersection with Highway 5, the PM peak hour traffic volumes are the worst case scenario and as such were the traffic volumes used for this analysis. The volume of left turn vehicles is 40 vph, the approaching volume is 160 vph, resulting in 25% left turn vehicles in the approaching volume and the opposing traffic is 6 vph. Based on D-7.6-7c with a design speed of 110 km/hr on Highway 508, a Type I intersection is warranted.

Right Turn Lane Warrant

Based on the right turn lane warrant stated earlier, a right turn lane is warranted for the westbound direction on Highway 508 at Highway 5 as the main road AADT is 7,000 vpd, the intersecting road AADT is 2,300 vpd and the right turn lane volume is 1,170 vpd.

5.1.2 Intersection Capacity Analysis

The Synchro 8.0 software package was used to assess the study area intersections based on the Opening Day post development traffic conditions. The Opening Day post development traffic analysis was completed assuming the existing lane arrangements with the realignment of the proposed access as previously discussed along with the intersection treatment types determined above and the existing traffic controls. The intersection capacity results for the Opening Day post development traffic conditions are summarized in **Table 5.1.** The Synchro outputs are attached in Appendix C.

Table 5.1: Opening Day Post Development Intersection Capacity Analysis

			AM	Peak		PM Peak					
Intersection	Movement	v/c	LOS	Delay (s)	Queue (m)	v/c	LOS	Delay (s)	Queue (m)		
	EBT	0.18	В	11.2	5.3	0.93	E	45.5	99.0		
	EBR	0.18	В	11.2	5.3	0.93	E	45.5	99.0		
Highway 508/Highway 4	WBL/T	0.50	С	24.9	21.1	0.12	В	13.4	3.1		
(west Intersection)	SBL	< 0.01	Α	7.3	0.1	< 0.01	A	0.0	0.0		
	SBT	0.07	Α	0.0	0.0	0.10	Α	0.0	0.0		
	SBR	0.28	A	0.0	0.0	0.07	A	0.0	0.0		
	EBL/T	0.34	С	20.2	12.0	0.76	D	26.9	55.6		
	WBT/R	0.14	С	17.5	3.8	0.03	В	11.2	0.8		
Highway 508/Highway 4 (east Intersection)	NBL	0.08	Α	7.5	2.2	0.03	Α	7.4	0.7		
(case intersection)	NBT	0.13	Α	0.0	0.0	0.09	A	0.0	0.0		
	NBR	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0		
	EBL	0.17	A	9.7	4.9	0.03	Α	7.7	0.7		
	EBT	0.01	Α	0.0	0.0	0.01	Α	0.0	0.0		
Highway 508/ Future Realigned Access	WBT	0.01	Α	0.0	0.0	0.01	Α	0.0	0.0		
rature realigned Access	WBR	0.37	Α	0.0	0.0	0.09	Α	0.0	0.0		
	SB	0.29	В	13.7	13.7	0.83	D	26.1	77.4		
	EB	0.02	C	21.8	0.5	0.03	С	18.7	0.6		
	WBL/T	0.07	8	13.5	1.7	0.17	8	12.5	5.0		
	WBR	0.07	В	13.5	1.7	0.17	В	12.5	5.0		
Highway 508/Highway 5	NBL/T	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0		
	NBR	0.03	Α	0.0	0.0	0.01	Α	0.0	0.0		
	SBL	0.12	A	8.6	3.2	0.05	A	8.0	1.3		
	SBT/R	0.16	Α	0.0	0.0	0.19	Α	0.0	0.0		

As can be seen in the Table 5.1, with the addition of site generated traffic from the proposed development, the west intersection of Highway 4/ Highway 508 experiences LOS E and v/c ratio of 0.93 during the PM peak hour. Due to the location of this intersection, it is unlikely that a traffic signal would be implemented. Bunt & Associates completed a traffic signal warrant for the intersection which resulted in a score of 74 points out of the required 100 points. Therefore a traffic signal is not warranted. The signal warrant analysis is attached in **Appendix F**.

Bunt & Associates also completed a sensitivity analysis as it is likely that drivers may avoid the congestion at Highway 4/ Highway 508 if they are not captive to the route and will shift to utilize Highway 5 to the west and then head north towards the City of Lethbridge. If approximately 5-10% of the eastbound site generated traffic on Highway 508 in fact shifted to head to the west and utilize Highway 5 versus Highway 4 to head north, the west intersection at Highway 4/ Highway 508 would be within the acceptable capacity parameters and the increase in traffic volumes at the Highway 5/ Highway 508 intersection would continue to be accommodated with the intersection still operating within the acceptable capacity parameters.

Bunt & Associates therefore recommends that the intersection of Highway 4/ Highway 508 be reviewed as each stage of the proposed development is implemented to determine the impacts on the intersection of Highway 4/ Highway 508. This is crucial as trip rates applied to the site may be conservative, and the actual trip ends may be much lower than used in this analysis.

The queue length for the west intersection at Highway 508/ Highway 4 also was reviewed as the 95th percentile queue extends back to the west approximately 100 metres back to the west, crossing the CP rail line. A SimTraffic simulation run was completed, which resulted in a 53 metre 95th percentile queue length. The existing distance between the stop line on Highway 508 at Highway 4 to the railway crossing is approximately 30 metres and as such traffic will queue across the railway tracks resulting in a major safety concern. Bunt & Associates therefore recommends the implementation of warning gates at the railway crossing as a safety measure. It should be noted that the railway crossing warrant was subsequently completed and warning gates are in fact warranted at this crossing.

The east intersection of Highway 4/ Highway 508 experiences a LOS D for the eastbound movement; however the v/c ratio is only 0.76 and the queue length is less than the existing spacing between the east and west intersections. With that said, Bunt & Associates does not feel that any improvements are required at this time for the east intersection at Highway 4/ Highway 508.

The future realigned access with Highway 508 also experiences a LOS D during the PM peak hour for the southbound movements however the v/c ratio is 0.83. A southbound right turn lane of approximately 50 metres in length could be implemented to bring the LOS down to a LOS C, however in Bunt & Associates opinion it is not required since the southbound leg is within the proposed site.

5.1.3 Illumination Warrant

Once again, Bunt & Associates undertook an illumination warrant for the three study area intersections based on the Transportation Association of Canada (TAC) methodology for Illumination of Isolated Rural Intersections¹¹ utilizing the Opening Day post development traffic volumes. The illumination warrant again reviewed the geometric, operational, environmental and collision factors for the study area intersections.

Highway 508/ Highway 4

Based on the illumination warrant under the Opening Day post development traffic conditions, the intersection of Highway 508/ Highway 4 scored 236 points. As a result the intersection warrants partial and/or delineation lighting. Based on the above criteria and the results of the illumination warrant, the operational factors scored 180 points and thus is greater than the 120 points which warrants delineation lighting to illuminate pedestrians and or cross street traffic which is the case at this intersection.

As previously found under existing traffic conditions it was determined that illumination was warranted; however it was undetermined as to whether partial or delineated lighting was required. Now based on the post development traffic analysis, it is has been determined that delineation lighting required and thus is recommended to be installed at the intersection of Highway 4/Highway 508.

Highway 508/ Highway 5

Based on the illumination warrant under Opening Day traffic conditions, the intersection of Highway 508/ Highway 4 now scores 191 points. As a result the intersection warrants partial and/or delineation lighting. Based on the above criteria and the results of the illumination warrant, the operational factors scored 170 points and thus is greater than the 120 points which warrants delineation lighting to illuminate pedestrians and or cross street traffic which again is the case at this intersection.

It was determined that illumination was warranted under the existing traffic conditions; however it was undetermined as to whether partial or delineated lighting was required. Now based on the post development traffic analysis, it is has been determined that delineation lighting is required and is therefore recommended to be installed at the intersection of Highway 5/Highway 508.

Highway 508/ Realigned Access

Based on the illumination warrant under Opening Day traffic conditions, the intersection of Highway 508/ realigned access now scores 166 points. As a result the intersection warrants partial and/or delineation lighting. Based on the above criteria and the results of the illumination warrant, the operational factors scored 140 points and thus is greater than the 120 points which warrants delineation lighting to illuminate pedestrians and or cross street traffic which again is the case at this intersection.

¹¹ Illumination of Isolated Rural Intersections, Transportation Association of Canada (TAC), February 2001.

As a result, Bunt & Associates recommends that delineation lighting be installed at the intersection of Highway 508 at the realigned access.

The Opening Day post development traffic illumination warrant summaries are included in Appendix D.

5.1.4 Rail Crossing Warrant

The rail crossing warrant was once again completed based on the Opening Day post development traffic volumes. Again, Transport Canada's¹² requirements for rail crossings determines that lights are required at a rail crossing when the forecast cross-product¹³ is 1,000 or more and gates are required when the forecast cross product is 50,000 or more. The cross product for the crossing at Highway 508 is now 55,200¹⁴ based on the Opening Day post development traffic volumes. As a result of the cross product being greater than 50,000, gates are now warranted at the railway crossing on Highway 508 with the inclusion of the proposed site generated traffic volumes. In addition, the warning gates will provide a safety measure for the queue that is expected to extend back towards the railway tracks as previously discussed.

5.1.5 Road Link Analysis

The Opening Day post development link volumes were again assessed based on typical Alberta Transportation highway standards. In general terms, this analysis was intended to assess the daily traffic volumes on all germane roadway links in the study area and to confirm the current roadway classification and/or identify any need for reclassification based on the addition of the proposed site generated traffic volumes to the existing traffic volumes. The results of the assessment are summarized in **Table 5.2** and also illustrated previously on Exhibit 5.1.

Table 5.2: Opening Day Post Development Road Link Analysis

Road Link	Road Classification	Recommended Daily Traffic Volume (vehicles per day)	Opening Day Post Development Daily Traffic Volume' ⁵ (vehicles per day)
Highway 4	4-lane Primary Highway	> 12,000	10,800
Highway 508	2-lane Secondary Highway	< 12,000	6,900
Highway 5	2-lane Primary Highway	< 12,000	7,000
Re-aligned Access	Rural Local Road (gravel)	< 500	8,100

¹² RTD 10 Road/Railway Grade Crossings Technical Standards and Inspection, Testing and Maintenance Requirements, Transport Canada, March 2002.

¹³ Forecast cross product = number of trains per day * daily traffic volume on the roadway

¹⁴ The cross product was calculated on the maximum number of expected trains per day (8 trains per day) to utilize the most conservative estimate.

¹⁵ For the purpose of this study, the daily traffic volumes estimates were based on ten times the PM peak hour volumes. Again rounding took place as under existing traffic conditions.

Based on the road link analysis, the majority of the road links within the vicinity of the site are within the recommended daily traffic volume design guidelines for the various classifications of roadways. However with the addition of the site generated traffic volumes to the proposed access, Bunt & Associates recommends that the access roads within the site be upgraded from a gravel surface to a paved surface roadway.

5.2 20-Year Post Development Conditions

The 20-year post development traffic volumes were developed by adding the site generated traffic volumes onto the 20-year background traffic volumes. The 20-year Post Development traffic volumes are illustrated in **Exhibit 5.2.**

5.2.1 Intersection Treatment Type

The Alberta Transportation Intersection Treatment type was determined on Highway 508 at both the realigned proposed site access and at Highway 5 based on the 20-year post development traffic volumes.

Highway 508 at Realigned Proposed Site Access

The left turn lane warrant was once again completed based on the 20-year post development traffic volumes however due to the minimal increase in traffic volumes the warrant continued to result in the need of a Type IV intersection.

With the implementation of a right turn lane already in place at the Opening Day horizon, the right turn lane warrant was not completed for the 20-year post development horizon.

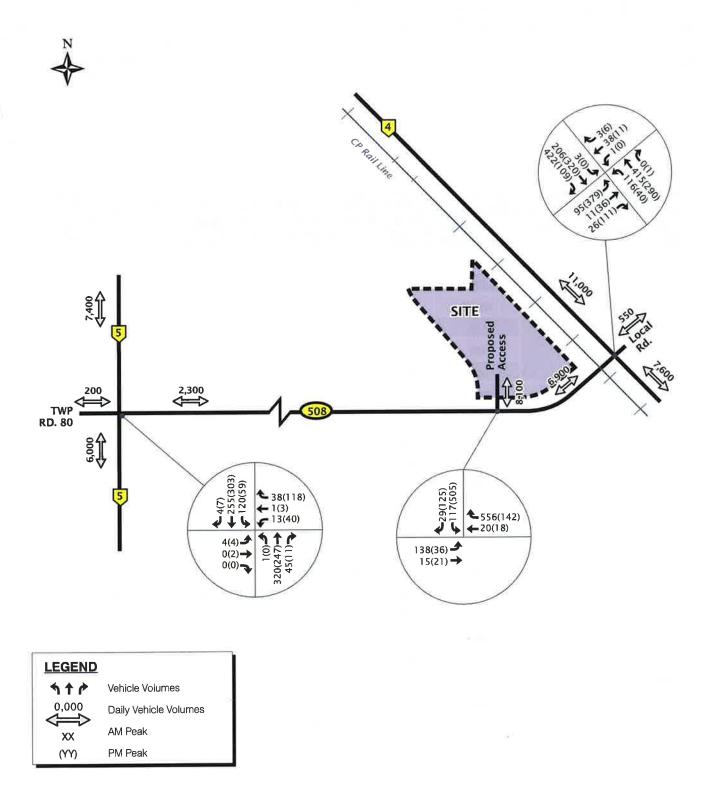
Highway 508 at Highway 5

Again, the left turn lane warrant was once again completed based on the 20-year post development traffic volumes however due to the minimal increase in traffic volumes the warrant continued to result in the need of a Type I intersection.

With the implementation of a right turn lane already in place at the Opening Day horizon, the right turn lane warrant was not completed for the 20-year post development horizon.

5.2.2 Intersection Capacity Analysis

The Synchro 8.0 software package was used to assess the study area intersections based on the 20-year post development traffic conditions. The 20-year post development traffic analysis was completed assuming the existing lane arrangements with the realignment of the proposed access as previously discussed along with the intersection treatment types determined above and the existing traffic controls. The intersection capacity results for the 20-year post development traffic conditions are summarized in **Table 5.3.** The Synchro outputs are attached in Appendix C.



20 Year Post Development Traffic Volumes

Lethbridge Agri-Business Park June 2014 Scale NTS



Table 5.3: 20-Year Post Development Intersection Capacity Analysis

		3.54	AM	Peak		PM Peak					
Intersection	Movement	v/c	LOS	Delay (s)	Queue (m)	v/c	LOS	Delay (s)	Queue (m)		
	EBT	0.19	В	11.3	5.4	0.94	E	49.0	103.6		
	EBR	0.19	8	11.3	5.4	0.94	E	49.0	103.6		
Highway 508/Highway 4	WBL/T	0.51	D	25.7	22.0	0.12	В	13.5	3.3		
(west Intersection)	SBL	< 0.01	Α	7.3	0.1	< 0.01	Α	0.0	0.0		
	SBT	0.07	Α	0.0	0.0	0.11	Α	0.0	0.0		
	SBR	0.28	Α	0.0	0.0	0.07	Α	0.0	0.0		
	EBL/T	0.35	С	20.8	12.5	0.77	D	28.1	57.8		
	WBT/R	0.15	С	18.0	4.1	0.03	D	11.3	0.8		
Highway 508/Highway 4 (east intersection)	NBL	0.08	Α	7.5	2.2	0.03	В	7.4	0.7		
(east intersection)	NBT	0.14	Α	0.0	0.0	0.10	A	0.0	0.0		
	NBR	< 0.01	Α	0.0	0.0	< 0.01	Α	0.0	0.0		
	EBL.	0.17	Α	9.7	4.9	0.03	Α	7.7	Α		
	EBT	0.01	Α	0.0	0.0	0.01	Α	0.0	Α		
Highway 508/ Future Realigned Access	WBT	0.01	A	0.0	0.0	0.01	A	0.0	Α		
. attail of Realing Flee Precess	WBR	0.37	Α	0.0	0.0	0.09	Α	0.0	Α		
	SB	0.29	В	13.7	9.4	0.83	D	26.3	D		
	EB	0.02	С	23.3	0.6	0.02	С	16.1	0.5		
	WBL/T	0.07	8	14.0	1.9	0.04	В	11.9	1.0		
	WBR	0.07	В	14.0	1.9	0.04	В	11.9	1.0		
Highway 508/Highway 5	NBL/T	< 0.01	Α	0.0	0.0	< 0.01	A	0.0	0.0		
	NBR	0.03	Α	0.0	0.0	< 0.01	Α	0.0	0.0		
	SBL	0.12	Α	8.6	3.3	0.03	Α	7.9	0.7		
	SBT/R	0.17	Α	0.0	0.0	0.21	Α	0.0	0.0		

As can be seen in the Table 5.3, with the addition of site generated traffic from the proposed development, the west intersection of Highway 4/ Highway 508 experiences LOS E and v/c ratio of 0.94 during the PM peak hour. Again, due to the location of this intersection and the high speed limit on the highway it is unlikely that a traffic signal would be implemented; however with that said Bunt & Associates did complete a traffic signal warrant for the intersection which resulted in a score of 76 points out of the required 100 points and thus a traffic signal is not warranted. The signal warrant analysis is attached in **Appendix F**.

Again, Bunt & Associates completed a sensitivity analysis as it is likely that drivers may avoid the congestion at Highway 4/ Highway 508 if they are not captive to the route and will shift to utilize Highway 5 to the west and then head north towards the City of Lethbridge. If approximately 5-10% of the eastbound site generated traffic on Highway 508 in fact shifted to head to the west and utilize Highway 5 versus Highway 4 to head north, the west intersection at Highway 4/ Highway 508 would operate within the acceptable capacity parameters. The increase in traffic volumes at the intersection of Highway 5/ Highway 508 can be accommodated and the intersection will continue to operate within acceptable capacity parameters.

Bunt & Associates however, recommends that the intersection of Highway 4/ Highway 508 be reviewed as each stage of the proposed development is implemented to determine the impacts on the intersection of Highway 4/ Highway 508. Again, this is crucial as trip rates applied to the site may be conservative, and the actual trip ends may be much lower than used in this analysis.

The queue length of the west approach of the west intersection at Highway 508/ Highway 4 also was reviewed as the 95th percentile queue extends back approximately 105 metres crossing the CP rail line. SimTraffic simulation run was completed which resulted in a 69-metre 95th percentile queue length. The existing distance between the stop line on Highway 508 at Highway 4 to the railway crossing is approximately 30 metres and as such traffic will queue across the railway tracks resulting in a major safety concern.

Bunt & Associates therefore recommends the implementation of warning gates at the railway crossing as a safety measure. It should be noted that the railway crossing warrant was completed subsequently and warning gates are in fact warranted at this crossing.

The east intersection of Highway 4/ Highway 508 experiences a LOS D for the eastbound and westbound movements; however the v/c ratio is only 0.77 and 0.03 respectively and the queue length is less than the existing spacing between the east and west intersections. With that said, Bunt & Associates does not recommend any improvements at this time for the east intersection at Highway 4/ Highway 508.

Again, the future realigned access with Highway 508 will experience a LOS D during the PM peak hour for the southbound movements, however the v/c ratio is 0.83. As such, changes are not recommended to the intersection configuration.

5.2.3 Illumination Warrant

Once again, Bunt & Associates undertook an illumination warrant for the three study area intersections based on the Transportation Association of Canada (TAC) methodology for Illumination of Isolated Rural Intersections¹⁶ utilizing the 20-year post development traffic volumes. The illumination warrant again reviewed the geometric, operational, environmental and collision factors for the study area intersections.

Highway 508/ Highway 4

Based on the illumination warrant under the 20-year post development traffic conditions, the intersection of Highway 508/ Highway 4 scored 236 points which is unchanged from the Opening Day warrant analysis. As such the operational factors again scored 180 points resulting in the warrant for delineation lighting to illuminate pedestrians and or cross street traffic.

Highway 508/ Highway 5

Based on the illumination warrant under 20-year post development traffic conditions, the intersection of Highway 508/ Highway 4 scored 191 points which again is unchanged form the Opening Day warrant analysis. As such the operational factors again scored 170 points resulting in the warrant for delineation lighting to illuminate pedestrians and or cross street traffic.

Highway 508/ Realigned Access

Based on the illumination warrant under 20-year post development traffic conditions, the intersection of Highway 508/ realigned access again scored 166 points, same as the Opening Day warrant analysis. As such the operational factors continue to score 140 points resulting in the warrant for delineation lighting to illuminate pedestrians and or cross street traffic.

The 20-year post development traffic illumination warrant summaries are included in Appendix D.

5.2.4 Rail Crossing Warrant

The rail crossing warrant was once again completed based on the 20-year post development traffic volumes. As stated, Transport Canada's¹⁷ requirements for rail crossings determines that lights are required at a rail crossing when the forecast cross-product¹⁸ is 1,000 or more and gates are required when the forecast cross product is 50,000 or more. The cross product for the crossing at Highway 508 is again 55,200¹⁹ based on the 20-year post development traffic volumes. As a result of the cross product being greater than 50,000, gates are now warranted at the railway crossing on Highway 508 with the inclusion of

¹⁶ Illumination of Isolated Rural Intersections, Transportation Association of Canada (TAC), February 2001.

¹⁷ RTD 10 Road/Railway Grade Crossings Technical Standards and Inspection, Testing and Maintenance Requirements, Transport Canada, March 2002.

¹⁸ Forecast cross product = number of trains per day * daily traffic volume on the roadway

¹⁹ The cross product was calculated on the maximum number of expected trains per day (8 trains per day) to utilize the most conservative estimate.

the proposed site generated traffic volumes as was the case under the 20-year post development traffic volumes. In addition, the warning gates will provide a safety measure for the queue that is expected to extend back towards the railway tracks as previously discussed.

5.2.5 Road Link Analysis

The 20-year post development link volumes were again assessed based on typical Alberta Transportation highway standards. In general terms, this analysis was intended to assess the daily traffic volumes on all germane roadway links in the study area and to confirm the current roadway classification and/or identify any need for reclassification based on the addition of the proposed site generated traffic volumes to the existing traffic volumes. The results of the assessment are summarized in **Table 5.4** and also illustrated previously on Exhibit 5.2.

Table 5.4: 20-Year Post Development Road Link Analysis

Road Link	Road Classification	Recommended Daily Traffic Volume (vehicles per day)	Opening Day Post Development Daily Traffic Volume ²⁰ (vehicles per day)
Highway 4	4-lane Primary Highway	> 12,000	11,000
Highway 508	2-lane Secondary Highway	< 12,000	6,900
Highway 5	2-lane Primary Highway	< 12,000	7,400
Re-aligned Access	Rural Local Road (gravel)	< 500	8.100

Based on the road link analysis, the majority of the road links within the vicinity of the site are within the recommended daily traffic volume design guidelines for the various classifications of roadways. However as was the case under the Opening Day post development road link analysis, Bunt & Associates recommends that the access roads within the site be upgraded from a gravel surface to a paved surface roadway.

Lethbridge Agri-Business Park TIA Final Report bunt & associates | Project No. 1283-09 | June 20, 2014

²⁰ For the purpose of this study, the daily traffic volumes estimates were based on ten times the PM peak hour volumes. Again rounding took place as under existing traffic conditions.



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CONCLUSIONS AND RECOMMENDATIONS

The key findings and recommendations are summarized as follows:

6.1 Key Findings and Recommendations

The key findings and recommendations are summarized here, as follows:

Existing Traffic Conditions

All study area intersections are currently operating within the acceptable capacity parameters and study area roadways are currently functioning within their respective environmental capacities.

Bunt & Associates also completed an illumination warrant for the three study area intersections. The intersections on Highway 508 at both Highway 4 and Highway 5 warrant either partial and/or delineated lighting; however, the warrant did not determine which specific or if both types of illumination are warranted and as such it is recommended that further review is undertaken to determine the specific illumination required.

A railway crossing warrant was also completed for the Canadian Pacific rail line that runs parallel to Highway 4 and intersects Highway 508. Based on the cross product of the daily traffic volumes and the maximum number of trains expected to cross at this location, flashing warning lights are to be implemented at the rail crossing on Highway 508.

20-Year Background Traffic Conditions

The 20-year background traffic conditions exhibits the same results as under the existing traffic conditions. As such, all study area intersections and roadways are expected to operate within the acceptable capacity parameters. The intersections of Highway 508 with both Highway 4 and Highway 5 both warrant partial and/or delineation lighting. Flashing warning lights are warranted at the CP rail crossing on Highway 508 just west of Highway 4.

Proposed Development

The proposed Agri-Business Park that will service both agricultural and oil field sectors and is expected to generate 829 trips (688 inbound/ 141 outbound) during the AM peak hour and 802 trips (176 inbound/ 626 outbound) during the PM peak hour.

Post Development Traffic Conditions

Opening Day Post Development Traffic Conditions

Based on the Opening Day post development traffic conditions, Highway 508 at both Highway 5 and the realigned proposed site access requires a westbound right turn lane. The new proposed intersection at the realigned site access with Highway 508 requires a Type IV intersection treatment.

With these additions in place, the west intersection of Highway 4/ Highway 508 is expected to operate at v/c ratio of 0.93 and LOS E. It is highly unlikely that a traffic signal would be implemented at this location due to the high speed on the roadway and based on TAC signal warrant, a traffic signal is in fact not warranted.

With that said, delays will be experienced at this intersection and as such it is likely that traffic will utilize Highway 5 versus Highway 4 to access the south end of the City of Lethbridge. With only a 5-10% shift in traffic from the eastbound movements at Highway 4 to the westbound movements at Highway 5, both intersections will be expected to operate within acceptable capacity parameters.

Even with this shift in traffic, the 95th percentile queue length is expected to extend across the CP railway tracks and as such causes a safety concern. Therefore, Bunt & Associates recommends that warning gates be installed at the railway crossing to ensure safety to eastbound vehicles at this crossing. Given the low number of daily train traffic, the impact of the gates would not decrease the capacity of Highway 508 beyond what would be experienced without the gate.

Based on the road link analysis, all study area roadways are expected to operate within the environmental capacities for their specific road classification. The proposed site access is recommended to be upgraded from gravel to a paved surface.

Illumination warrant was completed for the three study area intersections along Highway 508 and under opening day post development traffic conditions, all three intersections warrant delineated lighting based on operational factors.

The railway crossing warrant was completed for the Canadian Pacific rail line that runs parallel to Highway 4 and intersects Highway 508 based on the opening day traffic conditions. Based on the cross product of the daily traffic volumes and the maximum number of trains expected to cross at this location, warning gates are warranted at the rail crossing on Highway 508. As previously stated, warning gates are also recommended to ensure the safety of vehicles what will queue beyond the railway crossing.

20-Year Post Development Traffic Conditions

The 20-year post development traffic conditions exhibited much the same results as the Opening Day traffic conditions. The new proposed intersection at the realigned site access with Highway 508 warrants a Type IV intersection treatment.

The west intersection of Highway 4/ Highway 508 will continue to operate at v/c ratio of 0.94 and LOS E. Based on TAC signal warrant analysis, a traffic signal is not warranted. However, some delays will be experienced at the intersection and as such it is likely that some non-captive traffic will shift to Highway 5 from Highway 4 to access the south end of the City of Lethbridge. With only a 5-10% shift in traffic from the eastbound movements at Highway 4 to the westbound movements at Highway 5, both intersections are expected to operate within acceptable capacity parameters. Again, even with the shift in traffic, the 95th percentile queue length is expected to extend across the CP railway tracks and as such causes a safety concern. Therefore, Bunt & Associates recommends that warning gates be installed at the railway crossing at the Opening Day to ensure safety of vehicles at this crossing.

Based on the road link analysis, all study area roadways are expected to operate within the environmental capacities for their specific road classification assuming the proposed access has been upgraded to a paved surface based on the Opening Day traffic conditions.

Once again, an illumination warrant was completed for the three study area intersections along Highway 508 and under opening day post development traffic conditions, all three intersections warrant delineated lighting based on operational factors.

The railway crossing warrant was again completed for the Canadian Pacific rail line that runs parallel to Highway 4 and intersects Highway 508 based on the opening day traffic conditions. Based on the cross product of the daily traffic volumes and the maximum number of trains expected to cross at this location, warning gates are warranted at the rail crossing on Highway 508. As previously stated, warning gates are recommended to ensure the safety of vehicles what will queue beyond the railway crossing.

Summary

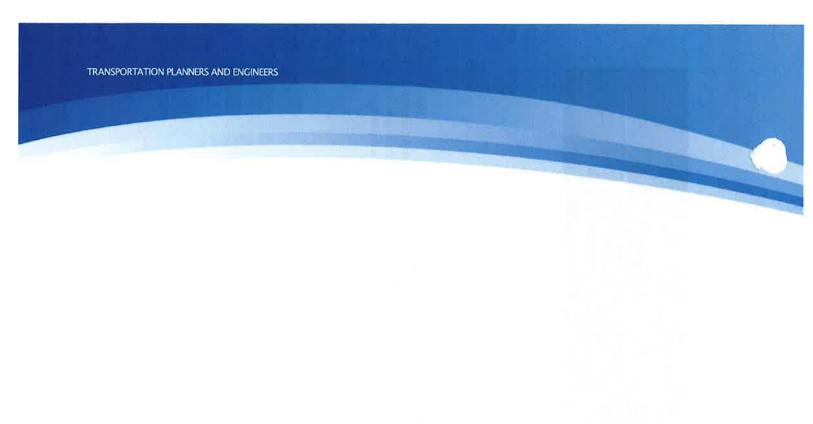
The proposed Agri-Business Park is anticipated to add a significant amount of traffic to the surrounding road network resulting in road network improvements at each horizon year. With that said **Table 6.1** summarizes the improvements required to accommodate the proposed site generated traffic volumes as discussed above.

Table 6.1 Summary of Road Network Improvements

Horizon Year		Recommended I	Recommended Intersection Improvements		
Traffic Conditions	Highway 508/ Highway 4 (west intersection)	Highway 508/ Highway 4 (east intersection)	Highway 508/ Highway 5	Highway 508/ Site Access	Highway 508 CP Rail Crossing
Existing	 No intersection improvements required Partial and/or delineated illumination is warranted 	 No intersection improvements required Partial and/or delineated illumination is warranted 	No improvements are required	 No improvements are required 	Flashing warning lights are warranted
20-Year Background	 No intersection improvements required Partial and/or delineated illumination is warranted 	 No intersection improvements required Partial and/or delineated illumination is warranted 	No improvements are required	 No improvements are required 	 Flashing warning lights are warranted
Opening Day Post Development	 Eastbound movement does not operate within acceptable capacity parameters; however a traffic signal is not warranted. Traffic may utilize alternate route of Hwy 5 to avoid congestion at Hwy 4, thus a 5-10% shift in traffic will bring the intersection within acceptable parameters. The queue length extends beyond the rail line and as such warning gates are to be implemented based on the warrant and for safety reasons. Delineation illumination is warranted 	No intersection improvements required Delineation illumination is warranted	Westbound right turn lane required Delineation illumination is warranted	 Type IV intersection treatment required Westbound right turn lane required Site access roadway requires a paved surface Delineation illumination is warranted 	Rail Crossing Gates are warranted

Table 6.1 Summary of Road Network Improvements - Continued

	Highway 508 CP Rail Crossing	Rail Crossing Gates are warranted
	Highway 508/ Site Access	 Type IV intersection treatment required Westbound right turn lane required Site access roadway requires a paved surface Delineation is warranted
Recommended Intersection Improvements	Highway 508/ Highway 5	Westbound right turn lane required Delineation is warranted
Recommended In	Highway 508/ Highway 4 (east intersection)	 No intersection improvements required Delineation illumination is warranted
	Highway 508/ Highway 4 (west intersection)	 Eastbound movement does not operate within acceptable capacity parameters; however a traffic signal is not warranted. Traffic may utilize alternate route of Hwy 5 to avoid congestion at Hwy 4 and thus a 5-10% shift in traffic will bring the intersection within acceptable parameters. The queue length extends beyond the rail line and as such warning gates are to be implemented based on the warrant and for safety reasons. Delineation illumination is warranted
Horizon Year	Traffic Conditions	20-Year Post Development



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APPENDIX A

Scope of Work Correspondence



Subject: RE: Lethbridge Agri-Business Park

Date: Tuesday, May 27, 2014 11:47:10 AM GMT-06:00

From: Amanda Leibel
To: John Thomas

HI John

I just wanted to follow up on the below for your scope approval.

Thanks!

Amanda Leibel, P.Eng. Transportation Engineer

306-315-9447 www.bunteng.com

From: Amanda Leibel

Sent: Thursday, May 22, 2014 11:07 AM

To: John Thomas

Subject: Re: Lethbridge Agri-Business Park

Hi John

I just wanted to follow up with our phone conversation, sorry it has taken so long but I just needed to confirm a few things so I could send one email. The following is the updated scope of work based on our conversation and I have a few other questions as follows:

- Trip rates will be based on ITE Land Use 110, General Light Industrial AM peak = 7.51 trips/acre (83%in/17% out) and PM peak = 7.26 trips/acre (22% in/78% out). The proposed land use for the sight is light to medium industrial servicing the agricultural/oil sectors.
- The intersections at Hwy 4 and Hwy 5 with Hwy 508 will be reviewed and the existing AT counts will be utilized. The AM and PM peak counts are for the 100th highest hour. We counted the existing access point since there are currently a few businesses in operation and there are less than 10 vehicles entering/exiting during the peak hour and thus factoring this to the 100th highest hour likely is not much different and thus the peak hour volumes will just be utilized.
- Are there any other developments in the area that set to occur and should be included in this TIA?
- The site access has been moved to one access along the tangent, please see attached updated plan.
- Do you know the radius of the horizontal curve on Hwy 508 at this location?
- I assume Hwy 508 is under AT jurisdiction?
- Yearly growth rate Hwy 4 has an average of 2.01% yearly growth over the last five years and thus a 2% yearly linear growth rate will be applied. Hwy 5 yearly data only increased in 2012 over the last five years when an update count was completed and as such had a large

- increase of roughly 13% with no 0% growth in the other years. As such an average of 3.44% was found over the last five years. Therefore a linear growth rate of 3.5% will be applied on Hwy 5. Highway 508 showed a yearly growth rate of 0.46% over the last year; however Bunt feels it is prudent to utilize a growth rate of 2%/ year on Hwy 508.
- Trip Distribution based on the existing traffic count for the few businesses on site, the majority of traffic is coming from the north on Hwy 4, traffic coming from Hwy 5 and from the south on Hwy 4 is about the same and a small portion is coming from the east. With that said, the client has stated that employees will likely come from south Lethbridge and customers will likely come from outside of Lethbridge and/or have interactions with the industrial area. I completed time trials while I was in Lethbridge and from the site to the intersection of Mayor Magrath/ 24th Avenue S, it is faster to take Hwy 4 to this location versus Hwy 5 by approximately 3 mins. With all of this taken into consideration, I propose the following distribution for site traffic:
 - To/from the north on Hwy 4 60%
 - To/From the south on Hwy 4 15%
 - \circ To/ From the West via Hwy 5 20% (of this traffic 15% will come from the north and 5% from the south)
 - ∘ To/From the East 5%

I believe this covers the entire scope of work. Please review and if you could answer the remaining questions it would be greatly appreciated.

Thanks!

Amanda Leibel, P.Eng. | Transportation Engineer

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Suite 380 11012 Macleod Trail SE, Calgary, AB, Canada T2J 6A5 p 403 252 3343 | www.bunteng.com



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From: John Thomas < John. Thomas@gov.ab.ca >

Date: Thursday, May 8, 2014 2:25 PM
To: Amanda Leibel aleibel@bunteng.com
Subject: RE: Lethbridge Agri-Business Park

Amanda:

Is your extension 101? I would like to give you a quick call to discuss.

thanks

John Thomas

Development/Planning Technologist Southern Region - Lethbridge Alberta Transportation Regional Services ph: 403-381-5426 | john.thomas@gov.ab.ca





From: Amanda Leibel [mailto:aleibel@bunteng.com]

Sent: Thursday, May 08, 2014 11:29 AM

To: John Thomas

Subject: FW: Lethbridge Agri-Business Park

Hi John!

I just wanted to follow up on my below email, I am heading out of town to do the site visit on Monday so was hoping for a response from you prior to that so I don't miss any data collection while completing my site visit.

Thanks again!

Amanda Leibel, P.Eng. | Transportation Engineer

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From: Amanda Leibel <a leibel@bunteng.com>

Date: Monday, May 5, 2014 6:37 PM

To: John Thomas < <u>John.Thomas@gov.ab.ca</u> > Subject: Lethbridge Agri-Business Park

Hi John!

We are completing a TIA on behalf of Hasegawa Engineering for an Agri-Business Park located just south of Lethbridge. The site is located in the NW corner of Hwy 4/ Hwy 508 as shown in the attached plan.

I am proposing the following scope for the TIA:

- Opening day analysis (Existing Traffic + Site Generated Traffic) at the intersections of Hwy 4/ Hwy 508 and Hwy 508/site accesses
- 20-Year analysis at the intersections of Hwy 4/ Hwy 508 and Hwy 508/site accesses
- We will utilize the existing AT traffic count at the intersection of Hwy 4/ Hwy 508.
- Distribution will be based on existing traffic patterns at the study area intersection.
- Trip Generation rates will be based on ITE Trip Generation Manual for a similar site, business park. Once I
 receive more details from the client on potential developments within the area I will determine the exact

rate.

- 20-year volumes will be determined based on the yearly % of traffic increase on Hwy 4 and Hwy 508 for the last 5 years.
- Illumination warrant will be completed
- Rail Crossing warrant will be completed

Lastly, are you aware of any other developments occurring in this area that should be included as background traffic? Is this intersection expected to remain as is within the 20-year horizon?

I look forward to your review of the scope, please let me know if this is acceptable to AT and if there are any questions/comments/additions on the scope of work.

Thanks!

Amanda Leibel, P.Eng. | Transportation Engineer

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http://511.alberta.ca/ab/en.html https://twitter.com/511Alberta

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APPENDIX B

Existing Traffic Count



Weather:

sunny

Date: Tuesday, May 20, 201-Day of Week: Tuesday, May 20, 201-Road Cond: Dry



						Traffic Mo	vements							Pedes	strians	
Time Intervals	NBLT	NB TH	NB RT	SB LT	SB TH	SBRT	EB LT	EB TH	EB RT	WB LT	WB TH	WB RT	N	S	E	W
07:00 - 07:15	1	0	0	0	0	0	0	0	0	0	. 0	0	0	0	0	0
07:15 - 07:30	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0
07:30 - 07:45	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0
07:45 - 08:00	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0
08:00 - 08:15	0	0	0	1	0	1	0	0	0	0	0	1	0	0	0	0
08:15 - 08:30	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0
08:30 - 08:45	0	0	0	1	0	0	0	0	0	0	0	2	0	0	0	0
08:45 - 09:00	0	0	0	2	0	0	0	0	0	0	0	1	0	0	0	0
PHF				0.50		0.25						0.63			-	
Peak V _{15min}				2		1						2				

	SB Truck Percentages LT TH RT 25% 0% 0% SB Turn Percentages LT TH RT 80% 0% 20%		WB Truck Percentages LT TH RT 0% 0% 20% WB Turn Percentages LT TH RT 0% 0% 100%
0		N W E S	5 0 5
	EB Truck Percentages LT TH RT 0% 0% 0% EB Turn Percentages LT TH RT 0% 0% 0%		NB Truck Percentages LT TH RT 0% 0% 0% NB Turn Percentages LT TH RT 0% 0% 0%

Existing Access & Highway 508 (PM) Project #: 1283-09

Peak Hour: Overall PHF:

Weather:

17:00 - 18:00

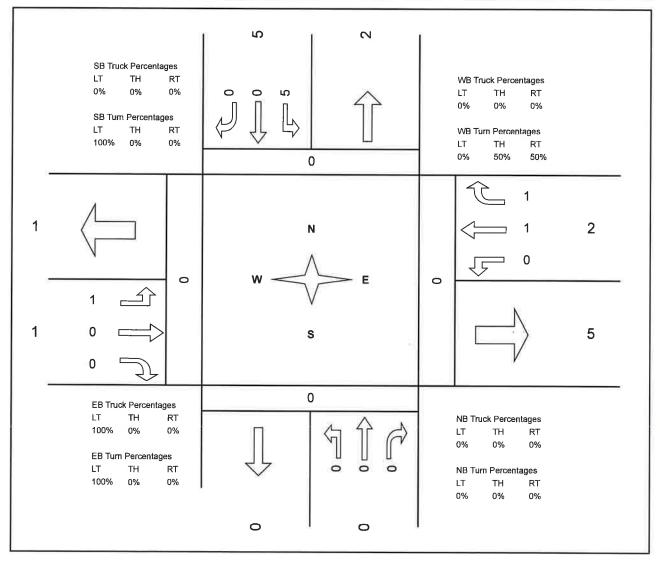
0.67 sunny Date:

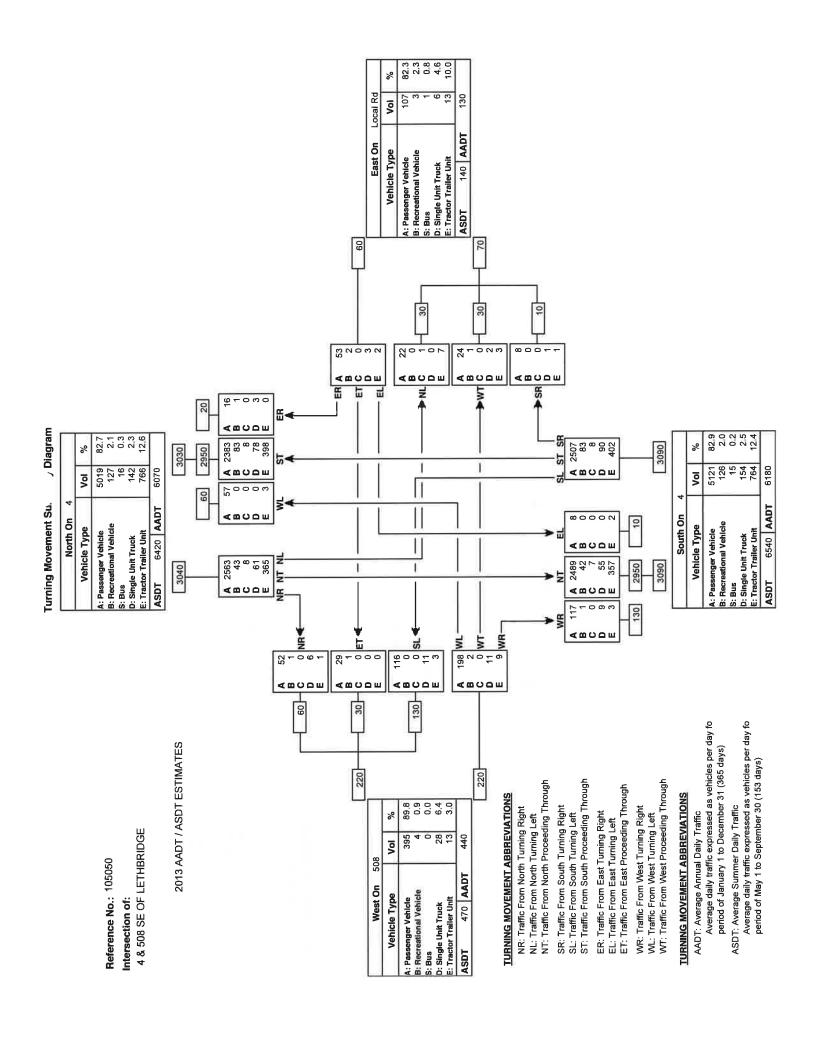
Tuesday, May 20, 201-Day of Week: Tuesday, May 20, 201

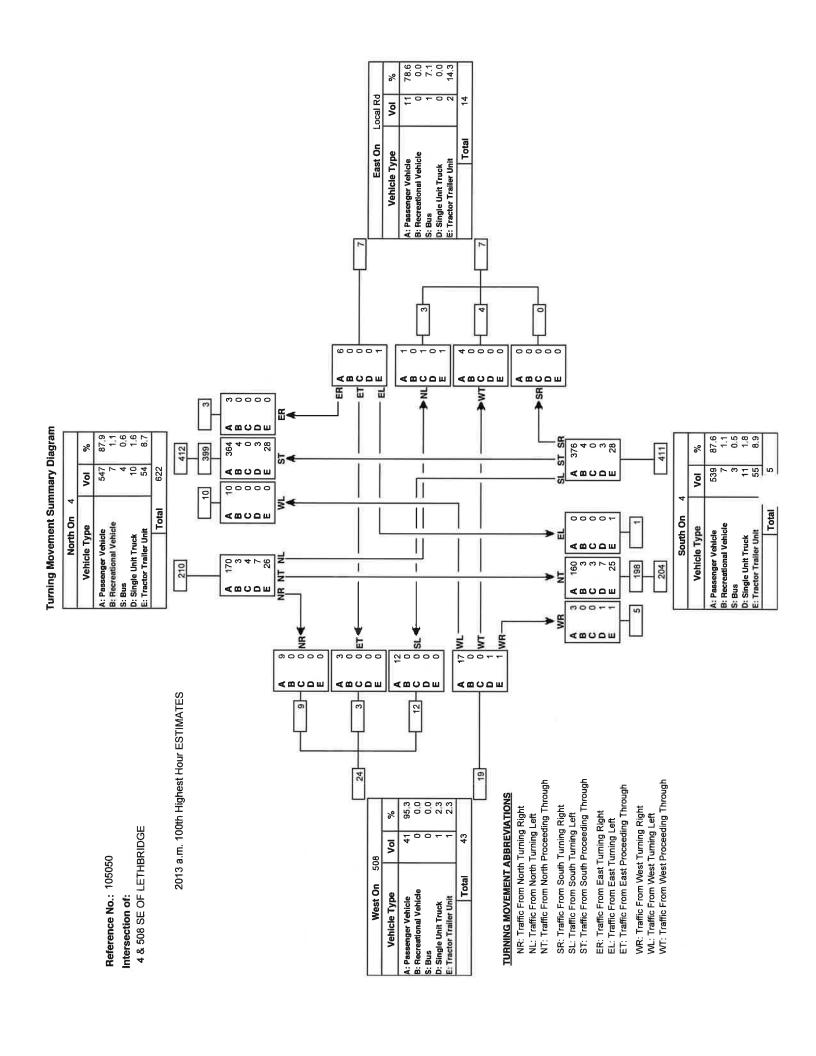
Road Cond: Dry

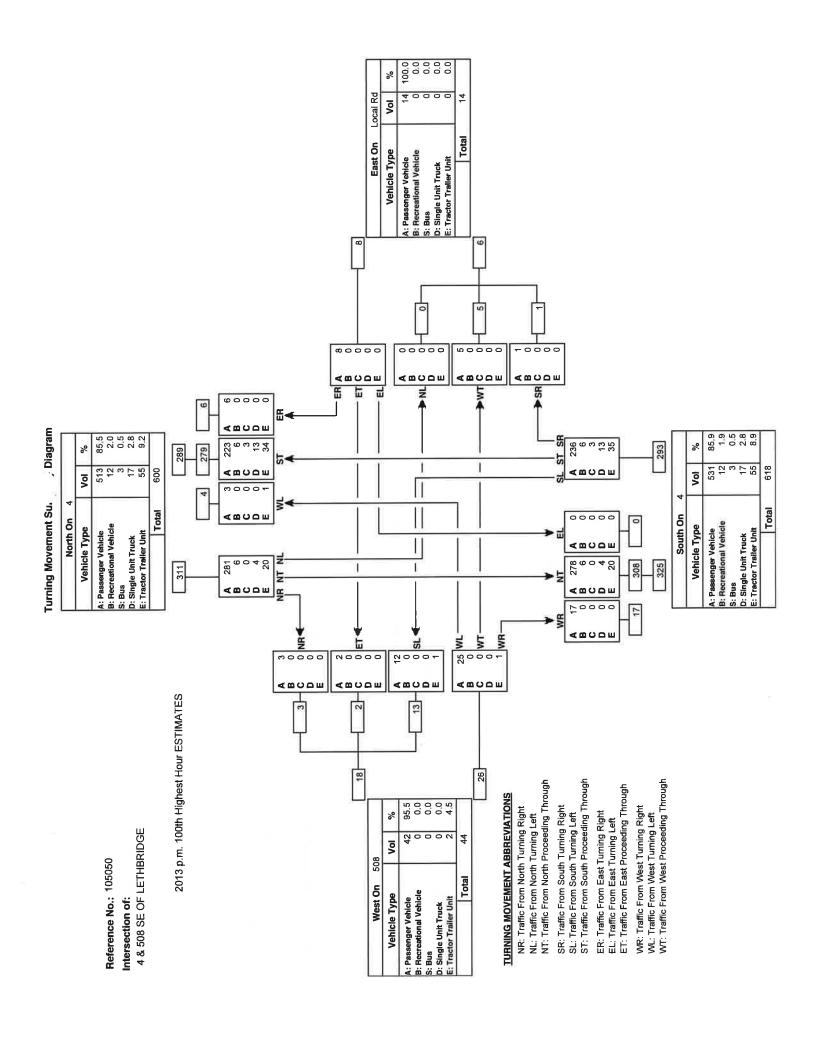


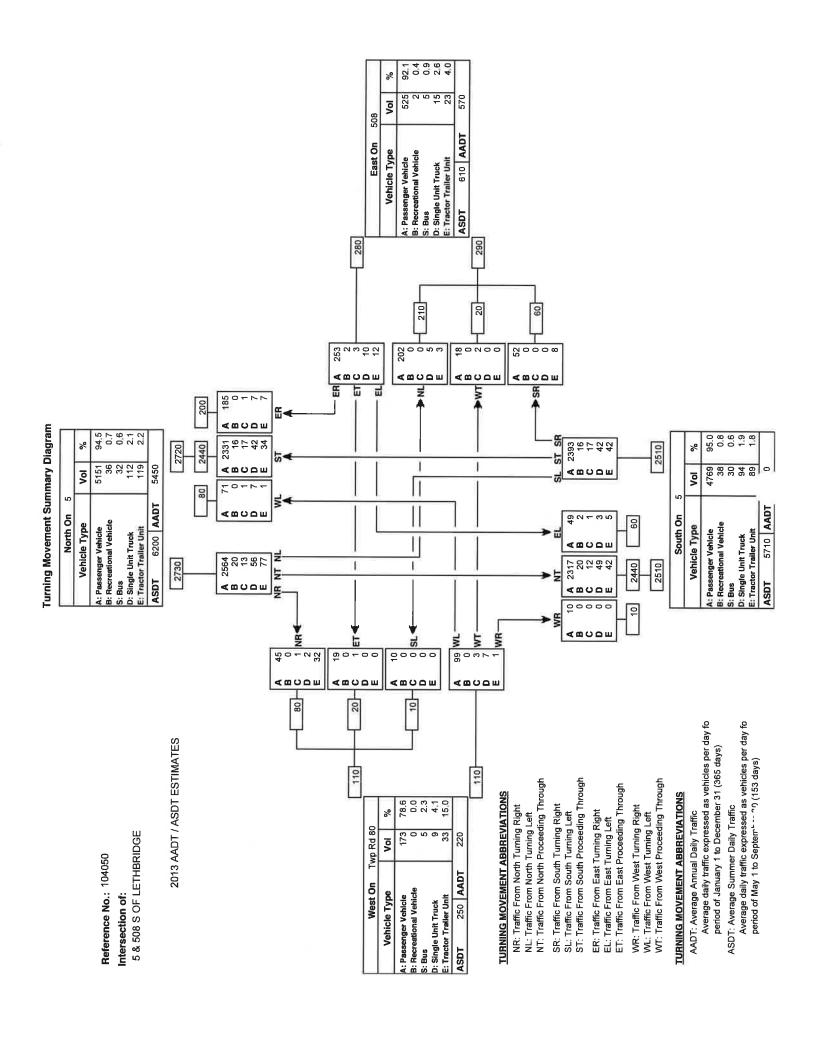
			Traffic Movements											Pedestrians				
Time Inte	rvals	NB LT	NB TH	NB RT	SB LT	SB TH	SB RT	EB LT	EB TH	EB RT	WB LT	WB TH	WB RT	N	S	E	l w	
16:00 -	16:15	0	0	0	0	0	0	0	0	1	0	0	2	0	0	0	0	
16:15 -	16:30	0	0	0	1	0	0	0	0	0	0	0	1	0	0	0	0	
16:30 -	16:45	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	
16:45 -	17:00	0	0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	
17:00 -	17:15	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	
17:15 -	17:30	0	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	
17:30 -	17:45	0	0	0	1	0	0	1	0	0	0	1.	0	0	0	0	0	
17:45 -	18:00	0	0	0	0	. 0	0	0	0	0	0	0	1	0	0	0	0	
PHF					0.42			0.25				0.25	0.25				_	
Peak V	15min				3			1				1	1					

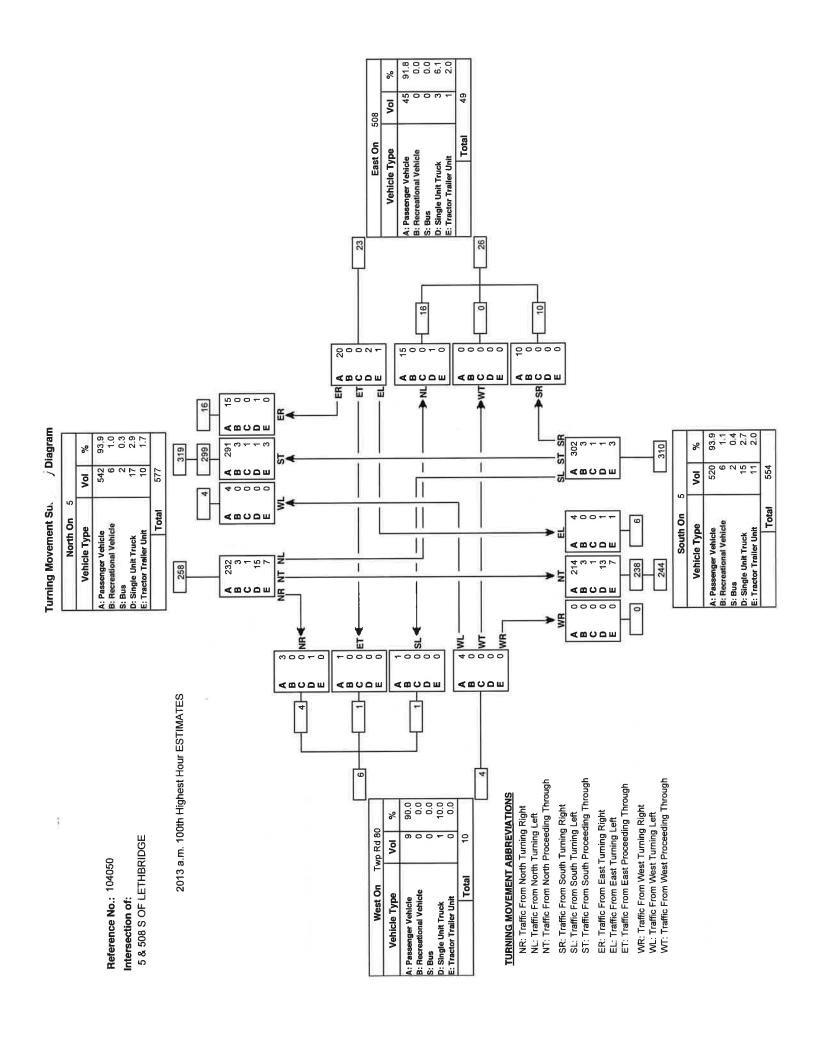


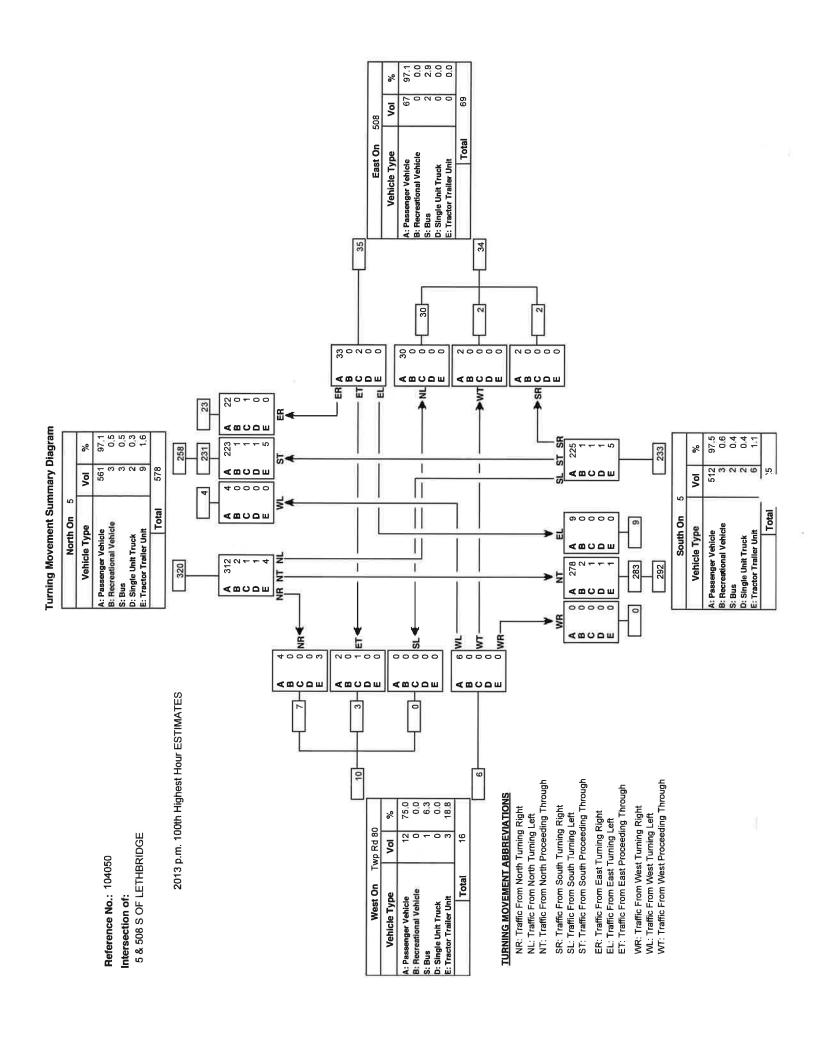






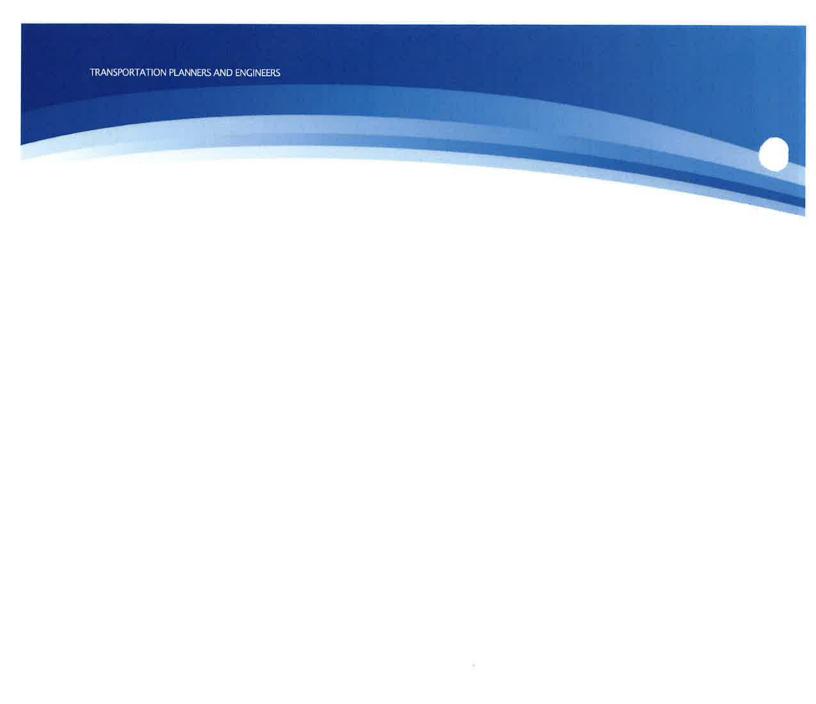






APPENDIX C

Synchro Outputs



Lane Configurations Image: Configuration of the confi		۶	→	*	1	←	•	•	†	1	-	ļ	4
Volume (veh/h)	Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL					SBR
Sign Control Stop	Lane Configurations		4			4							
Grade 0 0% 0.88 0.88 0.88 0.88 0.88 0.88 0.88	Volume (veh/h)	4	0	0	6	1	16	1	299	10	16		4
Peak Hour Factor 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.8	Sign Control		Stop			Stop							
Hourly flow rate (vph) 5 0 0 7 1 18 1 340 11 18 270 Pedestrians Lane Width (m) Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median type	Grade		0%			0%							
Pedestrians Lane Width (m) Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median storage veh) Upstream signal (m) pX, platoon unblocked vCc, conflicting volume vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC3, stage 2 conf vol vC4, stage 1 conf vol vC5, stage 2 conf vol vC5, stage 2 conf vol vC6, stage 2 conf vol vC7, stage 2 conf vol vC9, stage 2 conf vol vC1, stage 1 conf vol vC1, stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB1 WB1 NB1 NB2 SB1 SB2 Volume Total 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume Right 0 0.3 1.2 0.0 0.0 0.4 0.0 Cueue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Cueue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Cueue Length 95th (m) 0.3 1.2 0.0 0.0 0.8 1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B A A Approach CoSacity Utilization 30.5% ICU Level of Service A	Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88			0.88	0.88
Pedestrians Lane Width (m) Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median type	Hourly flow rate (vph)	5	0	0	7	1	18	1	340	11	18	270	. 5
Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median storage veh) None None Upstream signal (m) pxX, platoon unblocked vC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 1 conf vol vC2, stage 1 conf vol vC2, stage 1 conf vol vC2, stage (sol T.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 C2, stage (s) T.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 C5, 2 stage (s) T.5 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 2 SB 1 SB 2 Volume Capacity (veh/h) 356 341 11 18 275 275 2													
Walking Speed (m/s) Percent Blockage Right turn flare (veh) Median storage veh) None None Upstream signal (m) pxX, platoon unblocked vC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 1 conf vol vC2, stage 1 conf vol vC2, stage 1 conf vol vC2, stage (sol T.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 C2, stage (s) T.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 C5, 2 stage (s) T.5 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 2 SB 1 SB 2 Volume Capacity (veh/h) 356 341 11 18 275 275 2	Lane Width (m)												
Reject turn flare (veh) Median type None None Median storage veh) Upstream signal (m) pX, platoon unblocked VC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vC1, unblocked vol 670 662 273 649 653 340 275 351 tC, stage (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) 1f (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0													
Right turn flare (veh) Median type None None None Median storage veh													
Median type None None Median storage veh) Upstream signal (m) pX, platoon unblocked vC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, unblocked vol 670 662 273 649 653 340 275 351 vC2, stage 2 conf vol vC2, unblocked vol 670 662 273 649 653 340 275 351 vC2, stage (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) 1f (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (velr/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1													
Median storage veh) Upstream signal (m) ppx, platoon unblocked vC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vC1, unblocked vol 670 662 273 649 653 340 275 351 tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 1 0 1 0 0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>None</td><td></td><td></td><td>None</td><td></td></t<>									None			None	
Upstream signal (m) pX, platoon unblocked vC, conflicting volume vC2, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 8) tC, single (s) tF (s)													
pX, platoon unblocked vC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vCQ, unblocked vol 670 662 273 649 653 340 275 351 tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A A Approach LOS C B Intersection Summary Average Delay													
vC, conflicting volume 670 662 273 649 653 340 275 351 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, unblocked vol 670 662 273 649 653 340 275 351 tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach Dolay (s) 15.3 11.9 0.0 0.5 NB Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A													
vC1, stage 1 conf vol vC2, stage 2 conf vol vCu, unblocked vol 670 662 273 649 653 340 275 351 tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A		670	662	273	649	653	340	275			351		
vC2, stage 2 conf vol vCu, unblocked vol 670 662 273 649 653 340 275 351 tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.0 0.0 <td></td> <td>• • • •</td> <td></td>		• • • •											
vCu, unblocked vol 670 662 273 649 653 340 275 351 tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 CSH 356 546 1265 1700 1186 1700													
tC, single (s) 7.1 6.5 6.2 7.2 6.6 6.3 4.2 4.2 tC, 2 stage (s) tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2		670	662	273	649	653	340	275			351		
tC, 2 stage (s) tF (s)								4.2			4.2		
tF (s) 3.5 4.0 3.3 3.6 4.1 3.4 2.3 2.3 p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 CSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A													
p0 queue free % 99 100 100 98 100 97 100 98 cM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2		3.5	4.0	3.3	3.6	4.1	3.4	2.3			2.3		
CM capacity (veh/h) 356 376 766 370 373 689 1265 1186 Direction, Lane # EB 1 WB 1 NB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 CSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach LOS C B Intersection Summary Average Delay								100			98		
Direction, Lane # EB 1 WB 1 NB 2 SB 1 SB 2 Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A							689	1265			1186		
Volume Total 5 26 341 11 18 275 Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A					NR 2	SB 1	SB 2	-	00000	- T-	- 75		-
Volume Left 5 7 1 0 18 0 Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B A A Intersection Summary Average Delay 0.8 ICU Level of Service A													
Volume Right 0 18 0 11 0 5 cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A													
cSH 356 546 1265 1700 1186 1700 Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization 30.5% ICU Level of Service A				-									
Volume to Capacity 0.01 0.05 0.00 0.01 0.02 0.16 Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay Intersection Capacity Utilization Output Outp													
Queue Length 95th (m) 0.3 1.2 0.0 0.0 0.4 0.0 Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay 0.8 Intersection Capacity Utilization 30.5% ICU Level of Service A													
Control Delay (s) 15.3 11.9 0.0 0.0 8.1 0.0 Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay 0.8 Intersection Capacity Utilization 30.5% ICU Level of Service A													
Lane LOS C B A A Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay 0.8 Intersection Capacity Utilization 30.5% ICU Level of Service A													
Approach Delay (s) 15.3 11.9 0.0 0.5 Approach LOS C B Intersection Summary Average Delay 0.8 Intersection Capacity Utilization 30.5% ICU Level of Service A					0.0		0.0						
Approach LOS C B Intersection Summary Average Delay 0.8 Intersection Capacity Utilization 30.5% ICU Level of Service A													
Intersection Summary Average Delay Intersection Capacity Utilization 0.8 ICU Level of Service A				U.U		0.0							
Average Delay 0.8 Intersection Capacity Utilization 30.5% ICU Level of Service A								-11	Section				
Intersection Capacity Utilization 30.5% ICU Level of Service A			110	Λ 9									
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	raidiyolo r ollou (Illili)												

	*	→	•	•	←	4	1	†	1	1	↓	1
Movement	EBL	EBT	EBR	WEL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			7		4	^	7			
Volume (veh/h)	10	7	0	0	4	3	12	399	0	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	11	8	0	0	5	3	14	453	0	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	260	481	0	485	481	227	0			453		
vC1, stage 1 conf vol										-		
vC2, stage 2 conf vol												
vCu, unblocked vol	260	481	0	485	481	227	0			453		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7.0	4.3			4.1		
tC, 2 stage (s)												
tF(s)	3.6	4.0	3.4	3.6	4.0	3.4	2.3			2.2		
p0 queue free %	98	98	100	100	99	100	99			100		
cM capacity (veh/h)	652	473	1075	450	473	767	1552			1104		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	19	8	14	227	227	0		177				
Volume Left	11	0	14	0	0	0						
Volume Right	0	3	0	0	0	0						
cSH	564	566	1552	1700	1700	1700						
Volume to Capacity	0.03	0.01	0.01	0.13	0.13	0.00						
Queue Length 95th (m)	0.9	0.3	0.2	0.0	0.0	0.0						
Control Delay (s)	11.6	11.5	7.3	0.0	0.0	0.0						
Lane LOS	В	В	Α	0.1011		0.0						
Approach Delay (s)	11.6	11.5	0.2									
Approach LOS	В	В	-						-			
Intersection Summary								8 N T		WIE SEII		
Average Delay			0.8									
Intersection Capacity Utilizat	ion		26.3%	10	U Level o	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4			4	
Volume (veh/h)	0	15	0	0	19	5	0	0	0	4	0	1
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	17	0	0	22	6	0	0	0	5	0	1
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	27			17			43	44	17	41	41	24
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	27			17			43	44	17	41	41	24
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.2	6.6	6.3
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3,3	3.6	4.1	3.4
p0 queue free %	100			100			100	100	100	100	100	100
cM capacity (veh/h)	1567			1581			959	847	1062	942	835	1029
Direction, Lane #	EB 1	WB 1	NB 1	SB 1						- 1		
Volume Total	17	27	0	6								
Volume Left	0	0	0	5								
Volume Right	0	6	0	1								
cSH	1567	1581	1700	958								
Volume to Capacity	0.00	0.00	0.00	0.01								
Queue Length 95th (m)	0.0	0.0	0.0	0.1								
Control Delay (s)	0.0	0.0	0.0	8.8								
Lane LOS			Α	Α								
Approach Delay (s)	0.0	0.0	0.0	8.8								
Approach LOS			Α	Α								
Intersection Summary			- "									
Average Delay			1.0									
Intersection Capacity Utiliz Analysis Period (min)	ation			10	CU Level o	of Service			Α			
	ation		13.3% 15	- 10	CU Level o	of Service			A			

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		^	7		र्स					4	^	7
Volume (veh/h)	0	14	5	1	15	0	0	0	0	3	198	9
Sign Control		Stop			Yield			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	16	6	1	17	0	0	0	0	3	225	10
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)			2									
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	240	232	112	130	242	0	235			0		
vC1, stage 1 conf vol			_									
vC2, stage 2 conf vol												
vCu, unblocked vol	240	232	112	130	242	0	235			0		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7.0	4.1			4.3		
tC, 2 stage (s)												
tF (s)	3.6	4.0	3.4	3.6	4.0	3.4	2.2			2.3		
p0 queue free %	100	98	99	100	97	100	100			100		
cM capacity (veh/h)	671	659	909	799	650	1075	1329			1552		
Direction, Lane#	EB 1	WB 1	SB 1	SB 2	SB 3	SB 4						
Volume Total	22	18	3	112	112	10			_	_		
Volume Left	0	1	3	0	0	0						
Volume Right	6	0	0	0	0	10						
cSH	894	658	1552	1700	1700	1700						
Volume to Capacity	0.02	0.03	0.00	0.07	0.07	0.01						
Queue Length 95th (m)	0.02	0.03	0.00	0.07	0.0	0.01						
Control Delay (s)	10.2	10.6	7.3	0.0	0.0	0.0						
Lane LOS	10.2 B	В	7.3 A	0.0	0.0	0.0						
Approach Delay (s)	10.2	10.6	0.1						14			
			0.1									
Approach LOS	В	В										
Intersection Summary			4.0									
Average Delay	41		1.6		411							
Intersection Capacity Utiliza	tion		22.6%	10	U Level c	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			र्स	7	7	Þ	
Volume (veh/h)	4	2	0	9	3	23	- 0	231	2	30	283	7
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	- 5	2	0	10	3	26	0	262	2	34	322	8
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	684	659	326	653	660	262	330			265		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	684	659	326	653	660	262	330			265		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)		0.0				•						
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	99	99	100	97	99	97	100			97		
cM capacity (veh/h)	341	374	716	370	372	774	1224			1293		
	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2		_				
Direction, Lane #				2	34	330	_			_		
Volume Total	7	40	262									
Volume Left	5	10	0	0	34	0						
Volume Right	0	26	0	2	0	4700						
cSH	351	563	1224	1700	1293	1700						
Volume to Capacity	0.02	0.07	0.00	0.00	0.03	0.19						
Queue Length 95th (m)	0.5	1.8	0.0	0.0	0.6	0.0						
Control Delay (s)	15.5	11.9	0.0	0.0	7.9	0.0						
Lane LOS	С	В			A							-
Approach Delay (s)	15.5	11.9	0.0		0.7							
Approach LOS	С	В										
Intersection Summary												
Average Delay			1.3									
Intersection Capacity Utilizati	on		37.1%	10	CU Level	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		सी			4		ሻ	^	7			
Volume (veh/h)	4	5	0	0	2	6	13	279	1	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	6	0	0	2	7	15	317	1	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)											.,,,,,,	
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	196	348	0	349	347	159	0			318		
vC1, stage 1 conf vol				0.0		100				010		
vC2, stage 2 conf vol												
vCu, unblocked vol	196	348	0	349	347	159	0			318		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.4			4.1		
tC, 2 stage (s)	1.0	0.0	7.0	7.0	0.0	0.0	100			41.1		
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	99	99	100	100	100	99	99			100		
cM capacity (veh/h)	724	562	1075	572	570	859	1538			1239		
							1000			1200		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	10	9	15	159	159	1						
Volume Left	5	0	15	0	0	0						
Volume Right	0	7	0	0	0	1						
cSH	624	762	1538	1700	1700	1700						
Volume to Capacity	0.02	0.01	0.01	0.09	0.09	0.00						
Queue Length 95th (m)	0.4	0.3	0.2	0.0	0.0	0.0						
Control Delay (s)	10.9	9.8	7.4	0.0	0.0	0.0						
Lane LOS	В	Α	Α									
Approach Delay (s)	10.9	9.8	0.3									
Approach LOS	В	Α										
Intersection Summary								5.	350			
Average Delay			0.9									
Intersection Capacity Utilization	no		19.2%	IC	U Level o	f Service			Α			
Analysis Period (min)			15									

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1 0.88	EBT 21 Free	EBR 0	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SET	SBR
	21 Free	0		_		The second second		MOIX	ODL		ODR
	Free	0		4			4			4	
0.88			0	17	1	0	0	0	5	0	0
0.88				Free			Stop			Stop	
0.88	0%			0%			0%			0%	
0.00	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
1	24	0	0	19	1	0	0	0	6	0	0
	None			None							
20			24			46	47	24	46	46	20
20			24			46	47	24			20
4.1			4.1			7.1	6.5	6.2	7.2	6.6	6.3
2.2			2.2			3.5	4.0				3.4
100			100								100
1576			1572			955	844	1053	935	830	1035
EB 1	WB 1	NB 1	SB 1				- 10	115	11,10	2	
25	20	0	6								
1	0	0	6								
0	1	0	0								
1576	1572	1700	935								
0.00	0.00	0.00									
0.0	0.0	0.0	0.1								
0.3	0.0	0.0	8.9								
Α		Α									
0.3	0.0	0.0	8.9								
		Α	Α								
n			- IC	CU Level o	f Service			Α			
		15									
	20 4.1 2.2 100 1576 EB 1 25 1 0 1576 0.00 0.0 0.3 A	20 20 4.1 2.2 100 1576 EB 1 WB 1 25 20 1 0 0 1 1576 1572 0.00 0.00 0.0 0.0 0.3 0.0 A 0.3 0.0	None 20 20 4.1 2.2 100 1576 EB 1 WB 1 NB 1 25 20 0 1 0 0 0 1 0 1576 1572 1700 0.00 0.00 0.00 0.0 0.0 0.0 0.0 0.0 0.	None 20 24 20 24 4.1 2.2 100 1576 1572 EB 1 WB 1 NB 1 SB 1 25 20 0 6 1 0 0 6 0 1 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.0 0.01 0.0 0.0 0.0 0.0 0.1 0.3 0.0 0.0 8.9 A A A 31.2 31.33% 10	None None 20 24 20 24 4.1 4.1 2.2 2.2 100 100 1576 1572 EB 1 WB 1 NB 1 SB 1 25 20 0 6 1 0 0 6 0 1 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.01 0.3 0.0 0.0 8.9 A A A 0.3 0.0 0.0 8.9 A A A 1.2 1.2 13.3% ICU Level o	None None 20 24 20 24 4.1 4.1 2.2 2.2 100 100 1576 1572 EB 1 WB 1 NB 1 SB 1 25 20 0 6 1 0 0 6 0 1 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.0 0.1 0.3 0.0 0.0 8.9 A A A A 0.3 0.0 0.0 8.9 A A A 1.2 13.3% ICU Level of Service	None None 20 24 46 20 24 46 4.1 4.1 7.1 2.2 2.2 3.5 100 100 100 100 1576 1572 955 EB 1 WB 1 NB 1 SB 1 25 20 0 6 1 0 0 6 0 1 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.01 0.0 0.0 0.0 0.01 0.3 0.0 0.0 8.9 A A A O.3 0.0 0.0 8.9 A A A A 1.2 1.2 13.3% ICU Level of Service	None None 20 24 46 47 20 24 46 47 4.1 4.1 7.1 6.5 2.2 2.2 3.5 4.0 100 100 100 100 100 1576 1572 955 844 EB 1 WB 1 NB 1 SB 1 25 20 0 6 1 0 0 6 0 1 0 0 6 0 1 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.01 0.0 0.0 0.0 0.1 0.3 0.0 0.0 8.9 A A A 0.3 0.0 0.0 8.9 A A A 1.2 1.2 13.3% ICU Level of Service	None None 20 24 46 47 24 20 24 46 47 24 4.1 4.1 7.1 6.5 6.2 2.2 2.2 3.5 4.0 3.3 100 100 100 100 100 100 1576 1572 955 844 1053 EB 1 WB 1 NB 1 SB 1 25 20 0 6 1 0 0 6 0 1 0 0 6 0 1 0 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.01 0.3 0.0 0.0 8.9 A A A 0.3 0.0 0.0 8.9 A A A 1.2 1.2 1.2 1.3.3% ICU Level of Service A	None None 20 24 46 47 24 46 20 24 46 47 24 46 4.1 4.1 7.1 6.5 6.2 7.2 2.2 2.2 3.5 4.0 3.3 3.6 100 100 100 100 100 100 99 1576 1572 955 844 1053 935 EB1 WB1 NB1 SB1 25 20 0 6 1 0 0 6 0 1 0 0 6 0 1 0 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.01 0.0 0.0 0.0 0.01 0.0 0.0 0.0 8.9 A A A O.3 0.0 0.0 8.9 A A A A 1.2 1.2 1.2 1.2 1.3.3% ICU Level of Service A	None None 20 24 46 47 24 46 46 20 24 46 47 24 46 46 4.1 4.1 7.1 6.5 6.2 7.2 6.6 2.2 2.2 3.5 4.0 3.3 3.6 4.1 100 100 100 100 100 100 99 100 1576 1572 955 844 1053 935 830 EB1 WB1 NB1 SB1 25 20 0 6 1 0 0 6 0 1 0 0 6 0 1 0 0 0 1576 1572 1700 935 0.00 0.00 0.00 0.01 0.0 0.0 0.0 0.01 0.3 0.0 0.0 8.9 A A A O.3 0.0 0.0 8.9 A A A O.3 0.0 0.0 8.9 A A A ICU Level of Service A

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		^	7		4					ħ	^	7
Volume (veh/h)	0	9	17	0	15	0	0	0	0	0	308	3
Sign Control		Stop			Yield			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	10	19	0	17	0	0	0	0	0	350	3
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)			2									
Median type								None			None	
Median storage veh)								110110			110110	
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	359	350	175	190	353	0	353			0		
vC1, stage 1 conf vol		000	110	100	000		000					
vC2, stage 2 conf vol												
vCu, unblocked vol	359	350	175	190	353	0	353			0		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.1			4.4		
tC, 2 stage (s)		0.0	1.0	7.0	0.0	0.0	7.1			7.7		
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.2			2.3		
p0 queue free %	100	98	98	100	97	100	100			100		
cM capacity (veh/h)	552	566	829	725	570	1084	1202			1538		
							1202			1000		
Direction, Lane #	EB 1	WB 1	SB 1	SB 2	SB 3	SB 4						
Volume Total	30	17	0	175	175	3						
Volume Left	0	0	0	0	0	0						
Volume Right	19	0	0	0	0	3						
cSH	1267	570	1700	1700	1700	1700						
Volume to Capacity	0.02	0.03	0.00	0.10	0.10	0.00						
Queue Length 95th (m)	0.6	0.7	0.0	0.0	0.0	0.0						
Control Delay (s)	10.2	11.5	0.0	0.0	0.0	0.0						
Lane LOS	В	В										
Approach Delay (s)	10.2	11.5	0.0									
Approach LOS	В	В									(1)	
Intersection Summary		1										
Average Delay			1.2									
Intersection Capacity Utiliza	tion		25.9%	IC	U Level c	f Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4	7	*	\$	
Volume (veh/h)	4	0	0	6	1	17	1	320	11	17	255	4
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	0	0	7	-1	19	1	364	12	19	290	5
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	716	709	292	694	699	364	294			376		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	716	709	292	694	699	364	294			376		
tC, single (s)	7.1	6.5	6.2	7.2	6.6	6.3	4.2			4.2		
tC, 2 stage (s)												
tF(s)	3.5	4.0	3.3	3.6	4.1	3.4	2.3			2.3		
p0 queue free %	99	100	100	98	100	97	100			98		
cM capacity (veh/h)	330	353	747	344	350	668	1245			1161		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2	البال					" 1
Volume Total	5	27	365	12	19	294						
Volume Left	5	7	1	0	19	0						
Volume Right	0	19	0	12	0	5						
cSH	330	525	1245	1700	1161	1700						
Volume to Capacity	0.01	0.05	0.00	0.01	0.02	0.17						
Queue Length 95th (m)	0.3	1.3	0.0	0.0	0.4	0.0						
Control Delay (s)	16.1	12.2	0.0	0.0	8.2	0.0						
Lane LOS	С	В	Α		Α							
Approach Delay (s)	16.1	12.2	0.0		0.5							
Approach LOS	С	В										
Intersection Summary								H = 97. H				
Average Delay			8.0									
Intersection Capacity Utilizat Analysis Period (min)	ion		31.5% 15	10	U Level	of Service			Α			
Analysis renod (min)			10									

	*	-	*	•	4-	•	1	†	-	1	ļ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ની			1		N.	44	7			
Volume (veh/h)	10	7	0	0	4	3	12	415	0	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	11	8	0	0	5	3	14	472	0	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	269	499	0	503	499	236	0			472		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	269	499	0	503	499	236	0			472		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7.0	4.3			4.1		
tC, 2 stage (s)												
tF (s)	3.6	4.0	3.4	3.6	4.0	3.4	2.3			2.2		
p0 queue free %	98	98	100	100	99	100	99			100		
cM capacity (veh/h)	642	461	1075	436	461	757	1552			1087		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	19	8	14	236	236	0					11/41	T.
Volume Left	11	0	14	0	0	0						
Volume Right	0	3	0	0	0	0						
cSH	553	554	1552	1700	1700	1700						
Volume to Capacity	0.03	0.01	0.01	0.14	0.14	0.00						
Queue Length 95th (m)	0.9	0.3	0.2	0.0	0.0	0.0						
Control Delay (s)	11.7	11.6	7.3	0.0	0.0	0.0						
Lane LOS	В	В	Α	3.17		0.0						
Approach Delay (s)	11.7	11.6	0.2									
Approach LOS	В	В										
Intersection Summary												
Average Delay			0.8									
Intersection Capacity Utiliza	tion		26.8%	IC	U Level o	f Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations		4	₽		N/N		
Volume (veh/h)	0	15	19	5	4	1	
Sign Control	_	Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	
Hourly flow rate (vph)	0	17	22	6	5	1	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)		110110	110110				
Upstream signal (m)							
pX, platoon unblocked							
vC, conflicting volume	27				41	24	
vC1, stage 1 conf vol	LI				-11		
vC2, stage 2 conf vol							
vCu, unblocked vol	27				41	24	
	4.1				6.5	6.3	
tC, single (s)	4.1				0.0	0.0	
tC, 2 stage (s)	2.2				3.6	3.4	
tF (s)	100				100	100	
p0 queue free %					950	1029	
cM capacity (veh/h)	1567				950	1029	
Direction, Lane #	EB 1	WB 1	SB 1				
Volume Total	17	27	6				
Volume Left	0	0	5				
Volume Right	0	6	1				
cSH	1567	1700	965				
Volume to Capacity	0.00	0.02	0.01				
Queue Length 95th (m)	0.0	0.0	0.1				
Control Delay (s)	0.0	0.0	8.8				
Lane LOS			Α				
Approach Delay (s)	0.0	0.0	8.8				
Approach LOS			Α				
Intersection Summary		V	- 1111				
Average Delay			1.0				
Intersection Capacity Utiliz	zation		13.3%	10	CU Level	of Service	
Analysis Period (min)			15				

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		^	7		र्स					7	ተ ተ	7
Volume (veh/h)	0	14	5	1	15	0	0	0	0	3	206	9
Sign Control		Stop			Yield			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	16	6	1	17	0	0	0	0	3	234	10
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)			2									
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	249	241	117	135	251	0	244			0		
vC1, stage 1 conf vol						_						
vC2, stage 2 conf vol												
vCu, unblocked vol	249	241	117	135	251	0	244			0		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7.0	4.1			4.3		
tC, 2 stage (s)										7/1		
tF (s)	3.6	4.0	3.4	3.6	4.0	3.4	2.2			2.3		
p0 queue free %	100	98	99	100	97	100	100			100		
cM capacity (veh/h)	661	651	903	793	642	1075	1319			1552		
Direction, Lane #	EB 1	WB 1	SB 1	SB 2	SB 3	SB 4						
Volume Total	22	18	3	117	117	10						
Volume Left	0	1	3	0	0	0						
Volume Right	6	0	0	0	0	10						
cSH	884	650	1552	1700	1700	1700						
Volume to Capacity	0.02	0.03	0.00	0.07	0.07	0.01						
Queue Length 95th (m)	0.6	0.7	0.1	0.0	0.0	0.0						
Control Delay (s)	10.2	10.7	7.3	0.0	0.0	0.0						
Lane LOS	В	В	Α									
Approach Delay (s)	10.2	10.7	0.1									
Approach LOS	В	В										
Intersection Summary								1.7		100	. V	- " -
Average Delay			1.5									
Intersection Capacity Utiliza	tion		22.8%	IC	U Level o	f Service			Α			
Analysis Period (min)			15									
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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4			4	7	7	₽	
Volume (veh/h)	4	2	0	9	3	24	0	247	2	32	303	7
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	2	0	10	3	27	0	281	2	36	344	8
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	731	704	348	699	706	281	352			283		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	731	704	348	699	706	281	352			283		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	99	99	100	97	99	96	100			97		
cM capacity (veh/h)	316	351	695	344	349	756	1201			1274		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2			1100	11.33110		, 1º,
Volume Total	7	41	281	2	36	352						
Volume Left	5	10	0	0	36	0						
Volume Right	0	27	0	2	0	8						
cSH	327	541	1201	1700	1274	1700						
Volume to Capacity	0.02	0.08	0.00	0.00	0.03	0.21						
Queue Length 95th (m)	0.5	2.0	0.0	0.0	0.7	0.0						
Control Delay (s)	16.3	12.2	0.0	0.0	7.9	0.0						
Lane LOS	С	В			Α							
Approach Delay (s)	16.3	12.2	0.0		0.7							
Approach LOS	С	В										
Intersection Summary							HLIC					1
Average Delay			1.2									
Intersection Capacity Utilizat	tion		38.9%	IC	U Level	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			7		N.	^	7			
Volume (veh/h)	4	5	0	0	2	6	14	290	1	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	6	0	0	2	7	16	330	1	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	205	362	0	364	361	165	0			331		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	205	362	0	364	361	165	0			331		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.4			4.1		
tC, 2 stage (s)												
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	99	99	100	100	100	99	99			100		
cM capacity (veh/h)	713	551	1075	558	559	851	1538			1226		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	10	9	16	165	165	1	-				_	
Volume Left	5	0	16	0	100	0						
	0	7	0	0	0	1						
Volume Right cSH	613	752	1538	1700	1700	1700						
	0.02											
Volume to Capacity		0.01	0.01	0.10	0.10	0.00						
Queue Length 95th (m)	0.4	0.3	0.3	0.0	0.0	0.0						
Control Delay (s)	11.0	9.8	7.4	0.0	0.0	0.0						
Lane LOS	B	A	A									
Approach Delay (s)	11.0	9.8	0.3									
Approach LOS	В	Α										
Intersection Summary		تبدي										
Average Delay			0.9									
Intersection Capacity Utiliza	tion		19.5%	IC	CU Level o	of Service			_ A			
Analysis Period (min)			15									

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Movement	EBL	EBT	WBT	WBR	SBL	SBR			
Lane Configurations		र्स	1		W				
Volume (veh/h)	1	22	18	1	5	0			
Sign Control		Free	Free		Stop				
Grade		0%	0%		0%				
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88			
Hourly flow rate (vph)	1	25	20	1	6	0			
Pedestrians									
Lane Width (m)									
Walking Speed (m/s)									
Percent Blockage									
Right turn flare (veh)									
Median type		None	None						
Median storage veh)		,,,,,,,,							
Upstream signal (m)									
pX, platoon unblocked									
vC, conflicting volume	22				48	21			
C1, stage 1 conf vol					,,,				
C2, stage 2 conf vol									
Cu, unblocked vol	22				48	21			
C, single (s)	4.1				6.5	6.3			
C, 2 stage (s)	7.1				0.0	0.0			
tF (s)	2.2				3.6	3.4			
o0 queue free %	100				99	100			
cM capacity (veh/h)	1575				941	1034			
ow capacity (ven/n)	10/0				341	1034			
Direction, Lane #	EB 1	WB 1	SB 1						
/olume Total	26	22	6						
Volume Left	1	0	6						
/olume Right	0	1	0						
SH	1575	1700	941						
Volume to Capacity	0.00	0.01	0.01						
Queue Length 95th (m)	0.0	0.0	0.1						
Control Delay (s)	0.3	0.0	8.9						
ane LOS	Α		Α						
Approach Delay (s)	0.3	0.0	8.9						
Approach LOS			Α						
Intersection Summary							 100		
Average Delay			1.1						
Intersection Capacity Utilizat	tion		13.3%	IC	U Level o	of Service		Α	
Analysis Period (min)			15						

9 Stop 0% 0.88 10	18 0.88 20 2	0 0.88 0	16 Yield 0% 0.88 18	0 0.88 0	0 0.88 0	0 Free 0% 0.88 0	0 0.88 0	0 0.88 0	320 Free 0% 0.88 364	
9 Stop 0% 0.88 10	0.88 20	0.88	16 Yield 0% 0.88	0.88	0.88	Free 0% 0.88 0	0.88	0.88	320 Free 0% 0.88 364	0.88
Stop 0% 0.88 10	0.88	0.88	Yield 0% 0.88	0.88	0.88	Free 0% 0.88 0	0.88	0.88	Free 0% 0.88 364	0.88
0% 0.88 10	20		0% 0.88			0% 0.88 0			0% 0.88 364	
0.88 10	20		0.88			0.88			0.88 364	
10	20					0			364	0.88
	2	0	18	0	0		0	0		3
364						None			None	
364						None			None	
364						None			None	
364						None			None	
364						None			None	
364	400					None			None	
364	400								INOTIE	
364	400									
364	400									
364	400									
	102	197	367	0	367			0		
			•••							
364	182	197	367	0	367			0		
6.6	7.0	7.5	6.5	6.9	4.1			4.4		
4.0	3.4	3.5	4.0	3.3	2.2			2.3		
98	98	100	97	100	100			100		
556	820	715	560	1084	1188			1538		
WB 1	SE 1	SB 2	SB 3	SB 4			100			
18	0	182	182	3	_					
	_									
	0.0	0.0	0.0	0.0						
	0.0									
В	0.0									
									IIW e	
	1.3									
	26.3%	IC	U Level o	of Service			Α			
	15									
	0 560 0.03 0.8 11.6 B	0 0 0 0 560 1700 0.03 0.00 0.8 0.0 11.6 0.0 B 11.6 0.0 B	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 3 560 1700 1700 1700 1700 0.03 0.00 0.11 0.11 0.00 0.8 0.0 0.0 0.0 0.0 0.0 11.6 0.0 0.0 0.0 0.0 B 11.6 0.0 B 11.3 26.3% ICU Level of Service	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 3 560 1700 1700 1700 1700 1700 1700 0.03 0.00 0.11 0.11 0.00 0.0 0.0 11.6 0.0 0.0 0.0 0.0 0.0 B 11.6 0.0 B 11.6 0.0 B II.6 D.0	0 0 0 0 0 0 3 560 1700 1700 1700 1700 0.03 0.00 0.11 0.11 0.00 0.8 0.0 0.0 0.0 0.0 0.0 11.6 0.0 0.0 0.0 0.0 B 11.6 0.0 B 11.8 0.0 B 11.8 A 1.8 A	0 0 0 0 0 0 3 560 1700 1700 1700 1700 0.03 0.00 0.11 0.11 0.00 0.8 0.0 0.0 0.0 0.0 0.0 11.6 0.0 0.0 0.0 0.0 B 11.6 0.0 B 11.8 0.0 CU Level of Service	0 0 0 0 0 3 560 1700 1700 1700 1700 0.03 0.00 0.11 0.11 0.00 0.8 0.0 0.0 0.0 0.0 11.6 0.0 0.0 0.0 0.0 B 11.6 0.0 B 11.3 26.3% ICU Level of Service A

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SET	SBR
Lane Configurations		4			र्स	7		बी	7	19	Þ	
Volume (veh/h)	4	0	0	13	1	37	1	299	44	119	238	4
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	0	0	15	1	42	1	340	50	135	270	5
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)						4						
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	907	935	273	883	887	340	275			390		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	907	935	273	883	887	340	275			390		
tC, single (s)	7.1	6.5	6.2	7.2	6.6	6.3	4.2			4.2		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.6	4.1	3.4	2.3			2.3		
p0 queue free %	98	100	100	94	100	94	100			88		
cM capacity (veh/h)	218	234	766	236	244	689	1265			1147		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	5	58	341	50	135	275						
Volume Left	5	15	1	0	135	0						
Volume Right	0	42	0	50	0	5						
cSH	218	863	1265	1700	1147	1700						
Volume to Capacity	0.02	0.07	0.00	0.03	0.12	0.16						
Queue Length 95th (m)	0.5	1.7	0.0	0.0	3.2	0.0						
Control Delay (s)	21.8	13.5	0.0	0.0	8.6	0.0						
Lane LOS	С	В	Α		Α							
Approach Delay (s)	21.8	13.5	0.0		2.8							
Approach LOS	С	В										
Intersection Summary										"		
Average Delay			2.4									
Intersection Capacity Utilization	n		44.6%	IC	U Level	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્ન			ĵ.		ሻ	^	7			
Volume (veh/h)	95	14	0	0	38	3	115	399	0	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	108	16	0	0	43	3	131	453	0	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	513	715	0	723	715	227	0			453		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	513	715	0	723	715	227	0			453		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7:0	4.3			4.1		
tC, 2 stage (s)		3.0			0.0	,,,	.,,,					
tF (s)	3.6	4.0	3.4	3.6	4.0	3.4	2.3			2.2		
p0 queue free %	70	95	100	100	86	100	92			100		
cM capacity (veh/h)	366	320	1075	278	320	767	1552			1104		
Direction, Lane #	E8 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	124	47	131	227	227	0						_
Volume Left	108	0	131	0	0	0						
Volume Right	0	3	0	0	0	0						
cSH	359	334	1552	1700	1700	1700						
Volume to Capacity	0.34	0.14	0.08	0.13	0.13	0.00						
Queue Length 95th (m)	12.0	3.8	2.2	0.0	0.0	0.0						
Control Delay (s)	20.2	17.5	7.5	0.0	0.0	0.0						
Lane LOS	C	17.5 C	Α.	0.0	0.0	0.0						
Approach Delay (s)	20.2	17.5	1.7									
Approach LOS	C	C	1.1									
Intersection Summary	V 10.											
Average Delay			5.7									
Intersection Capacity Utilizat	ion		31.8%	IC	ll l evel d	of Service			Α			
Analysis Period (min)			15	10	O LOVOI (, OCI AIDC						
rinary or or or or (min)			10									

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Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	15	1	†	74	N/F		
Volume (veh/h)	138	15	18	556	117	29	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	
Hourly flow rate (vph)	157	17	20	632	133	33	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)		110110	110110				
Upstream signal (m)							
pX, platoon unblocked							
vC, conflicting volume	652				351	20	
vC1, stage 1 conf vol	002				301	20	
vC2, stage 2 conf vot	652				351	20	
vCu, unblocked vol	4.1				6.5	6.3	
tC, single (s)	4.1				0.0	0.5	
tC, 2 stage (s)	0.0				3.6	3.4	
:F (s)	2.2				75	97	
p0 queue free %	83				523		
cM capacity (veh/h)	920				523	1035	
Direction, Lane #	EB 1	EB 2	WB 1	WB 2	SB 1		10-11-12-22
Volume Total	157	17	20	632	166		
Volume Left	157	0	0	0	133		
Volume Right	0	- 0	0	632	33		
cSH	920	1700	1700	1700	580		
Volume to Capacity	0.17	0.01	0.01	0.37	0.29		
Queue Length 95th (m)	4.9	0.0	0.0	0.0	9.4		
Control Delay (s)	9.7	0.0	0.0	0.0	13.7		
Lane LOS	Α				В		
Approach Delay (s)	8.8		0.0		13.7		
Approach LOS			- i		В		
Intersection Summary							**
Average Delay			3.8				
Intersection Capacity Utilizat	tion		52.3%	IC	U Level	of Service	Α
Analysis Period (min)			15				

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		†	7		ર્ન					7	ተ ተ	7
Volume (veh/h)	0	106	26	1	152	0	0	0	0	3	198	422
Sign Control		Stop			Yield			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	120	30	1	173	0	0	0	0	3	225	480
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)			2									
Median type								None			None	
Median storage veh)								,,,,,,,			,,,,,,,	
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	318	232	112	194	711	0	705			0		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	318	232	112	194	711	0	705			0		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7.0	4.1			4.3		
tC, 2 stage (s)										1,,0		
tF (s)	3.6	4.0	3.4	3.6	4.0	3.4	2.2			2.3		
p0 queue free %	100	82	97	100	51	100	100			100		
cM capacity (veh/h)	369	659	909	614	350	1075	889			1552		
Direction, Lane#	EB 1	WB 1	SB 1	SB 2	SB 3	SB 4				1002		
Volume Total	150	174	3	112	112	480	_					
Volume Left	0	174	3	0	0	0						
Volume Right	30	0	0	0	0	480						
cSH	820	351	1552		1700	1700						
Volume to Capacity	0.18	0.50	0.00	1700 0.07	0.07	0.28						
Queue Length 95th (m)	5.3	21.1	0.00	0.0	0.07	0.28						
Control Delay (s)	11.2	24.9	7.3	0.0	0.0							
Lane LOS	11.2 B	24.9 C	7.3 A	0.0	0.0	0.0						
	11.2	24.9	0.0									
Approach Delay (s) Approach LOS	11.Z B	24.9 C	0.0									
	D	C										
Intersection Summary								12				
Average Delay			5.9	10								
Intersection Capacity Utilizatio Analysis Period (min)	n		43.8% 15	IC	U Level o	f Service			Α			
			16									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			4	7		લી	7	M	₽	
Volume (veh/h)	4	2	0	40	3	117	0	231	11	56	283	7
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	2	0	45	3	133	0	262	12	64	322	8
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)						4						
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	784	728	326	712	719	262	330			275		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	784	728	326	712	719	262	330			275		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	98	99	100	86	99	83	100			95		
cM capacity (veh/h)	246	333	716	331	335	774	1224			1282		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2						
Volume Total	7	182	262	12	64	330						
Volume Left	5	45	0	0	64	0						
Volume Right	0	133	0	12	0	8						
cSH	269	1058	1224	1700	1282	1700						
Volume to Capacity	0.03	0.17	0.00	0.01	0.05	0.19						
Queue Length 95th (m)	0.6	5.0	0.0	0.0	1.3	0.0						
Control Delay (s)	18.7	12.5	0.0	0.0	8.0	0.0						
Lane LOS	С	В			Α							
Approach Delay (s)	18.7	12.5	0.0		1.3							
Approach LOS	С	В										
Intersection Summary									X 331 E U			
Average Delay			3.4									
Intersection Capacity Utiliza	ntion		43.8%	IC	U Level	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્ન			1>		ሻ	个 个	7			
Volume (veh/h)	379	36	0	0	11	6	39	279	1	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	431	41	0	0	12	7	44	317	1	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)								710110			Hono	
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	260	407	0	426	406	159	0			318		
vC1, stage 1 conf vol					100	100				010		
vC2, stage 2 conf vol												
vCu, unblocked vol	260	407	0	426	406	159	0			318		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.4			4.1		
tC, 2 stage (s)	110	0.0	110	1.0	0.0	0.0	-11			7.1		
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	32	92	100	100	98	99	97			100		
cM capacity (veh/h)	632	510	1075	470	518	859	1538			1239		
							1000	- "		1233		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	472	19	44	159	159	1						
Volume Left	431	0	44	0	0	0						
Volume Right	0	7	- 0	0	0	1						
cSH	619	602	1538	1700	1700	1700						
Volume to Capacity	0.76	0.03	0.03	0.09	0.09	0.00						
Queue Length 95th (m)	55.6	0.8	0.7	0.0	0.0	0.0						
Control Delay (s)	26.9	11.2	7.4	0.0	0.0	0.0						
Lane LOS	D	В	Α									
Approach Delay (s)	26.9	11.2	0.9									
Approach LOS	D	В										
Intersection Summary			عليظ									
Average Delay			15.5									
Intersection Capacity Utilizat	ion		46.6%	IC	U Level o	f Service			Α			
Analysis Period (min)			15									
anaryolo i onou (ililii)			10									

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Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	19	^	†	7	N/F	
Volume (veh/h)	36	21	17	142	505	125
Sign Control		Free	Free		Stop	
Grade		0%	0%		0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	41	24	19	161	574	142
Pedestrians	•					
Lane Width (m)						
Walking Speed (m/s)						
Percent Blockage						
Right turn flare (veh)						
Median type		None	None			
Median type Median storage veh)		INOTIC	INOUG			
Upstream signal (m)						
pX, platoon unblocked	181				125	19
vC, conflicting volume	101				120	13
vC1, stage 1 conf vol						
vC2, stage 2 conf vol	404				405	40
vCu, unblocked vol	181				125	19
tC, single (s)	4.1				6.5	6.3
tC, 2 stage (s)						
tF (s)	2.2				3.6	3.4
p0 queue free %	97				31	86
cM capacity (veh/h)	1377				826	1036
Direction, Lane #	EB 1	EB 2	WB 1	WB 2	SB 1	
Volume Total	41	24	19	161	716	
Volume Left	41	0	0	0	574	
Volume Right	0	0	0	161	142	
cSH	1377	1700	1700	1700	860	
Volume to Capacity	0.03	0.01	0.01	0.09	0.83	
Queue Length 95th (m)	0.7	0.0	0.0	0.0	77.4	
Control Delay (s)	7.7	0.0	0.0	0.0	26.1	
Lane LOS	Α				D	
Approach Delay (s)	4.9		0.0		26.1	
Approach LOS					D	
Intersection Summary					1	
Average Delay			19.8			
Intersection Capacity Utiliza	ation		54.2%	IC	U Level	of Service
Analysis Period (min)			15			
ranaryolo i onou (iliii)						

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		†	7		र्स					1/2	十 十	7
Volume (veh/h)	0	415	111	0	50	0	0	0	0	0	308	109
Sign Control		Stop			Yield			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	472	126	0	57	0	0	0	0	0	350	124
Pedestrians												ν
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)			2									
Median type								None			None	
Median storage veh)								110110			110110	
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	378	350	175	474	474	0	474			0		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	378	350	175	474	474	0	474			0		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.1			4.4		
tC, 2 stage (s)		0.0	7.0	1.0	0.0	0.0				-11-7		
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.2			2.3		
p0 queue free %	100	17	85	100	88	100	100			100		
cM capacity (veh/h)	498	566	829	121	488	1084	1084			1538		
Direction, Lane #	EB 1	WB 1	SB 1	SB 2	SB 3	SB 4	1007			1000		
Volume Total	598	100000						_				
		57	0	175	175	124						
Volume Left	0	0	0	0	0	0						
Volume Right	126	0	0	0	0	124						
cSH	644	488	1700	1700	1700	1700						
Volume to Capacity	0.93	0.12	0.00	0.10	0.10	0.07						
Queue Length 95th (m)	99.0	3.1	0.0	0.0	0.0	0.0						
Control Delay (s)	45.5	13.4	0.0	0.0	0.0	0.0						
Lane LOS	E	B	0.0									
Approach Delay (s)	45.5	13.4	0.0									
Approach LOS	Е	В										
Intersection Summary								191				
Average Delay			24.8									
Intersection Capacity Utiliza	tion		39.6%	IC	U Level o	f Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्न	7"		ની	7	7	₽	
Volume (veh/h)	4	0	0	13	1	38	_ 1	320	45	120	255	4
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	88.0	0.88	0.88	0.88
Hourly flow rate (vph)	- 5	0	0	15	1	43	1	364	51	136	290	5
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)						4						
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	953	982	292	928	933	364	294			415		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	953	982	292	928	933	364	294			415		
tC, single (s)	7.1	6.5	6.2	7.2	6.6	6.3	4.2			4.2		
tC, 2 stage (s)		0.0	0.2		0.0							
tF (s)	3.5	4.0	3.3	3.6	4.1	3.4	2.3			2.3		
p0 queue free %	98	100	100	93	100	94	100			88		
cM capacity (veh/h)	202	219	747	219	228	668	1245			1123		
				NB 2	SB 1	SB 2	12.10					
Direction, Lane #	EB 1	WB 1	NB 1		136		_	_		_		
Volume Total	5	59	365	51		294						
Volume Left	5	15	1	0	136	0						
Volume Right	0	43	0	51	0	5						
cSH	202	817	1245	1700	1123	1700						
Volume to Capacity	0.02	0.07	0.00	0.03	0.12	0.17						
Queue Length 95th (m)	0.6	1.9	0.0	0.0	3.3	0.0						
Control Delay (s)	23.3	14.0	0.0	0.0	8.6	0.0						
Lane LOS	С	В	Α		Α							
Approach Delay (s)	23.3	14.0	0.0		2.7							
Approach LOS	С	В										
Intersection Summary												
Average Delay			2.3									
Intersection Capacity Utilization	1		46.8%	IC	U Level	of Service			Α			
Analysis Period (min)			15									

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Movement	EBL	EBT	EBR	WBL	VVBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		स्			î,		7	^	7			
Volume (veh/h)	95	14	0	0	39	3	116	415	0	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	108	16	0	0	44	3	132	472	0	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)								,110.110				
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	525	735	0	743	735	236	0			472		
vC1, stage 1 conf vol							-					
vC2, stage 2 conf vol												
vCu, unblocked vol	525	735	0	743	735	236	0			472		
tC, single (s)	7.6	6.6	7.0	7.6	6.6	7.0	4.3			4.1		
tC, 2 stage (s)												
tF (s)	3.6	4.0	3.4	3.6	4.0	3.4	2.3			2.2		
p0 queue free %	70	95	100	100	86	100	92			100		
cM capacity (veh/h)	356	311	1075	268	311	757	1552			1087		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4	- 1					
Volume Total	124	48	132	236	236	0	_					
Volume Left	108	0	132	0	0	0						
Volume Right	0	3	0	0	0	0						
cSH	350	324	1552	1700	1700	1700						
Volume to Capacity	0.35	0.15	0.08	0.14	0.14	0.00						
Queue Length 95th (m)	12.5	4.1	2.2	0.0	0.0	0.0						
Control Delay (s)	20.8	18.0	7.5	0.0	0.0	0.0						
Lane LOS	20.0 C	C	Α.	0.0	0.0	0.0						
Approach Delay (s)	20.8	18.0	1.6									
Approach LOS	C	C	1.0									
Intersection Summary	T'0.10											William I
Average Delay			5.7									
Intersection Capacity Utilizat	ion		32.3%	IC	U Level o	of Service			Α			
Analysis Period (min)	,		15			. 30, 1,30						

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Movement	EBL	EBT	WBT	WBR	SBL	SBR	
Lane Configurations	*	↑	^	7	K/F		
Volume (veh/h)	138	15	20	556	117	29	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	
Hourly flow rate (vph)	157	17	23	632	133	33	
Pedestrians							
Lane Width (m)							
Walking Speed (m/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (m)							
pX, platoon unblocked							
C, conflicting volume	655				353	23	
C1, stage 1 conf vol	000				000		
C2, stage 2 conf vol							
Cu, unblocked vol	655				353	23	
:C, single (s)	4.1				6.5	6.3	
:C, 2 stage (s)	7.1				Ų.	0.0	
iF (s)	2.2				3.6	3.4	
p0 queue free %	83				74	97	
cM capacity (veh/h)	918				521	1031	
						1001	
Direction, Lane #	EB 1	EB 2	WB 1	WB 2	SB 1		
/olume Total	157	17	23	632	166		
/olume Left	157	0	0	0	133		
Volume Right	0	0	0	632	33		
SH	918	1700	1700	1700	578		
Volume to Capacity	0.17	0.01	0.01	0.37	0.29		
Queue Length 95th (m)	4.9	0.0	0.0	0.0	9.4		
Control Delay (s)	9.7	0.0	0.0	0.0	13.7		
Lane LOS	Α				В		
Approach Delay (s)	8.8		0.0		13.7		
Approach LOS					В		
Intersection Summary					115 6		
Average Delay			3.8				
Intersection Capacity Utilizat	ion		52.3%	IC	U Level	of Service	Α
Analysis Period (min)			15				

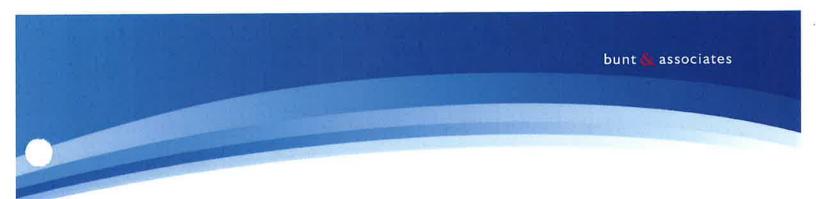
<i>></i>	→	\rightarrow	1	-	*	1	†	1	-	Ţ	1
EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
	^	7		4					7	44	7
0	106	26	1	154	0	0	0	0	3	206	422
	Stop			Yield			Free			Free	
	0%			0%			0%			0%	
0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
0	120	30	1	175	0	0	0	0	3	234	480
		2									
							None			None	
328	241	117	199	720	0	714			0		
328	241	117	199	720	0	714			0		
7.6	6.6	7.0	7.6	6.6	7.0	4.1			4.3		
3.6	4.0	3.4	3.6	4.0	3.4	2.2			2.3		
100	81	97	100	49	100	100			100		
356	651	903	608	345	1075	882			1552		
EB 1	WB 1	SB 1	SB 2	SB 3	SB 4				1		
150	176	3	117	117	480	-					11-1
0	1	3	0	0	0						
30	0	0	0	0	480						
811	346	1552	1700	1700	1700						
0.19	0.51	0.00	0.07	0.07	0.28						
5.4	22.0	0.1	0.0	0.0	0.0						
11.3	25.7	7.3	0.0	0.0	0.0						
В	D	Α									
11.3	25.7	0.0									
В	D										
							. 0.			3.	W #
on		43.9%	IC	U Level o	f Service			Α			
		15									
	328 328 328 7.6 3.6 100 356 EB 1 150 0 30 811 0.19 5.4 11.3 B 11.3 B	BL EBT 0 106 Stop 0% 0.88 0.88 0 120 328 241 7.6 6.6 3.6 4.0 100 81 356 651 EB 1 WB 1 150 176 0 1 30 0 811 346 0.19 0.51 5.4 22.0 11.3 25.7 B D 11.3 25.7 B D 11.3 25.7 B D	BL EBT EBR 0 106 26 Stop 0% 0.88 0.88 0.88 0 120 30 2 328 241 117 328 241 117 7.6 6.6 7.0 3.6 4.0 3.4 100 81 97 356 651 903 EB 1 WB 1 SB 1 150 176 3 0 1 3 30 0 0 811 346 1552 0.19 0.51 0.00 5.4 22.0 0.1 11.3 25.7 7.3 B D A 11.3 25.7 7.3 B D A 11.3 25.7 0.0 B D 6.0 on 43.9%	BL EBT EBR WBL 0 106 26 1 Stop 0% 0.88 0.88 0.88 0.88 0 120 30 1 2 328 241 117 199 7.6 6.6 7.0 7.6 3.6 4.0 3.4 3.6 100 81 97 100 356 651 903 608 EB 1 WB 1 SB 1 SB 2 150 176 3 117 0 1 3 0 356 651 903 608 EB 1 WB 1 SB 1 SB 2 150 176 3 117 0 1 3 0 30 0 0 0 811 346 1552 1700 0.19 0.51 0.00 0.07 5.4 22.0 0.1 0.0 11.3 25.7 7.3 0.0 B D A 11.3 25.7 7.3 0.0 B D A 11.3 25.7 0.0 B D 6.0 on 43.9% iC	BBL BBT BBR WBL WBT 1	BBL EBT EBR WBL WBT WBR 0 106 26 1 154 0 Stop Yield 0% 0% 0.88 0.88 0.88 0.88 0.88 0.88 0 120 30 1 175 0 328 241 117 199 720 0 7.6 6.6 7.0 7.6 6.6 7.0 3.6 4.0 3.4 3.6 4.0 3.4 100 81 97 100 49 100 356 651 903 608 345 1075 EB 1 WB 1 SB 1 SB 2 SB 3 SB 4 150 176 3 117 117 480 0 1 3 0 0 0 30 0 0 0 480 811 346 1552 1700 1700 1700 0.19 0.51 0.00 0.07 0.07 0.28 5.4 22.0 0.1 0.0 0.0 0.0 11.3 25.7 7.3 0.0 0.0 0.0 B D A 11.3 25.7 7.3 0.0 0.0 B D A 11.3 25.7 0.0 B D 6.0 G 1CU Level of Service	EBL EBT EBR WBL WBT WBR NBL 0 106 26 1 154 0 0 Stop Yield 0% 0% 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0 120 30 1 175 0 0 2 2 328 241 117 199 720 0 714 7.6 6.6 7.0 7.6 6.6 7.0 4.1 3.6 4.0 3.4 3.6 4.0 3.4 2.2 100 81 97 100 49 100 100 356 651 903 608 345 1075 882 EB1 WB1 SB1 SB2 SB3 SB4 150 176 3 117 117 480 0 1 3 3 0 0 0 0 30 0 0 0 480 811 346 1552 1700 1700 1700 0.19 0.51 0.00 0.07 0.07 0.28 5.4 22.0 0.1 0.0 0.0 0.0 11.3 25.7 7.3 0.0 0.0 0.0 11.3 25.7 7.3 0.0 0.0 0.0 B D 6.0 on 43.9% iCU Level of Service	EBL EBT EBR WBL WBT WBR NBL NBT 0 106 26 1 154 0 0 0 0 Stop Yield Free 0% 0% 0% 0% 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88	EBL EBT EBR WBL WBT WBR NBL NBT NBR 0 106 26 1 154 0 0 0 0 0 Stop Yield Free 0% 0% 0% 0% 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88	EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL 1 154 0 0 0 0 0 3 Stop Yield Free 0% 0% 0% 0% 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.8	EBL EBT EBR WBL WBT WBR NBL NBT NBR SBL SBT 0 106 26 1 154 0 0 0 0 3 206 Stop 7ield Free Free 0% 0% 0% 0% 0.88 0.88 0.88 0.88 0.88 0.88 0.88 0.88

	۶	→	*	1	•	•	4	†	1	-	ļ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4			र्स	7		सी	7	7	Þ	
Volume (veh/h)	4	2	0	9	3	24	0	247	2	32	303	7
Sign Control		Stop			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	5	2	0	10	3	27	0	281	2	36	344	8
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)						4						
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	717	704	348	699	706	281	352			283		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	717	704	348	699	706	281	352			283		
tC, single (s)	7.1	6.5	6.2	7.1	6.5	6.2	4.1			4.1		
tC, 2 stage (s)												
tF (s)	3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
p0 queue free %	99	99	100	97	99	96	100			97		
cM capacity (veh/h)	323	351	695	344	349	756	1201			1274		
Direction, Lane #	EB 1	WB 1	NB 1	NB 2	SB 1	SB 2					11-100	
Volume Total	7	41	281	2	36	352						
Volume Left	5	10	0	0	36	0						
Volume Right	0	27	0	2	0	8						
cSH	332	1035	1201	1700	1274	1700						
Volume to Capacity	0.02	0.04	0.00	0.00	0.03	0.21						
Queue Length 95th (m)	0.5	1.0	0.0	0.0	0.7	0.0						
Control Delay (s)	16.1	11.9	0.0	0.0	7.9	0.0						
Lane LOS	С	В			Α							
Approach Delay (s)	16.1	11.9	0.0		0.7							
Approach LOS	С	В										
Intersection Summary												
Average Delay			1.2									
Intersection Capacity Utilizat	ion		39.5%	IC	CU Level	of Service			Α			
Analysis Period (min)			15									

	*	-	*	•	←	*	1	†	-	-	↓	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		स			1		ň	44	7			
Volume (veh/h)	379	36	0	0	11	6	40	290	1	0	0	0
Sign Control		Yield			Stop			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	431	41	0	0	12	7	45	330	1	0	0	0
Pedestrians												
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)												
Median type								None			None	
Median storage veh)												
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	269	422	0	441	420	165	0			331		
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	269	422	0	441	420	165	0			331		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.4			4.1		
tC, 2 stage (s)												
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.3			2.2		
p0 queue free %	31	92	100	100	98	99	97			100		
cM capacity (veh/h)	623	500	1075	458	507	851	1538			1226		
Direction, Lane#	EB 1	WB 1	NB 1	NB 2	NB 3	NB 4						
Volume Total	472	19	45	165	165	1	- 11					
Volume Left	431	0	45	0	0	0						
Volume Right	0	7	0	0	0	1						
cSH	610	592	1538	1700	1700	1700						
Volume to Capacity	0.77	0.03	0.03	0.10	0.10	0.00						
Queue Length 95th (m)	57.8	0.8	0.7	0.0	0.0	0.0						
Control Delay (s)	28.1	11.3	7.4	0.0	0.0	0.0						
Lane LOS	D	В	Α	0.0	0.0	0.0						
Approach Delay (s)	28.1	11.3	0.9									
Approach LOS	D	В										
Intersection Summary		71 11 11			VIII.				- 4			
Average Delay			15.9									
Intersection Capacity Utilization	n		46.9%	IC	U Level o	of Service			Α			
Analysis Period (min)			15									

	*	-	•	*	-	4	
Movement	EBL	EBT	WBT	WBR	SBL	SBR	
ane Configurations	7		^	79	NA.		
olume (veh/h)	36	21	18	142	505	125	
gn Control		Free	Free		Stop		
rade		0%	0%		0%		
ak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	
ourly flow rate (vph)	41	24	20	161	574	142	
edestrians	•						
ane Width (m)							
alking Speed (m/s)							
rcent Blockage							
ght turn flare (veh)							
edian type		None	None				
edian storage veh)		1100	,,,,,,,				
ostream signal (m)							
(, platoon unblocked							
c, conflicting volume	182				126	20	
1, stage 1 conf vol	,02						
2, stage 2 conf vol							
Cu, unblocked vol	182				126	20	
, single (s)	4.1				6.5	6.3	
, 2 stage (s)					****		
(s)	2.2				3.6	3.4	
queue free %	97				30	86	
f capacity (veh/h)	1375				825	1035	
			771 E 7	1415.0			
ection, Lane #	EB 1	EB 2	WB 1	WB 2	SB 1	_	1
lume Total	41	24	20	161	716		
lume Left	41	0	0	0	574		
lume Right	0	0	0	161	142		
H _	1375	1700	1700	1700	859		
olume to Capacity	0.03	0.01	0.01	0.09	0.83		
ueue Length 95th (m)	0.7	0.0	0.0	0.0	77.8		
ontrol Delay (s)	7.7	0.0	0.0	0.0	26.3		
ine LOS	Α				D		
proach Delay (s)	4.9		0.0		26.3		
pproach LOS					D		
ersection Summary							
erage Delay			19.9				
tersection Capacity Utilizat	tion		54.2%	IC	U Level o	of Service	
nalysis Period (min)			15				

	٠	-	•	1	4-	*	4	†	1	-	ļ	1
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		†	7		सी					7	^	74
Volume (veh/h)	0	415	111	0	51	0	0	0	0	Ö	320	109
Sign Control		Stop			Yield			Free			Free	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88	0.88
Hourly flow rate (vph)	0	472	126	0	58	0	0	0	0	0	364	124
Pedestrians												,
Lane Width (m)												
Walking Speed (m/s)												
Percent Blockage												
Right turn flare (veh)			2									
Median type								None			None	
Median storage veh)								115.10			110110	
Upstream signal (m)												
pX, platoon unblocked												
vC, conflicting volume	393	364	182	481	488	0	488			0		
vC1, stage 1 conf vol			,04	101			100			•		
vC2, stage 2 conf vol												
vCu, unblocked vol	393	364	182	481	488	0	488			0		
tC, single (s)	7.6	6.6	7.0	7.5	6.5	6.9	4.1			4.4		
tC, 2 stage (s)					0.0	- 3						
tF (s)	3.6	4.0	3.4	3.5	4.0	3.3	2.2			2.3		
p0 queue free %	100	15	85	100	88	100	100			100		
cM capacity (veh/h)	484	556	820	113	479	1084	1072			1538		
Direction, Lane #	EB 1	WB 1	SB 1				1072			1000		
				SB 2	SB 3	SB 4	_		_			
Volume Total	598	58	0	182	182	124						
Volume Left	0	0	0	0	0	0						
Volume Right	126	0	0	0	0	124						
cSH	633	479	1700	1700	1700	1700						
Volume to Capacity	0.94	0.12	0.00	0.11	0.11	0.07						
Queue Length 95th (m)	103.6	3.3	0.0	0.0	0.0	0.0						
Control Delay (s)	49.0	13.5	0.0	0.0	0.0	0.0						
Lane LOS	E	В										
Approach Delay (s)	49.0	13.5	0.0									
Approach LOS	Е	В										
Intersection Summary	_		<u>,</u> λ " ="			" "						
Average Delay			26.3).".						
Intersection Capacity Utiliza	ation		40.0%	IC	U Level c	of Service			Α			
Analysis Period (min)			15									



APPENDIX D

Illumination Warrant Spreadsheets



This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001.

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS Main Road Minor Road City/Town Highway 508 Existing Access County of Lethbridge

Date Other

Existing Traffic Conditions
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT

GEOMETRIC FACTORS Channelization Rating	Value Descriptive	Rating	Weight	Comments Refer to Table 1(A) to determine rating value	Check OK	Score
Presence of raised channelization? (Y/N)	n				OK	
Highest operating speed on raised, channellzed approach (km/h) Channelization Factor	0		5		ok ok	0
Approach Sight Distance on most constrained approach (%)	100	0	10	Relative to the recommended minimum sight distance	ок	0
Posted Speed limit (in 10's of km/h)	90				ок	
Radius of Horizontal Curve (m)	400			Enter "T" for tangent (no horizontal curve at the intersection)	ок	
Posted Speed Category =		0				
Posted Speed Category = Posted Speed Category = Posted Speed Category =	В	0				
Horizontal Curvature Factor		4	5		OK	20
Angle of Intersection (10's of Degrees)	90	0	5		ок	0
Downhill Approach Grade (x.x%)	2.0	0	3	Rounded to nearest tenth of a percent	ок	0
Number of Intersection Legs	4	2	3	Number of legs = 3 or more	ок	6
97/1989A				Geometric I	actors Subtotal	26

the intersection signalized ? (Y/N)	n			Calculate the Signalization Warrant Factor		
AADT on Major Road (2-way) AADT on Minor Road (2-way) Signalization Warrant	450 100 Descriptive	0 0	10 20 30	Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be sat to Zero) Refer to Table 1(B) for description and rating values for signalization warrant,	OK OK OK	0 0 0
light-Time Hourly Pedestrian Volume	0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ок	0
ntersecting Roadway Classification	Descriptive	0	5	Refer to Table 1(B) for ratings	ок	0
perating Speed or Posted Speed on Major Road (km/h)	90	4	5	Refer to Table 1(B), note #3	ок	20
Operating Speed on Minor Road (km/h)	50	0	5	Refer to Table 1(B), note #3	ок	0
				Operational Factors	Subtotal	20

Lighted Developments within 150 m radius of intersection	0	0	5	Maximum of 4 quadrants OK	0
				Environmental Factor Subtotal	0
COLLISION HISTORY		-11			
Average Annual night-time collision frequency due to inadequate lighting (collisions/yr, rounded to nearest whole #) OR	0.0	0	0	Enter either the annual frequency (See Table 1(C), note #4) OR OK the number of collisions / MEV (Unused	0
Collision Rate over last 3 years, due to inadequate lighting (/MEV) is the average ratio of all night to day collisions >= 1.5 (Y/N)	0 n	0	0	values should be set to Zero) OK OK	0 K
				Collision History Subtotal	0

Check Intersection Signalization: Intersection is not Signalized

ENVIRONMENTAL FACTOR

LIGHTING IS NOT WARRANTED

SUMMARY		
Geometric Factors Subtotal	26	
Operational Factor Subtotal	20	
Environmental Factor Subtotal	0	
Collision History Subtotal	0	_
TOTAL POINTS	46	

isomplate cooping/or solution of Canada (601

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001. Please enter information in the cells with yellow background INTERSECTION CHARACTERISTICS Existing Traffic Conditions Site visit completed on May 12, 2014 Intersection turning movement volumes obtained from AT Date Other Minor Road County of Lethbridge City/Town GEOMETRIC FACTORS Rating Check Weight Channelization Rating Descriptive Refer to Table 1(A) to determine rating value Presence of raised channelization? (Y/N)
Highest operating speed on raised, channelized approach (km/h)
Channelization Factor 5 15 OK Approach Sight Distance on most constrained approach (%) 100 0 Relative to the recommended minimum sight distance ок 0 Posted Speed limit (in 10's of km/h) Radius of Horizontal Curve (m) 100 Enter "T" for tangent (no horizontal curve at the intersection) 400 Posted Speed Calegory = 0 Posted Speed Category = Posted Speed Category = Posted Speed Category = В Horizontal Curvature Factor 5 ОК 20 Angle of Intersection (10's of Degrees) 90 0 5 Downhill Approach Grade (х.х%) 2.0 0 3 Rounded to nearest tenth of a percent OK 0 Number of Intersection Legs 2 Number of legs = 3 or more ок Geometric Factors Subtotal 41 **OPERATIONAL FACTORS** Is the intersection signalized? (Y/N) Calculate the Signalization Warrant Factor OK OK OK AADT on Major Road (2-way) 6200 Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant. AADT on Minor Road (2-way) Signalization Warrant OK Night-Time Hourly Pedestrian Volume 0 0 10 Refer to Table 1(B), note #2, to account for children and seniors οк 0 Intersecting Roadway Classification Descriptive 5 Refer to Table 1(B) for ratings. OK 20 Operating Speed or Posted Speed on Major Road (km/h) 110 4 Refer to Table 1(B), note #3 οк 20 Operating Speed on Minor Road (km/h) 100 Refer to Table 1(B), note #3 ОК 20 Operational Factors Subtotal 100 **ENVIRONMENTAL FACTOR** Lighted Developments within 150 m radius of intersection Maximum of 4 quadrants ок 0 Environmental Factor Subtotal D **COLLISION HISTORY** Average Annual night-time collision (requency due to inadequate lighting (collisions/yr, rounded to nearest whole #) OR Enter either the annual frequency (See Table 1(C), note #4) the number of collisions / MEV ОК 15 (Unused Collision Rate over last 3 years, due to inadequate lighting (/MEV) 0 0 values should be set to Zero) OK 0 is the average ratio of all night to day collisions >= 1.5 (Y/N) Collision History Subtotal 15

> Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED REVIEW SITE AND COLLISIONS TO DETERMINE LIGHTING TYPE PARTIAL OR DELINEATION)

SUMMARY	
Geometric Factors Subtotal	41
Operational Factor Subtotal	100
Environmental Factor Subtotal	0
Collision History Subtotal	15
TOTAL POINTS	156

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001.

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS Main Road Minor Road City/Town County of Lethbridge

Date Other

Existing Traffic Conditions
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT

GEOMETRIC FACTORS Channelization Rating	Value Descriptive	Rating 3	Weight	Comments Refer to Table 1(A) to determine rating value	Check	Score
Presence of raised channelization? (Y/N)	n				OK	
Highest operating speed on raised, channelized approach (km/h)	0		5		OK	
Channelization Factor					OK	15
Approach Sight Distance on most constrained approach (%)	100	0	10	Relative to the recommended minimum sight distance	ок	0
Posted Speed limit (in 10's of km/h)	100				ок	
Radius of Horizontal Curve (m)	T			Enter "T" for tangent (no horizontal curve at the intersection)	OK	
Posted Speed Category =		0				
Posted Speed Category =	В	0				
Posted Speed Category = Posted Speed Category =		0				
Horizontal Curvature Factor		0	5		ок	0
TOTAL CHITCHE F GOLO						
Angle of Intersection (10's of Degrees)	90	0	5		ok	0
Downhill Approach Grade (x.x%)	2.0	0	3	Rounded to nearest tenth of a percent	OK	0
Number of Intersection Legs	4	2	3	Number of legs = 3 or more	OK	6
-				Geometric F	ctors Subtotal	21

OPERATIONAL FACTORS							
Is the intersection signalized ? (Y/N)	n -			Calculate the Signalization Warrant Factor			
AADT on Major Road (2-way) AADT on Minor Road (2-way) Signalization Warrant	5500 550 Descriptive	4 1 0	10 20 30	Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant,	ok ok ok	ОК	40 20 0
Night-Time Hourly Pedestrian Volume	0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ок		0
Intersecting Roadway Classification	Descriptive	2	5	Refer to Table 1(B) for ratings	ОК		10
Operating Speed or Posted Speed on Major Road (km/h)	100	4	5	Refer to Table 1(B), note #3	ОК		20
Operating Speed on Minor Road (km/h)	100	4	5	Refer to Table 1(B), note #3	ОК		20
				Operational Factor	s Subtota		110

Lighted Developments within 150 m radius of intersection	0	0	5	Maximum of 4 quadrants OK	0
				Environmental Factor Subtotal	0
COLLISION HISTORY					
Average Annual night-time collision (requency due to inadequate lighting (collisions/yr, rounded to nearest whole #) OR	0.0	0	0	Enter either the annual frequency (See Table 1(C), note #4) OR OK the number of collisions / MEV (Unused	0
Collision Rate over last 3 years, due to inadequate lighting (MEV) Is the average ratio of all night to day collisions >= 1.5 (Y/N)	0 n	0	0	values should be set to Zero) OK OK OK	0
				Collision History Subtotal	0

Check Intersection Signalization: Intersection is not Signalized

ENVIRONMENTAL FACTOR

ILLUMINATION WARRANTED

REVIEW SITE AND COLLISIONS TO DETERMINE LIGHTING TYPE (
PARTIAL OR DELINEATION)

SUMMARY		
Geometric Factors Subtotal	21	
Operational Factor Subtotal	110	
Environmental Factor Subtotal	0	
Collision History Subtotal	0	_
TOTAL POINTS	131	

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001. Please enter information in the cells with yellow background INTERSECTION CHARACTERISTICS Date Other 20-Year Background Traffic Conditions Site visit completed on May 12, 2014 Minor Road Intersection turning movement volumes obtained from AT County of Lethbridge City/Town GEOMETRIC FACTORS Value Check Rating Channelization Rating Descriptive Refer to Table 1(A) to determine rating value OK OK OK Presence of raised channelization? (Y/N) Highest operating speed on raised, channelized approach (km/h)
Channelization Factor 0 Approach Sight Distance on most constrained approach (%) 100 0 Relative to the recommended minimum sight distance OK 0 Posted Speed limit (in 10's of km/h) Radius of Horizontal Curve (m) 400 Enter "T" for tangent (no horizontal curve at the intersection) Posted Speed Category = 0 Posted Speed Category = Posted Speed Category = R Posted Speed Category = Horizontal Curvature Factor 5 ОК 20 Angle of Intersection (10's of Degrees) 0 Downhill Approach Grade (x.x%) 2.0 0 3 Rounded to nearest tenth of a percent oĸ 0 Number of Intersection Leas 2 Number of legs = 3 or more ОК Geometric Factors Subtotal 26 **OPERATIONAL FACTORS** ls the intersection signalized? (Y/N) Calculate the Signalization Warrant Factor ok ok ok AADT on Major Road (2-way) 450 10 20 30 Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for Descriptive description and rating values for signalization warrant. OK Night-Time Hourly Pedestrian Volume 0 10 Refer to Table 1(B), note #2, to account for children and seniors οк 0 Intersecting Roadway Classification Descriptive 5 Refer to Table 1(B) for ratings. OK 0 Operating Speed or Posted Speed on Major Road (km/h) 90 Refer to Table 1(B), note #3 ОК 20 Operating Speed on Minor Road (km/h) 50 Refer to Table 1(B), note #3 OK 0 Operational Factors Subtotal 20 **ENVIRONMENTAL FACTOR** Lighted Developments within 150 m radius of intersection Maximum of 4 quadrants ok 0 Environmental Factor Subtotal n COLLISION HISTORY Average Annual night-time collision frequency due to inadequale lighting (collisions/yr, rounded to nearest whole #) OR Enter either the annual frequency (See Table 1(C), note #4) the number of collisions / MEV OK 0 Collision Rate over last 3 years, due to inadequate lighting (/MEV) is the average ratio of all night to day collisions >= 1.5 (Y/N) 0 0 values should be set to Zero) OK 0

> Check Intersection Signalization: Intersection is not Signalized

LIGHTING IS NOT WARRANTED

SUMMARY		
Geometric Factors Subtotal	26	
Operational Factor Subtotal	20	
Environmental Factor Subtotal	0	
Collision History Subtotal	0	
TOTAL POINTS	46	

Collision History Subtotal

Transportation Association of Canada 2001

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001.

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS Main Road Minor Road City/Town Highway 4 Highway 508 County of Lethbridge

20-Year Background Traffic Conditions
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT Date Other

GEOMETRIC FACTORS	Value	Rating	Weight	Comments	Check	Score
Channelization Rating	Descriptive	Rating	vveignt	Refer to Table 1(A) to determine rating value	OK	Guore
Presence of raised channelization? (Y/N)	Descriptive			Training to table 10 to a determine young you	OK	
Highest operating speed on raised, channelized approach (km/h)	Ö		5		OK	
Channelization Factor					ok	15
Approach Sight Distance on most constrained approach (%)	100	0	10	Relative to the recommended minimum sight distance	ок	0
Posted Speed limit (In 10's of km/h)	100				ок	
Radius of Horizontal Curve (m)	400			Enter "T" for tangent (no horizontal curve at the intersection)	OK	
Posted Speed Category =	100	0				
Posted Speed Category =	В	4				
Posted Speed Category =		0				
Posted Speed Category =		0	25		OK	20
Horizontal Curvature Factor		4	5		UK	20
Angle of Intersection (10's of Degrees)	90	0	5		ок	0
Angle of Intersection (100 b) Dogrado)						
Downhill Approach Grade (x.x%)	2.0	0	3	Rounded to nearest tenth of a percent	OK	0
Number of Intersection Legs	4	2	3	Number of legs = 3 or more	OK	6
2555525				Geometric I	actors Subtotal	41

OPERATIONAL FACTORS							
the intersection signalized ? (Y/N)	n			Calculate the Signalization Warrant Factor			
AADT on Major Road (2-way) AADT on Minor Road (2-way) Signalization Warrant	6400 450 Descriptive	4 0 0	10 20 30	Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant.	OK OK OK	ок	40 0 0
ght-Time Hourly Pedestrian Volume	0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ок		0
ntersecting Roadway Classification	Descriptive	4	5	Refer to Table 1(B) for ratings.	ок		20
Operating Speed or Posted Speed on Major Road (km/h)	110	4	5	Refer to Table 1(B), note #3	ок		20
Operating Speed on Minor Road (km/h)	100	4	5	Refer to Table 1(B), note #3	ок		20
				Operational Factors	s Subtota	1	100

ENVIRONMENTAL FACTOR			- 2				
inhted Developments within 150 m radius of intersection	0	0	5	Maximum of 4 quadrants		ок	0
				Envir	Environmental Factor Subtotal		0
COLLISION HISTORY							III E
Average Annual night-time collision frequency due to inadequate lighting (collisions/yr, rounded to nearest whole #)	1.0	1	15	Enter either the annual frequency (See Table 1(C), no the number of collisions / MEV	te #4) OR (Unused	ОК	15
OR Collision Rate over last 3 years, due to inadequate lighting (/MEV) s the average ratio of all night to day collisions >= 1.5 (Y/N)	0 n	0	0	values should be set to Zero)	(5),2004	OK OK	0

Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED

REVIEW SITE AND COLLISIONS TO DETERMINE LIGHTING TYPE (
PARTIAL OR DELINEATION)

SUMMARY		
Geometric Factors Subtotal	41	
Operational Factor Subtotal	100	
Environmental Factor Subtotal	0	
Collision History Subtotal	15	
TOTAL POINTS	156	
TOTALFORTO	130	_

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Collision History Subtotal 15

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001. Please enter information in the cells with yellow background INTERSECTION CHARACTERISTICS 20-Year Background Traffic Conditions Site visit completed on May 12, 2014 Intersection lurning movement volumes obtained from AT Date Other Highway 5 Highway 508 County of Lethbridge City/Town GEOMETRIC FACTORS Value Rating Check Score Channelization Rating
Presence of raised channelization? (Y/N) Refer to Table 1(A) to determine rating value OK OK OK Highest operating speed on raised, channelized approach (km/h) Channelization Factor 5 15 Approach Sight Distance on most constrained approach (%) 100 0 10 Relative to the recommended minimum sight distance ОК 0 Posted Speed limit (in 10's of km/h) Radius of Horizontal Curve (m) 100 Enter "T" for tangent (no horizontal curve at the intersection) Posted Speed Category = 0 0 Posted Speed Category = В Posted Speed Category = Posted Speed Category = 000 Horizontal Curvature Factor 5 ОК 0 Angle of Intersection (10's of Degrees) 90 0 5 0 Downhill Approach Grade (x,x%) 2.0 0 3 Rounded to nearest tenth of a percent OK o Number of Intersection Leas 2 3 Number of legs = 3 or more ок Geometric Factors Subtotal 21 **OPERATIONAL FACTORS** the intersection signalized ? (Y/N) Calculate the Signalization Warrant Factor AADT on Major Road (2-way) 6200 Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant. AADT on Minor Road (2-way) 700 OK OK Signalization Warrant 0 OK Night-Time Hourly Pedestrian Volume 0 0 10 Refer to Table 1(B), note #2, to account for children and seniors ок 0 Intersecting Roadway Classification Descriptive 5 Refer to Table 1(B) for ratings. ОК 10 Operating Speed or Posted Speed on Major Road (km/h) 100 4 5 Refer to Table 1(B), note #3 ОК 20 Operating Speed on MInor Road (km/h) 100 Refer to Table 1(B), note #3 OK 20 Operational Factors Subtotal 110 **ENVIRONMENTAL FACTOR** Lighted Developments within 150 m radius of intersection 0 Maximum of 4 quadrants Ωĸ 0 **Environmental Factor Subtotal** 0 **COLLISION HISTORY** Average Annual night-time collision frequency due to inadequate lighting (collisions/yr, rounded to nearest whole #) 0.0 0 Enter either the annual frequency (See Table 1(C), note #4) the number of collisions / MEV ΟK 0 OR
Collision Rate over last 3 years, due to inadequate lighting (/MEV) (Unused 0 0 values should be set to Zero) ОК 0 is the average ratio of all night to day collisions >= 1.5 (Y/N) Collision History Subtotal

> Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED

REVIEW SITE AND COLLISIONS TO DETERMINE LIGHTING TYPE PARTIAL OR DELINEATION)

SUMMARY	
Geometric Factors Subtotal	21
Operational Factor Subtotal	110
Environmental Factor Subtotal	0
Collision History Subtotal	0
TOTAL POINTS	131

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001.

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS City/Town Date Other

Opening Day Traffic Conditions
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT

GEOMETRIC FACTORS Channelization Rating	Value Descriptive	Rating	Weight	Comments Refer to Table 1(A) to determine rating value	Check OK	Score
Presence of raised channeszation? (Y/N)	n			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	OK	
lighest operating speed on raised, channelized approach (km/h)	0		5		ОК	
Channelization Factor					ок	0
Approach Sight Distance on most constrained approach (%)	100	0	10	Relative to the recommended minimum sight distance	ОК	0
Posted Speed limit (in 10's of km/h)	90				ок	
ladius of Horizontal Curve (m)	400			Enter "T" for tangent (no horizontal curve at the intersection)	ок	
Posted Speed Calegory =		0				
Posted Speed Category =	В	4				
Posted Speed Category =		0				
Posted Speed Category =		0			ок	20
Horizontal Curvature Factor		4	9		OK	
Angle of Intersection (10's of Degrees)	90	0	5		OK	0
Downhill Approach Grade (x,x%)	2.0	0	3	Rounded to nearest tenth of a percent	ОК	0
Number of Intersection Legs	4	2	3	Number of legs = 3 or more	ОК	8
1011001 01 11101-0				Geomel	ric Factors Subtotal	26

OPERATIONAL FACTORS						
s the intersection signalized ? (Y/N)	n			Calculate the Signalization Warrant Factor		
AADT on Major Road (2-way) AADT on Minor Road (2-way) Signalization Warrant	6900 B100 Descriptive	4 4 0	10 20 30	Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant.	OK OK OK	40 80 0
Night-Time Hourly Pedestrian Volume	0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ОК	0
ntersecting Roadway Classification	Descriptive	0	5	Refer to Table 1(B) for ralings	ОК	0
Operating Speed or Posted Speed on Major Road (km/h)	90	4	5	Refer to Table 1(B), note #3	ОК	20
Operating Speed on Minor Road (km/h)	50	0	5	Refer to Table 1(B), note #3	ок	0
				Operational Factors	Subtota	140

ENVIRONMENTAL FACTOR						
Lighted Developments within 150 m radius of intersection	0	0	5	Maximum of 4 quadrants	ок	0
					Environmental Factor Subtotal	
COLLISION HISTORY					No.	
Average Annual night-time collision frequency due to	0,0	0	0	Enter either the annual frequency (See Table 1(C), note #4) OR OK	0

the number of collisions / MEV (Unused OR
Collision Rate over last 3 years, due to inadequate lighting (MEV)
Is the average ratio of all night to day collisions >= 1.5 (Y/N) OK OK 0 values should be set to Zero) Collision History Subtotal

> Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED DELINEATION LIGHTING TO ILLUMINATE PEDESTRIANS OR CROSS STREET TRAFFIC

SUMMARY		
Geometric Factors Subtotal	26	
Operational Factor Subtotal	140	
Environmental Factor Subtotal	0	
Collision History Subtotal	0	_
TOTAL POINTS	166	

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001. Please enter information in the cells with yellow background INTERSECTION CHARACTERISTICS Date Opening Day Traffic Conditions Site visit completed on May 12, 2014 Minor Road ntersection turning movement volumes obtained from AT County of Lethbridge City/Town **GEOMETRIC FACTORS** Value Rating Weight Check Channelization Rating Refer to Table 1(A) to determine rating value Presence of raised channelization? (Y/N) Highest operating speed on raised, channelized approach (km/h) Channelization Factor 5 15 OK Approach Sight Distance on most constrained approach (%) 100 0 Relative to the recommended minimum sight distance ок 0 Posted Speed limit (in 10's of km/h) Radius of Horizontal Curve (m) 100 400 OK Enter "T" for tangent (no horizontal curve at the intersection) OK Posted Speed Calegory = 0 Posled Speed Category =
Posled Speed Category =
Posted Speed Category = В Horizontal Curvature Factor 5 ОК 20 Angle of Intersection (10's of Degrees) 90 0 ок 0 Downhill Approach Grade (x.x%) 2.0 0 3 Rounded to nearest tenth of a percent OK 0 Number of Intersection Legs 2 Number of legs = 3 or more Geometric Factors Subtotal 41 **OPERATIONAL FACTORS** the intersection signalized ? (Y/N) Calculate the Signalization Warrant Factor AADT on Major Road (2-way) 10800 10 OK OK Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for AADT on Minor Road (2-way) Signalization Warrant 20 30 80 OK description and rating values for signalization warrant, Night-Time Hourly Pedestrian Volume 0 0 10 Refer to Table 1(B), note #2, to account for children and seniors ок 0 Intersecting Roadway Classification Descriptive 5 Refer to Table 1(B) for ratings. OK 20 Operating Speed or Posted Speed on Major Road (km/h) 110 Refer to Table 1(B), note #3 20 Operating Speed on Minor Road (km/h) 100 Refer to Table 1(B), note #3 ОК 20 Operational Factors Subtotal 180 **ENVIRONMENTAL FACTOR** Lighted Developments within 150 m radius of intersection Maximum of 4 quadrants OK 0 Environmental Factor Subtotal n **COLLISION HISTORY** Average Annual night-lime collision frequency due to inadequate lighting (collisions/yr, rounded to nearest whole #) OR Collision Rate over last 3 years, due to inadequate lighting (/MEV) Is the average ratio of all night to day collisions >= 1,5 (Y/N) Enter either the annual frequency (See Table 1(C), note #4) the number of collisions / MEV OK 15 0 0 values should be set to Zero) 0

> Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED

DELINEATION LIGHTING TO ILLUMINATE PEDESTRIANS OR CROSS
STREET TRAFFIC

SUMMARY	
Geometric Factors Subtotal	41
Operational Factor Subtotal	180
Environmental Factor Subtotal	0
Collision History Subtotal	15
TOTAL POINTS	236

Collision History Subtotal

Transportation Association of Canada 2001

15

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001,

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS Main Road Minor Road City/Town Highway 5 Highway 508 County of Lethbridge

Opening Day Traffic Conditions
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT Date Other

GEOMETRIC FACTORS	Value	Rating	Weight	Comments	Check	Score
Channelization Rating	Descriptive	3		Refer to Table 1(A) to determine rating value	OK OK	
Presence of raised channelization? (Y/N)	ņ		-		OK	
lighest operating speed on raised, channelized approach (km/h) Channelization Factor	0		5		ок	15
Approach Sight Distance on most constrained approach (%)	100	0	10	Relative to the recommended minimum sight distance	ОК	0
3 - 1 - 1 0 1 (i)1 (i 10 11 /h)	100				OK	
Posted Speed limit (in 10's of km/h) Radius of Horizontal Curve (m)	7			Enter "T" for langent (no horizontal curve at the intersection)	OK	
Posted Speed Category =		D				
Posted Speed Category =	В	0				
Posted Speed Category =		0				
Posted Speed Category =		0			ОК	0
Horizontal Curvature Factor		0	5		OK	U
Angle of Intersection (10's of Degrees)	90	0	5		ok	0
The state of the s						121
Downhill Approach Grade (x,x%)	2.0	0	3	Rounded to nearest tenth of a percent	ок	0
Number of Intersection Legs	4	2	3	Number of legs = 3 or more	ок	6
centralia:				Geometric I	actors Subtotal	21

OPERATIONAL FACTORS						X H	
is the intersection signalized ? (Y/N)	n			Calculate the Signalization Warrant Factor			
AADT on Major Road (2-way) AADT on Minor Road (2-way) Signalization Warrant	7000 2300 Descriptive	4 4 0	10 20 30	Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant.	OK OK OK		10 30 0
light-Time Hourly Pedestrian Volume	0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ок		0
ntersecting Roadway Classification	Descriptive	2	5	Refer to Table 1(B) for ratings	ОК	1	10
Operating Speed or Posted Speed on Major Road (km/h)	100	4	5	Refer to Table 1(B), note #3	ок	2	20
Operating Speed on Minor Road (km/h)	100	4	5	Refer to Table 1(B), note #3	ок	2	20
				Operational Factors	Subtota	17	70

			Environmental Factor Subtotal	0
		-		
0,0	0	0	Enter either the annual frequency (See Table 1(C), note #4) OR OK	0
0	0	0	values should be set to Zero) OK OK	0
	0,0 0 n	0.0 0	0,0 0 0 0 0 n 0 0	0.0 0 Enter either the annual frequency (See Table 1(C), note #4) OR OK the number of collisions / MEV (Unused OK)

Check Intersection Signalization: Intersection is not Signalized

ENVIRONMENTAL FACTOR

ILLUMINATION WARRANTED DELINEATION LIGHTING TO ILLUMINATE PEDESTRIANS OR CROSS STREET TRAFFIC

SUMMARY	
Geometric Factors Subtotal	21
Operational Factor Subtotal	170
Environmental Factor Subtotal	0
Collision History Subtotal	0
TOTAL POINTS	191

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001.

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS
Highway 508
Existing Access
County of Lethbridge

Date Other

Main Road Minor Road City/Town

20-Year Post Development Traffic Conditions
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT

Channelization Rating	Value	Rating	Weight	Comments	Check	Score
Presence of raised channelization? (Y/N)	Descriptive	0		Refer to Table 1(A) to determine rating value	OK OK	
lighest operating speed on raised, channelized approach (km/h)	Ö		5		OK	
Channelization Factor					ok	0
Approach Sight Distance on most constrained approach (%)	100	0	10	Relative to the recommended minimum sight distance	ок	0
Posted Speed limit (in 10's of km/h)	90				ок	
Radius of Horizontal Curve (m)	400			Enter "T" for tangent (no horizontal curve at the intersection)	OK	
Posted Speed Category =	1961	0				
Posted Speed Category = Posted Speed Category =	В	4				
Posted Speed Category =		o o				
Horizontal Curvalure Factor		4	5		ок	20
Angle of Intersection (10's of Degrees)	90	0	5		ок	0
Downhill Approach Grade (x.x%)	2,0	0	3	Rounded to nearest tenth of a percent	ОК	0
Number of Intersection Legs	4	2	3	Number of legs = 3 or more	ок	6
				Geometric Fa	tors Subtotal	26

in.			Calculate the Signalization Warrant Factor		
6900 8100 Descriptive	4 4 0	10 20 30	Elther Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant.	OK OK	40 80 0
0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ок	0
Descriptive	0	5	Refer to Table 1(B) for ratings.	ок	0
90	4	5	Refer to Table 1(B), note #3	ок	20
50	0	5	Refer to Table 1(B), note #3	OK	0
	6900 8100 Descriptive 0 Descriptive 90	6900 4 8100 4 Descriptive 0	\$600 4 10 8100 4 20 Descriptive 0 30 0 0 10 Descriptive 0 5 90 4 5	S800 4 10 8100 4 20 Descriptive 0 30 Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant. O 0 10 Refer to Table 1(B), note #2, to account for children and seniors Descriptive 0 5 Refer to Table 1(B) for ratings. 90 4 5 Refer to Table 1(B), note #3	Second S

ENVIRONMENTAL FACTOR						
Lighted Developments within 150 m radius of intersection	0	0	5	Maximum of 4 quadrants	ОК	0
					Environmental Factor Subtotal	0

COLLISION HISTORY						
Average Annual night-time collision frequency due to inadequate lighting (collisions/yr, rounded to nearest whole #) OR	0.0	0	0		OR OK	0
Collision Rate over last 3 years, due to inadequate lighting (/MEV)	0	0	0	values should be set to Zero)	OK	0
the average ratio of all night to day collisions >= 1,5 (Y/N)	n	0			OK	
				₩		OK
				Collision	History Subto	eal o

Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED DELINEATION LIGHTING TO ILLUMINATE PEDESTRIANS OR CROSS STREET TRAFFIC

SUMMARY	
Geometric Factors Subtotal	26
Operational Factor Subtolal	140
Environmental Factor Subtotal	0
Collision History Subtotal	0
TOTAL POINTS	166

Transportation Association of Canada 2001

This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001,

Please enter information in the cells with yellow background

INTERSECTION CHARACTERISTICS Main Road Minor Road City/Town Highway 4 Highway 508 County of Lethbridge

20-Year Post Development Traffic Conditions.
Site visit completed on May 12, 2014
Intersection turning movement volumes obtained from AT Date Other

GEOMETRIC FACTORS Channelization Rating		Value Descriptive	Rating 3	Weight	Comments Refer to Table 1(A) to determine rating value	Check OK	Score
Presence of raised channellzation? (Y/N)		n				OK	
Highest operating speed on raised, channelized	i approach (km/h)	0		5		OK	
Channelization Factor						OK	15
Approach Sight Distance on most constrained a	approach (%)	100	0	10	Relative to the recommended minimum sight distance	ОК	0
Posted Speed limit (in 10's of km/h)		100				OK	
Radius of Horizontal Curve (m)		400			Enter "T" for tangent (no horizontal curve at the intersection) OK	
	Posted Speed Category =		0		•		
	Posted Speed Category =	В	4				
	Posted Speed Category =		0				
	Posted Speed Category =		0			O.K	
Horizontal Curvature Factor			4	5		ok	20
Angle of Intersection (10's of Degrees)		90	0	5		OK	0
530 7 5.5			1211			OK	0
Downhill Approach Grade (x,x%)		2.0	0	3	Rounded to nearest tenth of a percent	OK	0
Number of Intersection Legs		4	2	3	Number of legs = 3 or more	OK	6
					Geome	tric Factors Subtotal	41

OPERATIONAL FACTORS						
Is the intersection signalized ? (Y/N)	n			Calculate the Signalization Warrant Factor		
AADT on Major Road (2-way) AADT on Minor Road (2-way) Signalization Warrant	11000 6900 Descriptive	4 4 0	10 20 30	Either Use the two AADT inputs OR the Descriptive Signalization Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant.	OK OK OK	40 80 0
Night-Time Hourly Pedestrian Volume	0	0	10	Refer to Table 1(B), note #2, to account for children and seniors	ок	0
Intersecting Roadway Classification	Descriptive	4	5	Refer to Table 1(B) for ratings.	ок	20
Operating Speed or Posted Speed on Major Road (km/h)	110	4	5	Refer to Table 1(B), note #3	ок	20
Operating Speed on Minor Road (km/h)	100	4	5	Refer to Table 1(B), note #3	ок	20
				Operational Factor	s Subtotal	180

ENVIRONMENTAL FACTOR				The state of the s		
Lighted Developments within 150 m radius of intersection	0	0	5	Maximum of 4 quadrants	ок	0
					Environmental Factor Subtotal	0

							_
1.0	1-	15			ОК		15
0	0	0	values should be set to Zero)	(0.110000	ОК		0
n	0				ок	ОК	4
	1.0 0 n	1.0 1 0 n 0	1.0 1 15 0 0 0 n 0	Enter either the annual frequency (See Table 1(C), note #4) the number of collisions / MEV	the number of collisions / MEV Enter either the annual frequency (See Table 1(C), note #4) Unused	the number of collisions / MEV Collisions / MEV Collisions / MEV Collisions / MEV Collisions / MEV	the number of collisions / MEV (Unused O 0 values should be set to Zero) OK OK OK OK OK OK OK OK OK

Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED DELINEATION LIGHTING TO ILLUMINATE PEDESTRIANS OR CROSS STREET TRAFFIC

SUMMARY	
Geometric Factors Subtotal	41
Operational Factor Subtotal	180
Environmental Factor Subtotal	0
Collision History Subtotal	15
TOTAL POINTS	236

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This spreadsheet is to be used in conjunction with Illumination of Isolated Rural Intersections, Transportation Association of Canada, February 2001. Please enter information in the cells with yellow background INTERSECTION CHARACTERISTICS Date 20-Year Post Development Traffic Conditions Main Road Site visit completed on May 12, 2014 Intersection furning movement volumes obtained from AT Other Minor Road County of Lethbridge **GEOMETRIC FACTORS** Value Rating Weight Comments Check Channelization Rating
Presence of raised channelization? (Y / N)
Highest operating speed on raised, channelized approach (km/h)
Channelization Factor Refer to Table 1(A) to determine rating value OK OK OK OK 15 Approach Sight Distance on most constrained approach (%) 100 0 Relative to the recommended minimum sight distance ок Posted Speed limit (in 10's of km/h) Radius of Horizontal Curve (m) 100 T Enter "T" for langent (no horizontal curve at the intersection) OK Posted Speed Category = 0 0 Posted Speed Category = Posted Speed Category = B Posted Speed Category = Horizontal Curvature Factor 5 ок Angle of Intersection (10's of Degrees) 0 5 OK 0 Downhill Approach Grade (x.x%) 2.0 0 3 Rounded to nearest tenth of a percent QΚ 0 Number of Intersection Legs Number of legs = 3 or more ОК Geometric Factors Subtotal 21 **OPERATIONAL FACTORS** s the intersection signalized ? (Y/N) Calculate the Signalization Warrant Factor AADT on Major Road (2-way) AADT on Minor Road (2-way) 7400 Either Use the two AADT inputs OR the Descriptive Signalization 2300 20 30 OK 80 Warrant (Unused values should be set to Zero) Refer to Table 1(B) for description and rating values for signalization warrant. Signalization Warrant Descriptive OK ОК Night-Time Hourly Pedestrian Volume 0 10 Refer to Table 1(B), note #2, to account for children and seniors OK 0 Intersecting Roadway Classification Descriptive 5 Refer to Table 1(B) for ratings. ОК 10 Operating Speed or Posted Speed on Major Road (km/h) 100 Refer to Table 1(8), note #3 ОК 20 Operating Speed on Minor Road (km/h) 100 Refer to Table 1(B), note #3 ок 20 Operational Factors Subtotal 170 **ENVIRONMENTAL FACTOR** Lighted Developments within 150 m radius of intersection Maximum of 4 quadrants Environmental Factor Subtotal ٥ **COLLISION HISTORY** Average Annual night-time collision frequency due to 0,0 0 nadequate lighting (collisions/yr, rounded to nearest whole #) Enter either the annual frequency (See Table 1(C), note #4) OR OK 0 OR the number of collisions / MEV values should be set to Zero) Collision Rate over last 3 years, due to inadequate lighting (/MEV) is the average ratio of all night to day collisions >= 1.5 (Y/N) 0 OK OK

> Check Intersection Signalization: Intersection is not Signalized

ILLUMINATION WARRANTED

DELINEATION LIGHTING TO ILLUMINATE PEDESTRIANS OR CROSS
STREET TRAFFIC

SUMMARY	
Geometric Factors Subtotal	21
Operational Factor Subtotal	170
Environmental Factor Subtotal	0
Collision History Subtotal	0
TOTAL POINTS	191

Collision History Subtotal

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0



APPENDIX E

Background Growth Calculations



1283-09 Lethbridge Agri-Business Park

Highway 4 (N of Hwy 508) Yearly Traffic Growth

Highway 4 (S of Hwy 508) Yearly Traffic Growth

Year	AADT		% Growth	Year	AADT	%	Growth
	2013	6052	1.32%		2013	6180	1.64%
	2012	5973	3.86%		2012	6080	5.74%
	2011	5751	0.02%		2011	5750	0.17%
	2010	5750	2.10%		2010	5740	1.23%
	2009	5632			2009	5670	
	Averag	e	1.82%		Averag	je	2.20%

Hwy 4 Average = 2.01%

Highway 5 Yearly Traffic Growth

Highway 5 (S ofHwy 508) Yearly Traffic Growth

2013 2012 2011 2010	5450 5450 5450 5450	% Growth 0.00% 0.00% 0.00% 1.87%	Year 2013 2012 2011 2010	5020 5020 5030 5030	% Growth 0.00% -0.20% 0.00% 2.03%
2009	5350 Average	0.47%	2009	4930 Average	0.46%

Hwy 5 Average = 0.46%

Highway 508 @ Hwy 4 Yearly Traffic Growth

Highway 508 @ Hwy 5 Yearly Traffic Growth

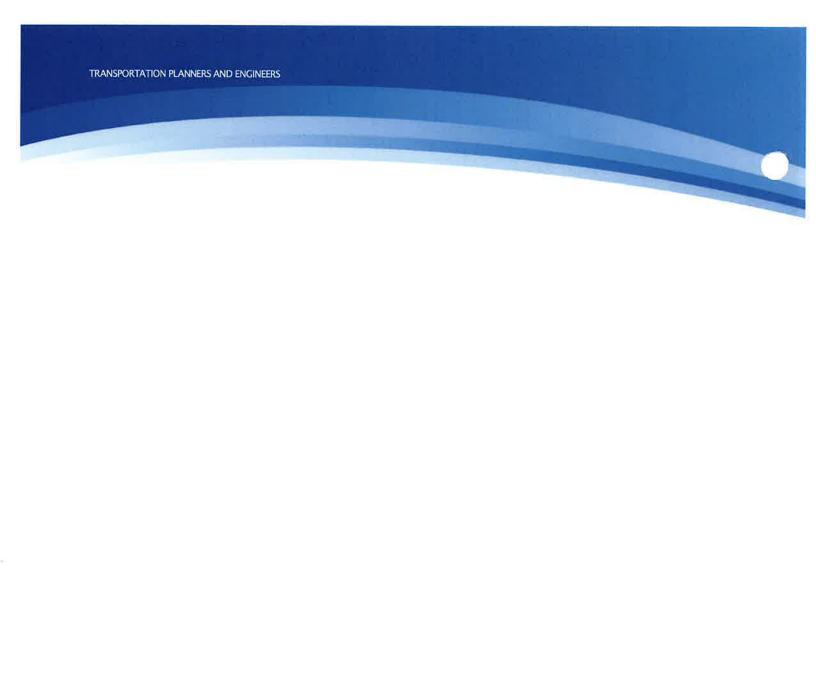
Year	AADT 2013 2012 2011 2010 2009	440 440 380 380 380	6 Growth 0.00% 15.79% 0.00% 0.00%	Year 2013 2012 2011 2010 2009		% Growth 0.00% 11.76% 0.00% 0.00%
	Average	!	3.95%		Average	2.94%

Hwy 508 Average = 3.44%



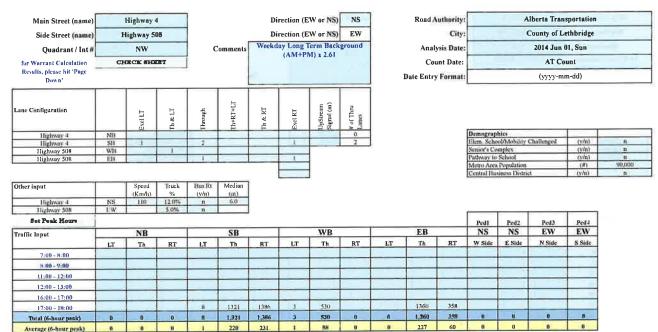
APPENDIX F

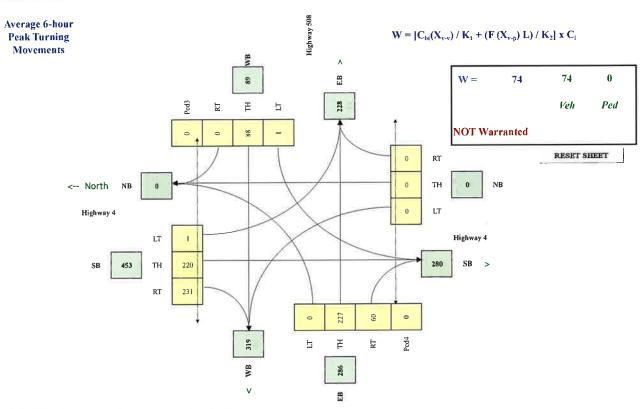
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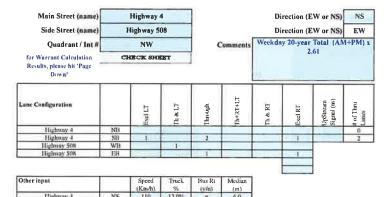
Alberta Transportation - Traffic Signal Warrant Analysis







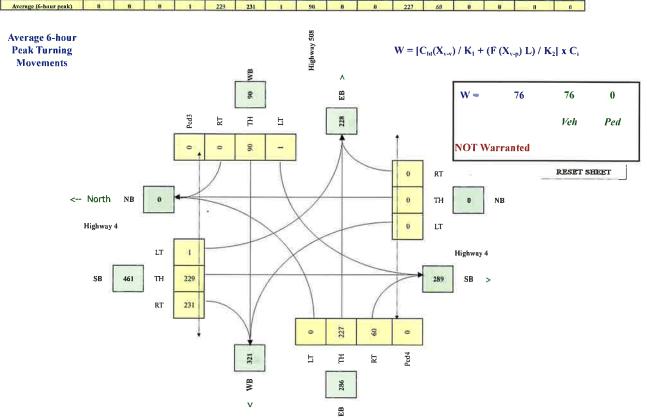
Alberta Transportation - Traffic Signal Warrant Analysis



Road Authority:	Alberta Transportation
City:	County of Lethbridge
Analysis Date:	2014 Jun 01, Sun
Count Date:	AT Count
Date Entry Format:	(yyyy-mm-dd)

Demographics		
Elem. School/Mobility Challenged	(y/n)	n
Senior's Complex	(y/n)	D
Pathway to School	(y/n)	n
Metro Area Population	(#)	90,000
Central Husiness District	(y/n)	n

Linguistay 4	3,9907	4 4 4 5 5	4 4 4 17 79	- 43	0.0											
Highway 508	EW		5.0%	.0]										
Set Peak Hours	1												Pedi	Ped2	Ped3	Ped-l
Traffic Input		NB			SB			WB			EB		NS	NS	EW	EW
	LT	Th	RT	LT	Th	RT	LT	Th	RT	LT	Th	RT	W Side	E Side	N Side	S Side
7;00 - H:00		100														0
N.00 - 9:00																
11:00 - 12:00																
12:00 - 13:00																
16:00 - 17:00																
17:00 - 18:00				8	1373	1386	- 3	538			1360	358				
Total (6-hour peak)	0	.0	0	R-	1,373	1.386	3	538	0	0	1,360	358		. 0	0	0



Traffic Signal Warrant Spreadsheet - $y3H \stackrel{@}{\otimes} 2007$ Transportation Association of Canada

Appendix D – Site Drainage Analysis

HYDROLOGICAL and SITE DRAINAGE ANALYSIS

Proposed Subdivision Located Within SE ¼ 5-8-20-W4
County of Lethbridge, AB



PREPARED FOR: Dar Ray Farms Ltd. PREPARED BY:
Hasegawa Engineering
Consulting Professional Engineers
A Division of 993997 Alberta Ltd.
1220 31st Street North
Lethbridge, AB T1H 5J8

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1.0 Introduction

On behalf of the Dar Ray Farms Ltd., Hasegawa Engineering (HE) has completed this preliminary hydrological analysis of the subject site. The hydrological analysis includes the following major aspects:

- 1. Overall site layout and conditions
- 2. Offsite topography
- 3. Precipitation and runoff analysis
- 4. Retention Pond calculations for storing all runoff up to a 100 year storm event

The legal land description for the site is SE 5-8-20-W4, County of Lethbridge, AB. The site is situated on approximately 8 kilometers southeast of Lethbridge at the intersection of Highways 4 and 508 as shown in Figure 1 (Appendix A.)

2.0 Site Conditions

2.1 Existing

The site consists of approximately 144 acres (58 ha.) of primarily agricultural land with an existing farmstead. There are 2 lots which have been divided out and developed; they have access roads and structures including grain silos with the remainder of the lot essentially graveled to accommodate storage and vehicle traffic. The site is bordered on the north by agricultural land, on the northeast by train tracks and Highway 4, on the southwest by an irrigation main canal and on the south by Highway 508. Adjacent ditches are variably defined and surface water tends to end up trapped in a low areas adjacent to the irrigation canal where it must be pumped out.

2.2 Proposed

The proposed development would further divide the site creating a total of about 25 agribusiness lots and two ponds, one for raw water/fire water and one for storm water management.

The site has poor existing drainage - all storm water will collect and need to be pumped into the irrigation ditch as permitted. It is anticipated that permission to release storm water will not be given until major storm events have ended; therefore, the development needs the capacity to store all storm runoff up to the 100 year design storm.

3.0 Surface Runoff Design Criteria

3.1 Onsite Runoff

Predevelopment

Normally, a predevelopment model would be developed to generate baseline storm water volumes and flow rates – allowable post development release rates during storm events would be dictated by these predevelopment results. In this case, all storm water needs to be stored prior to release and the predevelopment model becomes unnecessary.

Post-Development

A topographic survey of the area provided contour data to determine existing drainage patterns and slopes. Post development flows will generally be able to use existing topography and the site was divided into 16 post development catchments also shown in Figure 2 – Appendix A. Subcatchment boundaries are based on the existing drainage (direction and slope of overland drainage) along with proposed drainage through ditches. The proposed development has agribusiness lots ranging from 2-7 acres in size accessed from gravel service roads. Since overland flow is generally to the west, the model uses ditches on the west boundaries of lots (i.e. either in road allowances or along lots) to intercept storm water and drain it to roadside ditches. All ditches have been modeled as 0.5 meters deep and 5 meters across at the top with 3h:1v side slopes. Existing topography will generally drain storm water in the ditches to the storm pond although several areas require cuts or fills as part of final design elevations (especially for lots backing onto the irrigation canal.)

The retention pond is modelled with 0.6 meters of freeboard followed by 2 meters of active storage although it will actually be deeper to accommodate fire protection water and raw water storage. Pond side slopes are 5h:1v in the freeboard and active storage range.

The existing homestead is modeled as is while remaining areas are modelled with the following assumptions:

- Developed lots will have 25% of the lot area covered with buildings (modeled as 100% impervious surface) with the remaining 75% of the lot graveled for traffic and storage areas (modeled as 70% impervious surface.) These figures are the resulting average after checking 12 business lots in the Lethbridge industrial area ranging from 0.36 25.8 hectares in size.
- Subcatchment areas include the adjoining service roads up to the centerline. Assumptions for the model are based on a 10 meter gravel road (70% impervious) within a 20 meter road allowance that is otherwise 0% impervious for an overall average of 35% impervious.
- Pond surface is modeled as 100% impervious areas.

The post development model assumes a 100 year/24 hour storm event but the modeling period may be extended to allow runoff from all subcatchments to fully drain to the pond. The 100 year storm is a design storm that produces 109 mm of rain with a peak rate of 255 mm/hour (Figure 3 - Appendix A.) The final model is shown in Figure 4 of Appendix A. Results of the computer simulation are discussed in section 4 below. Key input parameters for SWMM analysis along with summaries of the computer simulations are attached in Appendix B.

3.2 Storm Water from Off-site

Runoff from agricultural land north of the property should generally drain away from the development. On the remaining sides, the development is generally isolated from off-site storm water by the surrounding roads and irrigation canal although runoff from adjacent roads (highway, secondary and canal road) is included where appropriate.

4.0 Surface Runoff Results

Results of initial runoff modelling show that the active storage volume in the pond is adequate to store the 100 year storm. Performance of the retention pond is shown in Table 1 below and shows the pond fills to 100% full.

Table 1 Post Development Results - Retention Pond Storage

	Maximum Volume	Change In Pond Height m	Total Volume (including ditches) m ³
Retention Pond	57184 (100% full)	2.00	57198

Results show the ditches are generally sufficient to route storm water to the retention ponds - final design will address flow and velocity within the ditches. Note that the 100 year storm generates significant storm flows; where drainage ditches are intersected by cross roads it will not be practical to convey the storm water under the road in culverts. Any culverts will be designed to convey a 100 year storm.

5.0 Conclusion

Results from computer modeling using inputs appropriate for the Lethbridge area have been used to design storm water retention facilities for the proposed development. Significant factors affecting the volume of storm water to be stored are:

- The proposed land use indicates more impervious surface and higher volumes of runoff.
- There is no release during the storm all runoff must be stored until release into the irrigation ditch is permitted.

This results in large storm water retention areas located in the lower elevations of the development next to the irrigation canal. Existing topography is generally adequate to allow drainage to the retention ponds although some final design will be needed. Because all release will be done by mechanically pumping the retention ponds after the storm has ended, there has been no modeling of the site to establish predevelopment runoff rates.

APPENDIX A - FIGURES



All construction shall be in accordance with the latest codes, may it be construction, mechanical,

HABEGAWA

RAY TAYLOR

AGRI-BUISNESS PARK

FIGURE 1 LOCATION MAP

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NOTES

s is a copyright drawing and shall not be roduced in any farm without writen mission of the engineer

onirador to check and verify all dimensions efore construction, any errors and omissions hall be reported to the engineer immediately

shall be reported to the engineer immediately Drawing shall not be used for construction to approved

Approved Do not scale the drawing

As construction shall be in accordance with the takent coders, may it be construction, mechanical, etc.

HABEGAWA 330, 370, 320 d Steet South Lethendage, Meen TH 784 Pr. 403-256-278 Fax. 403-258-278 Emelt ofter-@hasegawa ca

RAY TAYLOR

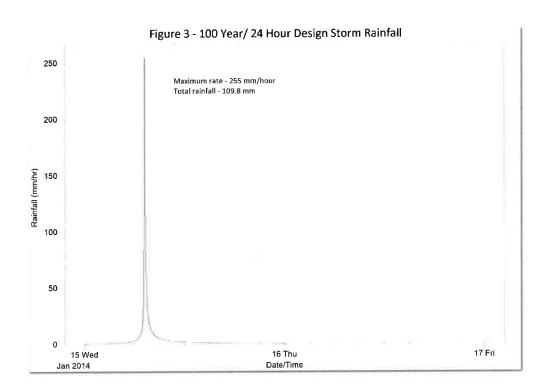
AGRI-BUISNESS PARK

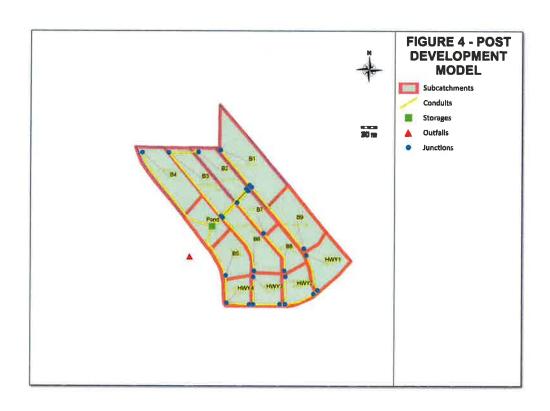
FIG. 2 - PROPOSED DEVELOPMENT & STORM CATCHMENTS

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APPENDIX B - MODELING SUMMARIES

[TITLE]

13-129 AgriBusiness Post Develop 100yr

[OPTIONS]	
FLOW UNITS	CMS
INFILTRATION	GREEN AMPT
FLOW ROUTING	DYNWAVE
START DATE	01/15/2014
START TIME	00:00:00
REPORT START DAT	E 01/15/2014
REPORT START TIM	E 00:00:00
END DATE	01/17/2014
END TIME	00:00:00
SWEEP START	01/01
SWEEP END	12/31
DRY DAYS	0
REPORT STEP	0:01:00
WET STEP	0:05:00
DRY_STEP	0:05:00
ROUTING STEP	5
ALLOW_PONDING	YES
INERTIAL DAMPING	PARTIAL
VARIABLE STEP	0.75
LENGTHENING STEP	0
MIN SURFAREA	0
NORMAL_FLOW_LIMI	TED BOTH
SKIP STEADY STAT	E NO
FORCE MAIN EQUAT	ION H-W
LINK_OFFSETS	DEPTH
MIN SLOPE	0
[EVAPORATION]	
;;Type	Parameters

CONSTANT 0.0
DRY_ONLY NO

[RAINGAGES]
;; Rain Time Snow Data
;; Name Type Intrvl Catch Source
;; ---- Interview of the content of the con

[SUBCATCHMENTS]

[motol	Dant		Pcnt.	Curb	S
;;			Total	Pcnt.	1 24 2			
;;Name	Raingage	Outlet	Area	Imperv	Width	Slope	Length	P
;;								-
B1	100yr/24hr	JB1_1	8.8797	64.9	479.984	0.84	0	
B2	100yr/24hr	JB2 1	3.7601	73.8	372.287	0.49	0	
В3	100yr/24hr	JB3 1	4.9242	61.7	437.707	0.36	0	
B4	100yr/24hr	JB4 1	6.1524	64	435.568	0.44	0	
B5	100yr/24hr	JB5 1	4.1604	69	237.06	0.34	0	
В6	100yr/24hr	JB6 1	5.2665	71	406.366	0.48	0	
В7	100yr/24hr	JB7 2	2.7945	69.4	251.011	0.96	0	
В8	100yr/24hr	JB8 1	2.9698	71.9	227.868	0.8	0	
В9	100yr/24hr	JB9_1	6.0132	68.5	470.996	0.78	0	
HWY1	100yr/24hr	JHWY1 1	4.6471	63.9	320.49	0.55	0	
HWY2	100yr/24hr	JHWY2 1	3.2559	69.1	190.962	0.56	0	
ншүз	100vr/24hr	JHWY3 1	3.0587	69.8	299.873	0.83	0	
HWY4	100yr/24hr	JHWY4 2	2.3915	65.8	235.616	0.83	0	
Pond	100vr/24hr	RetPond	3.9423	82.7	3942.3	1	0	

[SUBAREAS]

B2	OUTLET
B2	OUTLET
B3	OUTLET
B4 0.02 0.1 2 4 25 00 B5 0.02 0.1 2 4 25 00 B6 0.02 0.1 2 4 25 00 B6 B7 0.02 0.1 2 4 25 00 B8 0.02 0.1 2 4 25 00 B8 0.02 0.1 2 4 25 00 B9 0.02 0.1 2 4 25 00 B9 0.02 0.1 2 4 25 00 BWY1 0.02 0.1 2 4 25 00 BWY2 0.02 0.1 2 4 25 00 BWY2 0.02 0.1 2 4 25 00 BWY3 0.02 0.1 2 4 25 00 BWY3 0.02 0.1 2 4 25 00 BWY4 0.02 0.1 0.1 2 0.1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	OUTLET
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B5	OUTLET
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[INFILTRATION] ;;Subcatchment Suction HydCon IMDmax ;;	OUTLET
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B7 295 1 0.3	
B8 295 1 0.3	
B9 295 1 0.3	
HWY1 295 1 0.3	
HWY2 295 1 0.3	
HWY3 295 1 0.3	
HWY4 295 1 0.3	
Pond 295 1 0.3	
[JUNCTIONS]	
;; Invert Max. Init. Surcharge Ponded	
;;Name Elev. Depth Depth Area	
JB1 1 927.1 0.5 0 0 100	
JB2_1 926.6 0.5 0 0 100	
JB2 ⁻ 2 926.2 0.5 0 0 100	
JB3 1 925.9 0.5 0 0 100	
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JHWY4_2	925.35	0.75	0		0		100			
[OUTFALLS]										
;;	Invert	Outfal	ll Si	tage/I	able	Tide				
;;Name	Elev.	Type	T	ime Se	ries	Gate				
;;										
OF2	923.2	FREE				NO				
[STORAGE]										
;;	Invert M	ax.	Init.	st	orage	Curve			Ponded	Evap.
;;Name			Depth		rve	Param	S		Area	Frac.
;;									1.65.40	
RetPond	923.1 2		0	TA	BULAR	PondB	RawWater2		16540	0
[CONDUITS]										
;;	Inlet		Outlet				Mannino	Inlet	Outlet	In
;;Name	Node		Node		Leng	gth	N	Offset	Offset	Fl
;;										
C11	JB4_1		RetPond	d	607		0.1	0	2	0 0
C13	JB1_1		JB1_2 JB7 1		233 15		0.1	0	0	0
C14 C15	JB1_3 JB7_1		JB7_1 JB7_3		96		0.1	0	0	0
C16	JB7_1 JB7_3		JB6 2		96		0.1	0	0	0
C17	JB6 2		RetPon	d	15		0.1	0	2	0
C18	JB2 1		JB3 1		125		0.1	0	0	0
C19	JB3_1		JB3_2		474		0.1	0	0	0
C20	JB3_2		RetPon	d	15		0.1	0	2	0
C21	JB9_1		JB1_3		450		0.1	0	0	0 0
C22	JB7_2		JB7_3		213 230		0.1	0	0	0
C23 C24	JB6_1 JB5 1		JB6_2 RetPond	d	209		0.1	0	2	0
C25	JHWY4 2		JB5 1	u	110		0.1	0	0	0
C26	JB8 1		JB7 2		215		0.1	0	0	0
C27	JHWY3_1		JHWY3	3	158		0.1	0	0	0
C28	JHWY2_1		JHWY2_		119		0.1	0	0	0
C29	JHWY1_1		JHWY1_		195		0.1	0	0	0
C30	JHWY1_2		JHWY2_		15 198		0.1	0	0	0
C31 C32	JHWY2_2 JHWY2_3		JHWY2_: JHWY3 :		15		0.1	0	0	0
C32	JHWY3 2		JHWY3		164		0.1	Ö	0	0
C34	JHWY3 3		JHWY4		15		0.1	0	0	0
C35	JHWY4_1		JHWY4	2	144		0.1	0	0	0
C39	JB2_2		JB3_2		193		0.01	0	0	0
C6	JB1_2		JB2_2		15		0.01	0	0	0
[VORONTONO]										
[XSECTIONS] ;;Link	Shape	Geor	n 1		Geom2	Ge	om3	Geom4	Barrels	
;;										
C11	IRREGULAR	Dit	ch3:1		0	0		0	1	
C13	IRREGULAR		ch3:1		0	0		0	1	
C14	IRREGULAR		ch3:1		0	0		0	1	
C15	IRREGULAR		ch3:1		0	0 0		0	1 1	
C16	IRREGULAR IRREGULAR		ch3:1		0	0		0	1	
C17 C18	IRREGULAR		ch3:1		0	0		0	1	
C19	IRREGULAR		ch3:1		0	0		0	1	
C20	IRREGULAR		ch3:1		0	0		0	1	
C21	IRREGULAR	Dit	ch3:1		0	0		0	1	
C22	IRREGULAR		ch3:1		0	0		0	1	
C23	IRREGULAR		ch3:1		0	0		0	1	
C24	IRREGULAR		ch3:1		0	0		0	1 1	
C25 C26	IRREGULAR IRREGULAR		ch3:1 ch3:1		0	0		0	1	
C27	IRREGULAR		ch3:1		0	0		0	1	
- ·			-							

C28 C29 C30 C31 C32 C33 C34 C35 C39	IRREGULAF IRREGULAF IRREGULAF IRREGULAF IRREGULAF IRREGULAF IRREGULAF IRREGULAF	Ditch3	:1 :1 :1 :1 :1 :1 :1 :1	0 0 0 0 0 0 0 0	0 0 0 0 0 0	0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1	
[TRANSECTS]								
X1 Ditch	0.1 0.05 4 -0.5	0.0	0.0 -0.5	0.0	0.0	0.0 5	0.0	0.0
X1 Ditch3:1	0.01 0.01 4 0 -0.75		0.0 -0.75	0.0	0.0	0.0 5	0.0	0.0
X1 Swale	0.1 0.05 3 -0.3	0.0 1.5	0.0	0.0	0.0	0.0	0.0	0.0
[LOSSES] ;;Link ;;	Inlet	Outlet	Average	Flap	Gate			
[CUR ES] ;;Name	Type	X- alue	Y- alue					
PondB PondB PondB PondB	Storage	0 .5 1 1.5	13605 14184 15342 16540					
PondB2 PondB2 PondB2 PondB2 PondB2	Storage	0 .5 1 1.5 2	11985 13605 14184 15342 16540					
PondBRawWater PondBRawWater PondBRawWater PondBRawWater	c1.5	0 1 1.5	26500 28224 29998 31823			es:		
PondBRawWate: PondBRawWate:		0 2	25086 32226					
[TIMESERIES] ;;Name	Date	Time	alue					
;;		0:00 0:05 0:10 0:15 0:20 0:25	0 0.763 0.771 0.779 0.787 0.796 0.804					

100yr/24hr	0:50	0.841
100yr/24hr	0:55	0.851
100yr/24hr	1:00	0.861
100yr/24hr	1:05	0.871
	1:10	0.881
100yr/24hr		
100yr/24hr	1:15	0.892
100yr/24hr	1:20	0.903
100yr/24hr	1:25	0.914
100yr/24hr	1:30	0.926
_	1:35	0.938
100yr/24hr		
100yr/24hr	1:40	0.95
100yr/24hr	1:45	0.963
100yr/24hr	1:50	0.976
100yr/24hr	1:55	0.99
100yr/24hr	2:00	1.004
= .	2:05	1.018
100yr/24hr		
100yr/24hr	2:10	1.033
100yr/24hr	2:15	1.048
100yr/24hr	2:20	1.064
100yr/24hr	2:25	1.08
100yr/24hr	2:30	1.097
	2:35	1.114
100yr/24hr		
100yr/24hr	2:40	1.132
100yr/24hr	2:45	1.151
100yr/24hr	2:50	1.17
100yr/24hr	2:55	1.191
100yr/24hr	3:00	1.211
-	3:05	1.233
100yr/24hr		
100yr/24hr	3:10	1.256
100yr/24hr	3:15	1.279
100yr/24hr	3:20	1.304
100yr/24hr	3:25	1.329
100yr/24hr	3:30	1.356
	3:35	1.384
100yr/24hr		
100yr/24hr	3:40	1.413
100yr/24hr	3:45	1.443
100yr/24hr	3:50	1.475
100yr/24hr	3:55	1.509
100yr/24hr	4:00	1.544
100yr/24hr	4:05	1.581
-		1.62
100yr/24hr	4:10	
100yr/24hr	4:15	1.661
100yr/24hr	4:20	1.705
100yr/24hr	4:25	1.751
100yr/24hr	4:30	1.8
100yr/24hr	4:35	1.853
	4:40	1.908
100yr/24hr		
100yr/24hr	4:45	1.967
100yr/24hr	4:50	2.031
100yr/24hr	4:55	2.099
100yr/24hr	5:00	2.172
100yr/24hr	5:05	2.251
	5:10	2.337
100yr/24hr		
100yr/24hr	5:15	2.43
100yr/24hr	5:20	2.532
100yr/24hr	5:25	2.643
100yr/24hr	5:30	2.765
100yr/24hr	5:35	2.9
_	5:40	3.051
100yr/24hr		
100yr/24hr	5:45	3.219
100yr/24hr	5:50	3.409
100yr/24hr	5:55	3.625
100yr/24hr	6:00	3.873
100yr/24hr	6:05	4.159
	/ See	

100yr/24hr	6:10	4.496
=		
100yr/24hr	6:15	4.897
100yr/24hr	6:20	5.383
100yr/24hr	6:25	5.985
100yr/24hr	6:30	6.748
100yr/24hr	6:35	7.75
100yr/24hr	6:40	9.123
100yr/24hr	6:45	11.117
100yr/24hr	6:50	14.266
-		
100yr/24hr	6:55	19.931
100yr/24hr	7:00	32.779
100yr/24hr	7:05	
-		83.515
100yr/24hr	7:10	255.206
100yr/24hr	7:15	114.934
_		
100yr/24hr	7:20	63.946
100yr/24hr	7:25	43.017
100yr/24hr	7:30	31.998
100yr/24hr	7:35	25.321
100yr/24hr	7:40	20.889
100yr/24hr	7:45	17.754
_		
100yr/24hr	7:50	15.429
100yr/24hr	7:55	13.641
100yr/24hr		
_	8:00	12.226
100yr/24hr	8:05	11.08
100yr/24hr	8:10	10.134
-		
100yr/24hr	8:15	9.34
100yr/24hr	8:20	8.665
100yr/24hr	8:25	8.083
100yr/24hr	8:30	7.577
100yr/24hr	8:35	7.133
100yr/24hr	8:40	6.74
100yr/24hr	8:45	6.39
100yr/24hr	8:50	6.077
100yr/24hr	8:55	5.794
-		
100yr/24hr	9:00	5.538
100yr/24hr	9:05	5.304
100yr/24hr	9:10	5.091
100yr/24hr	9:15	4.895
100yr/24hr	9:20	4.714
100yr/24hr	9:25	4.547
-		
100yr/24hr	9:30	4.392
100yr/24hr	9:35	4.248
100yr/24hr	9:40	4.114
100yr/24hr	9:45	3.989
100yr/24hr	9:50	3.871
100yr/24hr	9:55	3.761
100yr/24hr	10:00	3.657
100yr/24hr	10:05	3.559
100yr/24hr	10:10	3.467
<u> </u>		
100yr/24hr	10:15	3.38
100yr/24hr	10:20	3.297
100yr/24hr	10:25	
		3.219
100yr/24hr	10:30	3.144
100yr/24hr	10:35	3.073
=		
100yr/24hr	10:40	3.006
100yr/24hr	10:45	2.941
100yr/24hr	10:50	2.88
- .		
100yr/24hr	10:55	2.821
100yr/24hr	11:00	2.765
100yr/24hr	11:05	2.711
_	T T . O J	
100yr/24hr	11 10	
1 0 0 / 0 41	11:10	2.659
luuyr/24nr		
100yr/24hr	11:15	2.61
100yr/24hr	11:15 11:20	2.61 2.562
_	11:15	2.61

100yr/24hr 100yr/24hr		11:30 11:35 11:40 11:45 11:50 11:55 12:00 12:05 12:10 12:15 12:20 12:25 12:30 12:35 12:40 12:45 12:50 12:55 13:00 13:05 13:15 13:20 13:25 13:30 13:35 13:40	2.472 2.43 2.389 2.35 2.312 2.275 2.24 2.205 2.172 2.14 2.109 2.079 2.05 2.021 1.994 1.967 1.941 1.916 1.892 1.868 1.845 1.822 1.8 1.779 1.758 1.738 1.718
100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr	(e	14:50 14:55 15:00 15:05 15:10 15:15 15:20 15:25 15:30 15:35 15:40 15:45	1.485 1.47 1.457 1.443 1.43 1.417 1.404 1.392 1.38 1.368 1.356
100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr 100yr/24hr		15:50 15:55 16:00 16:05 16:10 16:15 16:20 16:25 16:30 16:35 16:40	1.333 1.322 1.311 1.3 1.289 1.279 1.269 1.259 1.249 1.239 1.23

100yr/24hr	16:50	1 211
2		1.211
100yr/24hr	16:55	1.202
100yr/24hr	17:00	1.193
<u> </u>		
100yr/24hr	17:05	1.185
100yr/24hr	17:10	1.176
-		
100yr/24hr	17:15	1.168
100yr/24hr	17:20	1.159
_		
100yr/24hr	17: 25	1.151
100yr/24hr	17:30	1.143
100yr/24hr	17:35	1.135
100yr/24hr	17:40	1.127
- · · · · · · · · · · · · · · · · · · ·		
100yr/24hr	17:45	1.119
100yr/24hr	17:50	1.112
_		
100yr/24hr	17:55	1.104
100yr/24hr	18:00	1.097
100yr/24hr	18:05	1.089
100yr/24hr	18:10	1.082
100yr/24hr	18:15	1.075
100yr/24hr	18:20	1.068
100yr/24hr	18:25	
- · · · · · · · · · · · · · · · · · · ·		1.061
100yr/24hr	18:30	1.055
100yr/24hr	18:35	
		1.048
100yr/24hr	18:40	1.041
100yr/24hr	18:45	1.035
100yr/24hr	18:50	1.028
100yr/24hr	18:55	1.022
100yr/24hr	19:00	1.015
100yr/24hr	19:05	1.01
100yr/24hr	19:10	1.004
100yr/24hr	19:15	0.998
100yr/24hr	19:20	0.992
100yr/24hr	19:25	0.986
100yr/24hr	19:30	0.98
100yr/24hr	19:35	0.974
100yr/24hr	19:40	0.969
100yr/24hr	19:45	0.963
100yr/24hr		
	19:50	0.958
100yr/24hr	19:55	0.952
100yr/24hr	20:00	0.947
100yr/24hr	20:05	0.942
100yr/24hr	20:10	0.936
100yr/24hr	20:15	0.931
100yr/24hr	20:20	0.926
_		
100yr/24hr	20:25	0.921
100yr/24hr	20:30	0.916
100yr/24hr	20:35	0.911
100yr/24hr	20:40	0.908
100yr/24hr	20:45	0.901
<u> </u>		
100yr/24hr	20:50	0.897
100yr/24hr	20:55	0.892
_		
100yr/24hr	21:00	0.887
100yr/24hr	21:05	0.883
<u> </u>		
100yr/24hr	21:10	0.878
100yr/24hr	21:15	0.874
100yr/24hr	21:20	0.869
100yr/24hr	21:25	0.865
100yr/24hr	21:30	0.861
100yr/24hr	21:35	0.856
_		
100yr/24hr	21:40	0.852
100yr/24hr	21:45	0.848
_		
100yr/24hr	21:50	0.844
100yr/24hr	21:55	0.84
100yr/24hr		0.835
	22:00	
100yr/24hr	22:05	0.831

100yr/24hr	22:10	0.827
100yr/24hr	22:15	0.823
100yr/24hr	22:20	0.82
100yr/24hr	22:25	0.816
100yr/24hr	22:30	0.812
100yr/24hr	22:35	0.808
100yr/24hr	22:40	0.804
100yr/24hr	22:45	0.801
100yr/24hr	22:50	0.797
100yr/24hr	22:55	0.793
100yr/24hr	23:00	0.79
100yr/24hr	23:05	0.786
100yr/24hr	23:10	0.783
100yr/24hr	23:15	0.779
100yr/24hr	23:20	0.776
100yr/24hr	23:25	0.772
100yr/24hr	23:30	0.769
100yr/24hr	23:35	0.766
100yr/24hr	23:40	0.762
100yr/24hr	23:45	0.759
100yr/24hr	23:50	0.756
100yr/24hr	23:55	0.752
100yr/24hr	24:00	0.749

[REPORT]
INPUT NO
CONTROLS NO
SUBCATCHMENTS ALL
NODES ALL
LIN S ALL

[TAGS]

[MAP]

DIMENSIONS 484.423998361705 -716.515824588729 982.219750200746 -253.463683636686 UNITS Meters

[COORDINATES]

;;Node	X-Coord	Y-Coord
;; JB1 1	686.035	-368.798
JB1 2	747.09	-442.227
JB1 3		-446.568
JB2 1		-372.979
JB2 2	739.806	-449.717
JB3 1	576.978	-374.104
JB3_2	687.282	-506.878
JB4_1	521.572	-373.582
JB5_1	**	-631.294
JB6_1		-621.368
JB6_2		-510.009
JB7_1		-454.506
JB7_2	776.546	-542.977
JB7_3		-478.98
JB8_1		-621.481
JB9_1	* *	-575.48
JHWY1_1	866.722	-589.351
JHWY1_2	890.146	-662.104 -633.927
JHWY2_1	822.423	-633.927
JHWY2_2	881.525 821.856	-691.469
JHWY2_3	755.251	-634.588
JHWY3_1 JHWY3_2	810.726	-691.653
_	754.89	-691.983
JHWY3_3	194.03	001.000

JHWY4_1 JHWY4_2 OF2 RetPond	746.585 699.405 621.152 668.481	-692.127 -688.815 -591.325 -528.515
[ERTICES]	X-Coord	Y-Coord
C11	529.951	-399.568
C11	619.431	-512.772
C23		-584.835
C23	741.247	-565.009
C24	681.003	-593.444
C24		-579.045
C24		-561.11
C26	820.421	-593.647
C29		-621.141
C29		-641.745
C31		-686.665
[Polygons] ;;Subcatchment	X-Coord	Y-Coord
;;		1-0010
B1	683.475	-364.144
B1		-274.512
B1		-353.082
B1	769.889	-374.068
В1	787.468	-395.952
В1	827.185	-442.539
B1	781.563	-490.069
B1	674.626	-363.982
B1	683.475	-364.144
В2	674.744	-364.452
B2	744.478	-448.133
B2	716.277	-477.883
B2	619.483	-364.189
B2		-364.452
B3		-364.094
B3		-364.491
B3	716.028	-477.746
B3		-510.269
B3 B4		-364.094
B4	511.038 507.051	-372.469 -362.369
B4	566.588	-363.964
B4	647.921	-462.307
B4	608.583	-507.491
B4	544.528	-429.88
B4	530.972	-411.541
B4	519.809	-394.796
В4	511.038	-372.469
В5	663.846	-578.594
B5	706.842	-533.047
B5	737.327	-568.277
B5	748.091	-588.384
B5	750.7	-598.906
B5	751.131	-605.521
B5	750.843	-630.254
B5	691.024	-640.895
B5	687.708	-622.621
B5	682.646	-610.008
B5	676.701	-600.608
B5	663.846 686.992	-578.594 -510.691
В6	000.332	-510.681

В6	715.963	-478.254	
В6	814.04	-592.81	
B6	814.572	-627.629	
В6	751.749	-624.819	
B6	751.432	-602.8	
B6	746.586	-584.889	
B6	737.104	-567.821	
В6	686.992	-510.681	
B7	716.277	-478.117	
B7	744.215	-448.396	
B7	806.581	-521.288	
B7	776.582	-550.234	
В7	716.277	-478.117	
B8	777.948	-550.619	
B8	806.782	-521.507	
B8	858.628	-583.889	
B8	866.941	-602.73	
B8	815.188	-632.429	
B8	814.268	-592.761	
B8	777.948	-550.619	
B9	781.563	-489.687	
	826.994	-441.966	
B9	907.497	-540.031	
B9	891.153	-564.802	
B9	859.636	-584.749	
B9	781.563	-489.687	
B9	858.976	-584.466	
HWY1	891.664	-564.291	
HWY1	906.731	-539.52	
HWY1	959.593	-600.299	
HWY1	935.588	-628.39	
HWY1	911.072	-649.586	
HWY1	887.716	-669.67	
HWY1	876.852	-646.266	
HWY1	873.277	-622.516	
HWY1	870.723	-611.024	
HWY1	866.893	-601.576	
HWY1	858.976	-584.466	
HWY1 HWY2	814.538	-631.644	
HWY2	867.278	-602.997	
HWY2	870.618	-612.006	
HWY2	873.022	-622.005	
HWY2	875.32	-636.562	
HWY2	877.123	-647.603	
	887.578	-669.76	
HWY2 HWY2	881.023	-675.572	
HWY2	872.22	-680.312	
HWY2	859.626	-685.999	
HWY2	847.838	-690.891	
HWY2	835.331	-694.649	
HWY2	824.33	-695.468	
HWY2	814.955	-695.11	
HWY2	814.538	-631.644	
HWY3	751.671	-624.944	
HWY3	814.211	-626.994	
HWY3	816.236	-694.831	
HWY3	751.831	-695.019	
HWY3	751.631	-624.944	
HWY4	691.303	-640.239	
HWY4	750.325	-629.773	
HWY4	750.323	-694.971	
HWY4	697.429	-695.115	
HWY4	693.711	-688.564	
HWY4	691.303	-640.239	
114A T J	0,1,000	0.10.200	

]	608.529 647.955 706.358 K-Coord	-508.146 -462.721 -533.229 Y-Coord
-	647.955	-462.721
(647.955	-462.721
(647.955	-462.721
(608.529	-508.146
		F 0 0 1 1 C
•	657.492	-571.816
(663.485	-577.943
-	706.358	-533.229
	1	706.358 663.485

13-129 <i>F</i>	Agri	Business	Post	Develop 100	Dyr		
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Analysis							
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		Dry Days					
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Routing	Time	e Step	• • • • •	5.00 sec			
WARNING	02:	maximum	depth	increased	for	Node	JB1_1
				increased			
				increased			
WARNING	02:	maximum	depth	increased	for	Node	JB2_1
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				increased			
				increased increased			
				increased			
				increased			
WARNING	02:	maximum	depth	increased	for	Node	JB6 2
WARNING	02:	maximum	depth	increased	for	Node	JB7_1
WARNING	02:	maximum	depth	increased	for	Node	JB7_2
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WARNING			depth	increased	for	Node	JHWY3 Z
WARNING WARNING	02:	maximum		increased increased			

Depth	Volume	******
mm	hectare-m	Runoff Quantity Continuity
		******
109.858	6.835	Total Precipitation
0.000	0.000	Evaporation Loss

Infiltration Loss	1.093	17.567
Surface Runoff	5, 719	91.914
Final Surface Storage	0.064	1.030
Continuity Error (%)	-0.594	
*******	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*******		
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	5.719	57.186
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.000	0.000
Internal Outflow	0.000	0.000
Storage Losses	0.000	0.000
Initial Stored Volume	0.000	0.000
Final Stored Volume	5.720	57.198
Continuity Error (%)	-0.020	

Link C20 (3.99%) Link C17 (1.32%)

Minimum Time Step : 1.38 sec
Average Time Step : 4.83 sec
Maximum Time Step : 5.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 2.00

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Total Runoff mm	Total Runoff 10^6 ltr	Pea Runof CM
B1	109.86	0.00	0.00	19.53	90.00	7.99	3.8
B2	109.86	0.00	0.00	14.44	95.07	3.57	1.9
В3	109.86	0.00	0.00	21.32	88.27	1.35	2.1
B4	109.86	0.00	0.00	20.06	89.46	5.50	2.6
B5	109.86	0.00	0.00	17.36	92.00	3.83	1.5
B6	109.86	0.00	0.00	16.06	93.42	4.92	2.4
В7	109.86	0.00	0.00	16.85	92.76	2.59	1.5
B8	109.86	0.00	0.00	15.50	94.03	2.79	1.5
В9	109.86	0.00	0.00	17.40	92.17	5.54	3.0
HWY1	109.86	0.00	0.00	20.08	89.47	4.16	2.0

HWY2	109.86	0.00	0.00	17.19	92.25	3.00	1.3
НМХЗ	109.86	0.00	0.00	16.62	92.98	2.84	1.6
HWY4	109.86	0.00	0.00	18.85	90.80	2.17	1.2
Pond	109.86	0.00	0.00	9.42	99.35	3.92	2.7

ode	Туре	Depth Meters	Depth Meters	Maximum HGL Meters	Occu days	of Max rrence hr:min
B1 1	CTIO	0.06	0.66	927.76	0	07:15
B1 2	CTIO	0.03	0.46	926.96	0	07:16
B1 3	CTIO	0.03	0.40	926.90	0	07:17
B2 1	CTIO	0.03	0.40	927.00	0	07:15
B2 2	CTIO	0.05	0.60	926.80	0	07:16
B3 1	CTIO	0.07	0.78	926.68	0	07:17
вз 2	CTIO	0.04	0.55	925.95	0	07:17
B4 1	CTIO	0.04	0.50	927.20	0	07:19
B5 1	CTIO	0.08	0.99	926.49	0	07:25
в6 1	CTIO	0.04	0.51	926.71	0	07:15
B6 2	CTIO	0.04	0.57	925.97	0	07:18
B7 1	CTIO	0.04	0.53	926.73	0	07:17
B7 2	CTIO	0.04	0.58	926.88	0	07:16
В7 3	CTIO	0.06	0.73	926.43	0	07:18
B8 1	CTIO	0.03	0.37	927.67	0	07:15
B9 1	CTIO	0.04	0.57	928.67	0	07:15
HWY1 1	CTIO	0.03	0.45	928.55	0	07:15
HWY1 2	CTIO	0.03	0.45	927.75	0	07:16
HWY2 1	CTIO	0.03	0.40	927.50	0	07:15
HWY2 2	CTIO	0.04	0.50	927.70	0	07:16
HWY2 3	CTIO	0.03	0.49	927.19	0	07:17
HWY3 1	CTIO	0.04	0.58	926.78	0	07:22
HWY3 2	CTIO	0.05	0.60	927.10	0	07:17
нжүз з	CTIO	0.05	0.76	926.76	0	07:23
HWY4 1	CTIO	0.06	0.85	926.75	0	07:23
HWY4 2	CTIO	0.24	1.28	926.63	0	07:24
OF2	O TFALL	0.00	0.00	923.20	0	00:00
RetPond	STORAGE	1.61	2.00	925.10	2	00:00

ode	€	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Occu	of Max irrence hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr
B1	1	CTIO	3.885	3.885	0	07:15	7.993	7.992
B1	<del>-</del>	CTIO	0.000	3.939	0	07:16	0.000	7.995
В1		CTIO	0.000	2.993	0	07:16	0.000	5.549
В2	1	CTIO	1.962	1.962	0	07:15	3.575	3.575
В2	2	CTIO	0.000	3.924	0	07:16	0.000	7.992
вз	1	CTIO	2.170	4.055	0	07:15	4.347	7.925
В3	2	CTIO	0.000	7.593	0	07:17	0.000	15.930
В4	1	CTIO	2.617	2.617	0	07:15	5.505	5.504
В5	1	CTIO	1.562	5.918	0	07:19	3.828	15.990

B6 1 B6 2 B7 1 B7 2	CTIO CTIO CTIO CTIO	2.465 0.000 0.000 1.536	2.465 7.919 2.961 2.954	0 0 0	07:15 07:17 07:17 07:15	4.921 0.000 0.000 2.593	4.920 15.851 5.543 5.386
B7 3 B8 1	CTIO CTIO	0.000 1.530	5.908 1.530	0	07:17 07:15	0.000 2.793	10.935 2.792
B9 1 HWY1 1 HWY1 2	CTIO CTIO CTIO	3.049 2.046 0.000	3.049 2.046 2.069	0 0	07:15 07:15 07:15	5.544 4.158 0.000	5.543 4.158 4.160
HWY2 1	CTIO	1.390 0.000	1.390 2.007	0	07:15 07:16	3.004 0.000	3.004 4.158
HWY2 3 HWY3 1 HWY3 2	CTIO	0.000 1.692 0.000	3.350 1.692 3.320	0 0 0	07:17 07:15 07:17	0.000 2.845 0.000	7.164 2.844 7.161
HWY3 3 HWY4 1 HWY4 2	CTIO	0.000 0.000 1.295	4.775 4.283 4.964	0 0	07:17 07:18 07:18	0.000 0.000 2.172	10.019 10.005 12.180
OF2 RetPond	O TFALL	0.000 2.781	0.000	0	00:00	0.000 3.918	0.000 57.191

Surcharging occurs when water rises above the top of the highest conduit.

			Max. Height	Min. Depth
		Hours	Above Crown	Below Rim
ode	Type	Surcharged	Meters	Meters
HWY4 1	CTIO	0.01	0.099	0.000

Flooding refers to all water that overflows a node whether it ponds or not.

Hours Rate Occurrence Volume	Depth
	Meters
B3 1 0.07 1.004 0 07:15 0.047 B5 1 0.31 1.137 0 07:16 0.345	0.78
HWY3 3 0.11 0.364 0 07:18 0.016	0.76
HWY4 1 0.21 0.508 0 07:17 0.051	0.85
HWY4 2 0.52 1.152 0 07:14 0.374	1.28

	Average	Avg	E I	Maximum	Max	Time of Max	Maximum
	Volume	Pcnt	Pcnt	Volume	Pcnt	Occurrence	Outflow
Storage ni	it 1000 m3	Full	Loss	1000 m3	Full	days hr:min	CMS
RetPond	45.843	80	0	57.184	100	2 00:00	0.000

Outfall ode	Flow Fre . Pcnt.	Avg. Flow CMS	Max. Flow CMS	Total Volume 10^6 ltr
OF2	0.00	0.000	0.000	0.000
System	0.00	0.000	0.000	0.000

Link	Type	Maximum Flow CMS	Occur		Maximum Veloc m sec		Max Full Depth
			_				-
C11	CHA E	2.161	0	07:20	2.16	0.38	0.67
C13	CHA E	3.939	0	07:16	3.30	0.70	0.74
C14	CHA E	2.961	0	07:17	3.50	0.19	0.62
C15	CHA E	3.008	0	07:17	2.04	0.38	0.83
C16	CHA E	5.739	0	07:18	3.64	0.93	0.86
C17	CHA E	7.929	0	07:18	6.39	0.51	0.75
C18	CHA E	1.915	0	07:15	1.54	0.23	0.77
C19	CHA E	3.762	0	07:19	2.41	1.05	0.87
C20	CHA E	7.464	0	07:18	6.29	0.48	0.73
C21	CHA E	2.993	0	07:16	3.26	0.45	0.64
C22	CHA E	2.941	0	07:17	1.90	0.50	0.86
C23	CHA E	2.498	0	07:16	2.39	0.38	0.70
C24	CHA E	4.867	0	07:26	2.40	1.01	1.00
C25	CHA E	4.537	0	07:19	2.20	1.11	1.00
C26	CHA E	1.466	0	07:15	1.64	0.19	0.63
C27	CHA E		0	07:16	1.48	0.43	0.89
C28	CHA E		0	07:15	1.89	0.22	0.58
C29	CHA E		0	07:15	2.51	0.29	0.60
C30	CHA E		0	07:16	2.20	0 . 22	0.64
C31	CHA E		0	07:17	2.11	0.37	0.66
C32	CHA E		0	07:17	2.86	0, 26	0.73
C33	CHA E		0	07:18	2.04	0.55	0.90
C34	CHA E		0	07:18		0.47	1.00
C35	CHA E		0	07:19	1.96	0.59	1.00
C39	CHA E		0	07:16	3.20	0.56	0.76
C6	CHA E	L 3.924	0	07:16	3.58	0.25	0.70

Conduit	Ad usted Actual Length			on of Down	Time i Sub				Avg. Froude umber	Avg. Flow Change
C11 C13 C14 C15	1.00 1.00 1.00 1.00	0.00 0.00 0.01 0.01	0.00 0.00 0.00	0.00 0.00 0.00	0.00 0.43 0.27 0.96	0.00 0.57 0.72 0.03	0.00 0.00 0.00	1.00 0.00 0.00 0.00	0.82 1.04 1.39 0.60	0.0000 0.0000 0.0000 0.0000

C16 C17 C18 C19	1.00 1.00 1.00 1.00	0.01 0.01 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.45 0.00 0.99 0.94	0.54 0.00 0.01 0.06	0.00 0.00 0.00 0.00	0.00 0.99 0.00 0.00	1.04 2.12 0.34 0.59	'0.0001 0.0000 0.0000 0.000
C20 C21	1.00	0.01	0.00	0.00	0.00	0.00	0.00	0.99	2.12	0.0000
C22	1.00	0.00	0.00	0.00	0.41 0.98	0.59 0.02	0.00	0.00	1.12 0.53	0.0000
C23 C24	1.00 1.00	0.00	0.00	0.00	0.88	0.12	0.00	0.00	0.78 0.77	0.0000
C25	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.13	0.0001
C26	1.00	0.00	0.00	0.00	0.99	0.01	0.00	0.00	0.60	0.0000
C27 C28	1.00	0.00	0.00	0.00	1.00 0.88	0.00	0.00	0.00	0.37 0.78	0.0000
C29	1.00	0.00	0.00	0.00	0.46	0.54	0.00	0.00	0.99	0.0000
C30 C31	1.00	0.01	0.00	0.00	0.52 0.78	0.48 0.21	0.00	0.00	0.87 0.78	0.0000
C32 C33	1.00	0.01	0.00	0.00	0.42	0.58	0.00	0.00	1.12 0.85	0.0000
C34 C35	1.00	0.01	0.00	0.00	0.44	0.55	0.00	0.00	1.06	0.0000
C39 C6	1.00	0.01	0.00	0.00	0.46	0.53 0.70	0.00	0.00	1.01 1.34	0.0000

****** Conduit Surcharge Summary ************

		Hours Full		Hours Above Full	Hours Capacity
Conduit	Both Ends		Dnstream	ormal Flow	Limited
C19	0.01		0.01	0.06	0.01
C24	0.01	0.01	0.01	0.28	0.01
C25	0.31	0.31	0.31	0.09	0.01
C34	0.11	0.11	0.11	0.01	0.01
C35	0.21	0.21	0.21	0.01	0.01

Analysis begun on: Tue May 27 17:29:58 2014 Analysis ended on: Tue May 27 17:30:03 2014 Total elapsed time: 00:00:05

# Appendix E – SMRID Agreement

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	*	

#### WATER CONVEYANCE AGREEMENT

Municipal and Rural Drainage (Irrigation Districts Act, Section 21)

This agreement is made this 18 day of August

2011.

BETWEEN:

#### ST. MARY RIVER IRRIGATION DISTRICT

(the "District")

-and-

#### **COUNTY OF LETHBRIDGE**

(the "Applicant")

#### **BACKGROUND:**

- The District is the owner and operator of a system of open ditch canals, buried pipelines and drainage channels
  and associated structures and infrastructure (the "Irrigation Works") used by the District for the conveyance and
  drainage of water for irrigation and other licenced purposes under the Water Act and the Irrigation Districts Act.
- Section 21 of the Irrigation Districts Act authorizes the District to enter into a Water Conveyance Agreement with any person for the removal of drainage water, storm water or wastewater (the "Drainage") from an area.
- 3. The Applicant applies for permission to continue to outlet historic Drainage flows into the Irrigation Works (the "Drainage Flows") or to outlet flows into the Irrigation Works in the future (the "Prospective Drainage Flows").
- 4. The Drainage is not natural flow and as such an Approval under the *Water Act* issued by Alberta Environment ("AE") to outlet that flow into the Irrigation Works is required.
- 5. The District requires assurances that the outlet for the Drainage into the Irrigation Works will not have adverse consequences on the Irrigation Works or on the persons or property of any person whose lands are adjacent to the Irrigation Works, or will not cause the flows in the Irrigation Works to exceed the Operational Capacity of those Irrigation Works.
- 6. In exchange for the ability to outlet Drainage Flows, or the opportunity to outlet Prospective Drainage Flows into the Irrigation Works, the Applicant, has agreed to accept responsibility for adverse consequences on the Irrigation Works or on persons or property of any person whose lands are adjacent to the Imagation Works.

# AGREEMENT:

IN CONSIDERATION OF THE COVENANTS AND MUTUAL OBLIGATIONS HEREIN CONTAINED AND SUBJECT TO THE COVENANTS, CONDITIONS AND STIPULATIONS HEREINAFTER SET OUT THE PARTIES AGREE AS FOLLOWS:

#### 1 Definitions

Wherever used in this Agreement, the following terms have the meaning set opposite them except where the context otherwise requires:

- "Agreement" includes all components of this Agreement including the Background, Agreement and any Schedules hereto:
- b) "Approval" has the same meaning as in the Water Act;

- c) "Drainage Flows" means the water which the Applicant has caused or allowed to outlet into the Irrigation Works at any time prior to this Agreement.
- d) "Free-Board" means the difference in elevation between the normal operating surface level of water in an open ditch canal and the elevation at which an uncontrolled flow of water would occur out of the canal onto the adjoining lands by flowing over the canal banks and over and around any other Imigation Works;
- e) "Highway" means roads, public places and public works that are subject to the direction, control and management of the Applicant as those terms are used in the Municipal Government Act;
- f) "Irrigation Works" has the same meaning as in the Irrigation Districts Act;
- g) "Operational Capacity" means that capacity of the Irrigation Works, both in terms of volume and rate of flow:
  - sufficient to meet the operating requirements of the District for delivery demands of all the irrigation systems served, irrigation drainage and return flows, and the amount of water needed to cover the estimated conveyance losses; plus
  - capable of conveying surface runoff entering the Irrigation Works from any source, including Drainage Flows or Prospective Drainage Flows from the Applicant, whether or not such drainage is the subject of an express authorization by the District; plus
  - iii) sufficient Free-Board to prevent damage to the Irrigation Works and to prevent the uncontrolled escape of water from the Irrigation Works onto lands adjacent to the Irrigation Works.
- h) "Operational Plan" means the specific policies and procedures implemented by the Applicant regulating the outlet of Drainage including but not limited to the timing, rate and duration of any outlets of Drainage by the Applicant to the Irrigation Works to ensure the Drainage does not cause any adverse effects on the Irrigation Works or persons or property located adjacent to the Irrigation Works including the provision that the Applicant will obtain the specific express consent of the District prior to the outlet of any Drainage.
- "Prospective Drainage Flows" means Drainage Flows which the Applicant proposes to outlet into the Irrigation Works at any time hereafter arising from future construction, modification, maintenance, or repair of a Highway, or future subdivision, or future development, or for any other reason or purpose;

# 2 Governing Agreement

- a) The Parties agree that this Agreement shall be the sole agreement governing the right of the Applicant to outlet Drainage into the Irrigation Works of the District.
- b) The Parties agree that this Agreement applies to all locations at which such outlet of Drainage occurs regardless of whether that outlet is regulated or controlled by any structure or device.
- c) The Parties agree that in absence of this Agreement the Applicant has no legal right, entitlement, privilege or permission to permit or allow the outlet of Drainage to the Irrigation Works of the District at any location or by any means.

## 3 Authorized Drainage Flow

The Applicant is authorized to permit or allow the outlet of Drainage Flows into the Irrigation Works subject to the terms and conditions of this agreement and the following conditions precedent:

- a) The Drainage Flow from the Applicant is the subject of an Operational Plan and a copy of which has been provided to the District;
- b) No Drainage Flows are permitted or allowed to enter the Irrigation Works without the express prior permission of the District.

## 4 Authorized Prospective Drainage Flow

a) The Applicant is authorized to permit or allow the outlet of Prospective Drainage Flows into the Irrigation Works after it has complied with section 21(6) of the Irrigation Districts Act which provides that:

21 (6) If a water conveyance agreement is entered into under this section, the district must not deliver or remove water under the agreement until the other party to the agreement has compiled with the requirements, if any, of the Water Act, the Environmental Protection and Enhancement Act and the regulations under those Acts.

b) The Applicant agrees:

- to apply to Alberta Environment ("AE") pursuant to the Water Act for an Approval for Prospective Drainage Flows into the Irrigation Works;
- to abide by the terms and conditions imposed by AE and to at all times material hereto maintain the Approval in good standing;

 to provide the District with copies of all applications and correspondence with AE and the Approval so received, and all terms and conditions of the Approval;

- iv) to ensure the Approval terms and conditions are included in any subdivision or development approvals issued by it for any subdivision or development from which Prospective Drainage Flows will outlet to the Irrigation Works;
- all outlets of Prospective Drainage Flows into the Irrigation Works will comply with the Approvals issued by AE;

vi) the Prospective Drainage Flows from the Applicant are the subject of an Operational Plan;

vii) no Prospective Drainage Flows are permitted or allowed to enter the Irrigation Works without the express prior permission of the District;

viii) to provide the District with a complete copy of all Operational Plans; and

ix) to ensure all outlets of Drainage are in compliance with the applicable Operational Plan.

## 5 Control and Ownership

- At all times material hereto the Irrigation Works shall be owned by the District and, subject to this Agreement, shall be under the direction and control of the District.
- b) The Applicant acknowledges that the District uses the Irrigation Works primarily for irrigation purposes and that use will result in fluctuations in the water levels and flows, which fluctuations are a natural consequence of the District's use of the Irrigation Works which the Applicant agrees it will accept as incident to access to the Irrigation Works and that the Applicant shall make no claims or demands upon the District of any nature or kind whatsoever arising directly or indirectly from the fluctuation of or the level of the water in the Irrigation Works. Provided however, that at all times the District agrees to operate the Irrigation Works in a reasonable and diligent manner and that the fluctuation in the water level is not caused by the negligence of the District, its servants, employees or agents. The District has no obligation to take any action or refrain from taking any action to alter or control the fluctuation of or the water level of the Irrigation Works under any circumstances whatsoever, and the Applicant agrees not to bring any claims or demands of any nature or kind, including any claims for indemnity or contribution under the Tort-Feasors Act or the Contributory Negligence Act arising directly or indirectly from the fluctuation or change in the water level of the Irrigation Works which may affect the ability to outlet Drainage and the Applicant agrees to indemnify and save harmless the District from all such claims and demands by whosoever brought.
- The District reserves the right to make any changes to the operating conditions of the Irrigation Works from time to time as in its sole discretion it deems advisable in the management and operation of its system of irrigation works which changes may result in an alteration of the water level and flows in the Irrigation Works, and the Applicant shall make no claims or demands upon the District whatsoever including any claims for indemnity or contribution under the Tort-Feasors Act or the Contributory Negligence Act arising directly or indirectly from the alteration in the water level of the Irrigation Works and the Applicant agrees to indemnify and save harmless the District from all such claims and demands by whosoever brought.
- d) The District may in its absolute discretion:
  - i) require the Applicant to install structures or control devices at uncontrolled outlet locations; or
  - ii) close any structures which outlet Drainage into the Irrigation Works and prohibit any or further Drainage from the Applicant into the Irrigation Works without providing notice to the Applicant under circumstances where:
    - the District is aware of conditions which it has reasonable grounds to believe are or may pose a danger to property, human health or public safety;
    - (2) the inlet structures are being operated contrary to the AE Approvals or contrary to the applicable Operational Plan;

and such closures may be for such time or times and may be subject to such conditions as the District may determine in its absolute and unfettered discretion.

#### 6 Contamination

The Applicant acknowledges that they are aware that the Drainage outletted into the Irrigation Works enters the main water conveyance system of the District and that that the District conveys and delivers water for irrigation, domestic, municipal, industrial and other purposes and that contaminants in the water may cause significant adverse effects to the environment, animal health or human health. The Applicant shall not allow or permit the outlet of Drainage that may contain a substance or substances in an amount, concentration or level or at a rate of release that causes or may cause a significant adverse effect to the environment, animal health or human health, and they each shall at all times material hereto comply with all release and reporting requirements and regulatory requirements of the *Environmental Protection and Enhancement Act* and regulations.

# 7 Liability, Indemnity and Hold Harmless

- a) Each party (the "Indemnifying Party") agrees to indemnify and save harmless the other party, its agents and employees from and against any and all damage, injury, loss, costs, causes of action, and claims suffered or incurred by the other party, its agents or employees and which are caused either directly or indirectly or contributed to in whole or in part by the negligence or breach of this Agreement by the Indemnifying Party, its agents and employees and in respect of which the indemnifying party, its agents or employees is held liable or is otherwise responsible in law and to the extent of that responsibility in whole or in part.
- b) The Applicant shall indemnify and hold the District harmless from any claim, action, cause of action or demand, including any fees and disbursements of counsel for the District or its liability insurer, as a result of any water which may escape or overflow from or be diverted to and fail to enter or be retained in the Irrigation Works or escape by overflow or otherwise in any manner from the Irrigation Works and for all damage caused by sald escape or release of water in any manner, including erosion, land instability, or by flowing water, and the Applicant indemnifies and holds harmless the District from all liability with respect to any losses or damage incurred by any person as a direct or indirect result thereof, provided however that such escape or release is due to or contributed to in any degree by the outlets of Drainage by the Applicant into the Irrigation Works, or the breach or non-compliance of the Applicant with any of the terms or conditions of this agreement or the applicable Operations Plan.
- c) The Applicant assumes full responsibility for and agrees to indemnify and save hamless the District and its agents and employees from all claims for bodily injury or property damage or clean-up or mitigation costs arising out of the discharge, dispersal, release or escape of acids, alkalis, toxic chemicals, fossil fuels, fossil or synthetic lubricants, liquids or gases, waste materials or other irritants, contaminants or pollutants into the Irrigation Works which cause or may cause a significant adverse effect to the environment, animal health or human health provided however that such escape or release is caused by or contributed to in any degree by the outlets of Drainage by the Applicant into the Irrigation Works.
- d) The District shall not be liable to the Applicant for any claim direct, indirect or consequential, for loss, injury or damage whatsoever arising out of the inability of the District to have any Operational Capacity available at any time material hereto in the Irrigation Works and the Applicant shall indemnify and save harmless the District from and against all damages, costs or expense of any kind whatsoever, brought by anyone against the District or incurred by the District in any way, including any fees and disbursements of counsel for the District or its liability insurer, resulting directly or indirectly by reason of any lack of Operational Capacity in the Irrigation Works or from the decision, and the consequences thereof, of the District in closing access to the Irrigation Works and prohibit any or further outlets of Drainage from the Applicant into the Irrigation Works as provided for elsewhere in this Agreement, including all costs and expenses incurred by the District in investigating, adjusting, and defending such claims on a solicitor and own client basis.

# 8 Fee

The District reserves the right, in its absolute unfettered discretion and subject to the Irrigation Districts Act (the "Act"), to impose by Bylaw a fee for the conveyance of the Drainage pursuant to section 115 of the Act which fee will be payable by the Applicant as specified in the Bylaw from and after the date upon which the Applicant is given notice of the passage of the Bylaw.

#### 9 Termination and Default

a) The Applicant may terminate its participation in this Agreement by giving 180 days written notice in advance to the District of its intention to so terminate setting out the date on which its participation will terminate (the



"Termination Date"), and from and after the Termination Date the Applicant shall no longer be entitled to outlet any Drainage into the Irrigation Works.

- b) In the event the Applicant defaults in the performance of any of it obligations hereunder, the District may, without terminating this Agreement, remedy such defaults, after giving the Applicant thirty (30) days notice of its intention to do so, except in the case of emergency, which can be remedied without notice. All costs and expenses incurred by the District in remedying such defaults shall be recovered from the Applicant as a debt due by the Applicant to the District.
- c) In the event that the District defaults in the performance of any of its obligations hereunder, the Applicant may, without terminating this Agreement remedy such defaults, after giving the District thirty (30) days notice of its intention to do so, except in the case of an emergency, which can be remedied without notice. All costs and expenses incurred by the Applicant in remedying such defaults shall be recovered from the District as a debt due the Applicant by the District.
- d) In the event the Applicant commits a continuing course of defaults or multiple unrelated defaults, the cumulative effect of which is to evidence a failure to comply with the applicable Operation Plans or the performance of any of its obligations hereunder, the District may, terminate this Agreement, after giving the Applicant thirty (180) days notice of its intention to do so.

### 10 Entire Agreement

- a) This Agreement contains the entire agreement between the parties and supersedes all prior agreements, communications or representations between the parties, whether in writing or orally, dealing with the same subject matter, and the Parties have no other rights therein, save those hereby conferred, or those by implication of law.
- b) In consideration of the performances of the parties and the covenants and agreements under this Agreement, all matters connected with any former agreements of earlier dates dealing with Drainage are cancelled and disposed of, and this Agreement is substituted for those former agreements effective the date of the signing of this Agreement and hereafter neither party shall be further obliged under the former agreements.

## 11 Assignment

Assignment or transfer of this agreement by the Parties is prohibited.

#### 12 Notices

a) Wherever in this Agreement it shall be required or permitted that notice or demand be given or served by either party to or on the other, such notice or demand shall not be duly given or served unless it is in writing and sent by registered mail or hand delivered, addressed as follows:

To the District at:

General Manager 1210 - 36 Street North P. O. Box 278 Lethbridge, Alberta T1J 3Y7

To the Applicant at:

County Manager

#100, 905 - 4th Avenue South Lethbridge AB T1J 4E4 Fax: 403-328-5602

Each such notice or demand shall be deemed given on the date of delivery if hand delivered, or by fax, or email, or five (5) days after the date of mailing if sent by registered mail. Any party may change their address for service from time to time by notice as above provided.

In the event of interruption of postal service notices as aforesaid will be deemed effectively served upon the parties hereto by hand delivery of such notice to the street address of the parties as aforesaid and the notices shall be deemed to have been served on the date on which they were actually delivered to the offices of the parties.



#### Enurement

This Agreement shall be binding upon the parties hereto and their successors from and after it having been executed.

# 14 Amendments

This Agreement shall not be changed or modified except in writing signed by all parties hereto.

# 15 Arbitration of Disputes

It is agreed by the Parties that either Party may upon notice to the other Party refer disputes in matters of difference between them under this Agreement, except those matters included in sections 5, 7 and 8 hereof, that may arise throughout the term of this Agreement that cannot be resolved in negotiations between them to the award and determination of a single arbitrator which will be appointed with the consent of the parties who shall have all powers given to arbitrators pursuant to the provisions of the Arbitration Act of Alberta and who shall proceed to enter the procedures thereunder upon the request of the parties towards the resolution of the dispute.

IN WITNESS WHEREOF the Parties have by their proper officers signed these presents and have affixed their seals as of the day and year first above written.

# St. Mary River Irrigation District

Per:

Dan /

County of Lethbridge

Per: